TELEDYNE MATERIALS RESEARCH WALTHAM MASS
FIRST SEASON RESULTS FROM SHIP RESPONSE INSTRUMENTATION ABOARD --ETC(U)
SEP 76 R R BOENTGEN, R A FAIN, J W WHEATON
SSC-264
NL

ASSEPTED

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- AD A 039752

ERRATA: PLEASE REPLACE LAST PARAGRAPH OF INSIDE FRONT COVER LETTER WITH THE FOLLOWING: This report contains a portion of the data with a preliminary discussion and injunction of the first season of data collection from 8 October 1972 to 5 April 1973. Similar reports on the second season and third seasons of data collection have been published and are available through the National Technical Information Service. Please refer to the outside rear cover for ordering information on those two documents

numbered SL-7-9 and SL-7-10.

SSC-264

(SL-7-8)

Technical Report

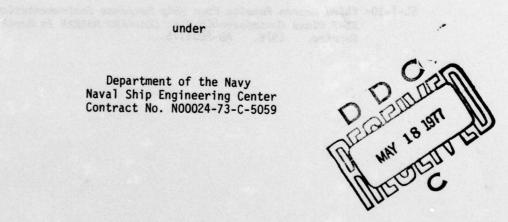
on

Project SR-211, "SL-7 Data Collection"

FIRST SEASON RESULTS FROM SHIP RESPONSE INSTRUMENTATION ABOARD THE SL-7 CLASS CONTAINERSHIP S.S. SEA-LAND MCLEAN IN NORTH ATLANTIC SERVICE

The cand the exposes to express by the end of the end o R. R. Boentgen, R. A. Fain, and J. W. Wheaton Teledyne Materials Research

Department of the Navy Naval Ship Engineering Center Contract No. N00024-73-C-5059



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> U. S. Coast Guard Headquarters Washington, D.C. 1976

ABSTRACT

This report contains data, with appropriate evaluation and discussions, collected during the first season on board the S.S. SEA-LAND McLEAN. Data collection began with westbound Voyage 1 on October 8, 1972 and terminated with the eastbound passage of Voyage 12 on April 5, 1973. A total of 80 data tapes were recorded containing in excess of 50,000 separate data intervals from more than 100 transducers.

Discussions include a description of the digitized data, comparisons of stresses with sea state, simultaneous response data from all transducers during selected portions of a rough voyage, and a consideration of torsional responses.

The reports from the second and third data-collection seasons are not being published in the Ship Structure Committee series of reports but they are available through the National Technical Information Service under the following titles.

- SL-7-9 Second Season Results From Ship Response Instrumentation Aboard The SL-7 Class Containership S.S. SEA-LAND McLEAN In North Atlantic Service. 1976. AD-A034162.
- SL-7-10- Third Season Results From Ship Response Instrumentation Aboard The SL-7 Class Containership S.S. SEA-LAND McLEAN In North Atlantic Service. 1976. AD-A034175.

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I. INTRODUCTION

The S.S. SEA-LAND McLEAN is the first of the new SL-7 class of high-speed containerships. Salient particulars of the vessel are given in Table I, and the vessel is shown in Figure 1. A multifaceted program of analysis and experiments, coordinated by the SL-7 Program Advisory Committee of the National Academy of Sciences--National Research Council, has been instituted to study this ship's structure and its responses to imposed loading. One important facet of this program is the collection of data on structural and dynamic responses of the actual (i.e., full scale) ship's structure. This is being accomplished by an on-board instrumentation system with sensors located throughout the vessel measuring strains, stresses, accelerations, various sea characteristics and ship operating parameters (see Reference 1). Presented in this report is a cross-section and summary of the data gathered during the first season of operation on North Atlantic Voyages 1-12 during the period 8 October 1972 to 5 April 1973.

Collection of full-scale data is necessary from a number of standpoints. Any predictions resulting from mathematical analyses or experimental models must accurately characterize the actual structure, or must be correctable, in a known way, to correlate the technique to the actual structure. Full-scale data, properly interpreted, provides the criterion against which all predictive techniques of structural response must be judged. A second but equally important use of full-scale data is to provide the input loads which form the basis of the rational design. Such load criteria can be gathered directly from a characterization of observed service conditions, such as wind and wave probability distributions, or inferred from the response of the vessel to the combination of these conditions. The latter scheme requires a knowledge of the structure's input-output or transfer function which again can be provided by adequate full-scale data describing loads and responses. In sum, full-scale data provides three indispensable parts of rational design: input loads, responses, and the derived characteristics of the link between the two.

Since different aspects of the full-scale data are of interest to different investigators, no summary can provide an exhaustive or even adequate characterization of all the gathered data. Indeed, the basic form of the data, analog or digital records on magnetic tape, is not reproducible here. The objective of this report, therefore, is to document the quantity, limits, and formats of the data now available and to present a cross-section and summary of it in a few of the forms most obviously useful to investigators. As a further aid to those interested, a description is given of some further possible data summary characterization and analysis schemes, along with their relative costs.

II. INSTRUMENTATION SYSTEM

The shipboard instrumentation system is described in detail in Reference 1; therefore, no attempt will be made in this report to duplicate that information. Rather, a brief description of the important features, with special emphasis on the data flow, will be presented as a convenient summary.



TABLE 1

CHARACTERISTICS OF S.S. SEA-LAND McLEAN

Nanc:	SEA-LAND MCLEAN
Builder:	Rotterdam Dry Dock (Hull 330)
Class:	SL-7 Containership
Length, overall	946' 1 1/2"
Length, between perpendiculars	880' 6"
Bean, molded	105' 6"
Depth to main deck, forward	64' 0"
Depth to main deck, aft	68' 6"
Draft, design	30' 0"
Draft, scantling	34' 0"
Dead weight - long tons	27,315
Displacement (34' 0" draft) - long tons	50,315
Machinery	Two separate cross-compound stems turbines driving two propeller shafts
Shaft horsepower-maximum continuous, both shafts	120,000
Propeller RPH	135
Speed, maximum, knots	33
Center of gravity - full load	399.32' forward of aft perpen- dicular 42.65' above base line

Container Capacity

	8' x 8.5' x 35'	8' x 8.5' x 40'	To:al
Below deck	354	140	694
Above deck	342	60	402
TOTAL.	896	200	1,096

A. Shipboard

All of the information obtained from the various transducers located throughout the vessel is recorded on two 14-track analog FM tape recorders located in the instrumentation room. Recorder No. 1, designated the primary recorder, records the same 13 signals whenever it is placed in operation. The fourteenth channel is used as a noise compensation channel during reproduction.

The second recorder has its first thirteen channels switched through four modes, designated A, B, C, and D. Each mode is recorded for thirty minutes sequentially. Channel 14 is again used as a compensation channel in all modes. Each 30-minute period is a data "interval", and is assigned an interval number. Any particular segment of data can thus be identified by referring to the following nomenclature.

- Tape number--(All odd numbers are from No. 1 Recorder and all even numbers are from Recorder No. 2).
- 2. Voyage number and direction (E = East, W = West).
- Index number (sequential numbering of each four-hour logbook entry accompanying each data tape).
- 4. Channel number and mode letter (Recorder No. 2 only)
- 5. Interval number.

Thus, by specifying "Tape No. 1, Voyage 1-W, Index 1, Channel 1-A, Interval 1" a very specific 30-minute data interval is identified. A complete summary of the signal assignments is provided in Table II. This presentation is in the same format used in Reference 1. Table III contains a list of sensor and signal abbreviations used in Table II and throughout this report.

Each interval of 30 minutes, whether on Recorder No. 1 or No. 2 is automatically preceded by a one-minute electrical zero and a one-minute period of calibration signals.

1. Strain Gage Signals

The majority of the transducers used in this system are obtained from various configurations of single-element strain gages with associated bridge completion and calibration resistors. These gages are attached to the surface of various hull structural elements. Each strain gage is constructed with inherent temperature compensation. That is, if the gage is attached to a plate which is subsequently warmed (or cooled) but is otherwise unrestrained, no change in strain will be indicated. If that plate is now restrained from expansion due to the temperature change, a strain, associated with the degree of restoring stress necessary, will be indicated even though no change in length occurred. Such a restraint is generated, for example, when the sun warms the deck or upper hull girder while the lower hull is in cooler water. This diurnal variation tends to induce compressive deck stresses and tensile stresses under the waterline even though the displacement tends to hog the ship.

п - 1

TABLE fI SENSOR LIST 72/73 Season and Calibration

Sensor	Sensor	1	Location (2)	Cantile) and and	Sensitive	Percentar	, enset	No.	Fell	ll of the	Circuit
		-	TOTAL CONTROL		1	3	Tan Tonay		-			
100	LVB	186 1	Tunnel Tops	Dyadic	Long.	V. Bend.	1	1		8214	ISA	1
7	TSM	186 1 S	Side N/A	Shear	Vert.	H.T. Shear	1	2		1667	PSI	•
•	Wave Ht.	300	Pud Deckhouse (Stbd)	Rader	Angled	Range (3)	1			3.6	Volt	
	Noll	178	26" Pud 31" ATT	Pend.	Trans.	Roll		,	•	20	De8.	
•	Pitch	178	26" Pvd 31' ATT	Pend.	Long.	Pitch	1	2		.20	Deg.	
•	MAV	178	23" Pud 31, ATT	Mass	Vert.	V. Accel.	1	9		1	*	
1	HAT	178	23" Fud 31, ATT	Mass	Trans.	T. Accel.	1	7	•	1	•	
	PAV	290	14" Pud 59' ATT	Mass	Vert.	V. Acrel.	1	60	•	1	00	
6	FAT	290	14" Fud 59' ATT	Mass	Trans.	T. Accel.	1	6		1		
10	Op Para.	•	RPH,(2)Rud, Wind 96D	Multiplex	1.	Transmitters	1	10	•	3.6	Volt	
11	CH3	186 1	Side NA	Dyadic	Long.	H. Bend	1.	п		8214	PSI	2
12	SRP	265	P Side 32' ATT	Shear	Vert.	Shear	1	12	•	2000	PSI	,
13	SFS	265	S Side 32' ATT	Shear	Vert.	Shear	1	13		2000	PSI	,
14 (1)	LVB						2	1	٧			
15	LSTS	186	S Tunnel Top	Dyadic	Long.	N. Stress	2	2	4	8240	PSI	•
16	LSMS	186	S Side N.A.	Dyadic	Long.	N. Stress	2	9	*	8240	PSI	2
17	LSBS	186	S Side Bottom	Dyadic	Long.	N. Stress	2	,	<	8240	ISA	6
18	LSTP	186	P Tunnel Top	Dyadic	Long.	N. Stress	2	s	4	8240	ISA	•
19	LSM	186	P Side NA	Dyadic	Long.	N. Stress	2	9	v	8240	154	2
20	LSBP	186	P Side Bottom	Dyadic	Long.	N. Stress	2	7	4	8240	PSI	2
21	SAP	87	P Side 26' ATT	Shear	Vert.	Shear	2	80	4	2000	PSI	
22	SAS	87	S Side 26' ATT	Shear	Vert.	Shear	2	6	4	2000	PSI	•
1	1	1		-	-		1			The state of the s		

					TABL	TABLE II (Continued)	0					II
					72/73 \$	72/73 Scason and Calibration	ation					- 2
Sensor No.	Sensor Non.	Frame	Frame Position	Config.	Orient	Sensitive	Recorder	Channel	Mode	Full	Units	Cfreuft No.
23	FDE7	307	Level 04 CL	Mass	Vert.	V. Accel.	2	10	4	+1 (4)	8	
77	THE	307	Level 04 CL	Mass	Trans.	T. Accel.	2	n	*	7	*	
25	ADHL	130	Level 05 1" P	Mass	Long.	L. Accel.	2	10 (0)	4	7		
26	ADIIT	130	Level 05 1" P	Mass	Trans	T. Accel.	2	11 (0)	*	7	•	
27	BCST	186 1	S Tunnel Top	Shear	Long.	Shear	2	12	4	2000	PSI	4
28	BCSB	186 1	S Tunnel Bot	Shear	Long.	Shear	2	n	4	2000	PSI	4
29 (1)	LVB						2	1				
30	AR-1A	143	(Port Side Girder	Single	Long.	N. Strain	7	2		334.6	/	•
31	AR-18	143	Near Deck Cutout	Single	Diag.	N. Strain	2	3	•	334.6	/	9
32	AR-1C	143	Under Deck	Single	Trans.	N. Strain	7	,	*	334.6	"/"4	9
33	AR-2A	143	C Stbd Side Gird.	Single	Long.	N. Strain	7	2	80	334.6	/	9
34	AR-28	143	Near Deck Cutout	Single	Diag.	N. Strain	2	9	m	334.6	"/"	9
35	AR-2C	143	Under Deck	Single	Trans.	N. Strain	7	7		334.6	"/""	9
36	AR-3A	143	CStbd Tunnel	Single	Long.	N. Strain	7	60	•	334.6	"/""	9
37	AR-38	143.	In Board	Single	Dieg.	N. Strain	7	6 .	•	334.6	/	9
38	AR-3C	143	C Under Deck	Single	Trans.	N. Strain	2	10		334.6	"/"	9
39	A8-4A	143	C Stbd Tunnel	Single	Long.	N. Strain	2	п		334.6	"/"	9
07	AR-48	143	Out Board	Single	Diag.	N. Strain	2	12		334.6	/	•
11	AR-4C	.143	Under Deck	Single	Trans.	N. Strain	2	13	•	334.6	1/14	•

TABLE II (Continued)
SFNSOR LIST

II - 3

Circuit No. Units 334.6 Full 2-13 L RSB 2-13 Channel r2-13 VIA RSB \(\begin{align*}
2-13 \\
VIA \\
RSB \\
(2-13 \end{align*} r2-13 r 2-13 VIA VIA 2-13 VIA RSB VIA VIA RSB Recorder 72/73 Season and Calibration N. Strain N. Struin N. Strain N. Strain N. Strain N. Strain N. Strain Sensitive N. Strain Trans. Trans. Trans. Orient Diag. Trans. Trans. Trans. Diag. Long. Long. Long. Diag. Long. Diss. Long. Long. Diag. Didg Single Single Single Config. Single Near Deck Cutout Near Deck Cutout Near Deck Cutout Out Corn. Hat 2 Port Side Gird Stbd Side Gird Stbd Side Gird In Corn. Hat 2 Stbd Side Gird Stbd Side Gird Location (2) Frame Position Under Deck Under Deck Stbd Tunnel Under Deck Stbd Tunnel Under Deck Stbd Tunnel Under Deck Under Deck In Board Under Deck In Board Under Deck Out Board LVB RZA RZA RZS R3A 838 42 (1) Sensor No. 6 6 6 6 6 6

TABLE II (Continued)
SENSOR LIST

11 - 4

72/73 Season and Calibration

No.	Sensor Non.	Prame	Location (2) Frame Position	Config.	Orient	Sensitive	Recorder	Channel	Mode	Full Cal	Unite	Circuit No.
	.04	35.0	1000 0000			7,000			,	7 7.1.		•
	ww	6.30	Stod Immet	TRUTC	.Suor	N. 5.141B	•	7	,	234.0		
89	868	258	Out Board	Single	Dieg.	N. Strain	2	VIV }	o	334.6	/	9
69	1860	258	Under Deck	Single	Trans.	N. Strain	2	L RSB	v	334.6	/	•
70	R10A	126	Stbd Side Gird	Single	Long.	N. Strain	.2	C 2-13	ပ	334.6	"/"v	•
11	RIOB	226	In Corn. Hat 4	Single	Diag.	N. Strain	2	AIV	v	334.6	/	9
72	N10C	226	Under Deck	Single	Trans.	N. Strain	2	(RSB	ü	334.6	/	9
73	RUIA	226	CStbd Side Gird	Single	Long.	N. Strain	2	C 2-13	v	334.6	./	9
74	RIIS	226	Out Corn Hat 4	Single	Diag.	N. Strain	2	AIA	v	334.6	1.4	•
75	RIIC	226	Underdeck	Single	Trans.	N. Strain	2	C RSB	v	334.6	./4	9
76	R12A	326	CStbd Side Gird	Single	Long.	N. Strain	2	(2-13	v	334.6	/4	•
11	R128	226	Near Deck Cutout	Single	Diag.	N. Strain	2	AIN	0	334.6	1./.,1	•
78	R12C	226	Underdeck	Single	Trans.	N. Strain	7	L 258	o	334.6	./	9
19	R13A	226	Cathd Tunnel	Single	Long.	N. Strain	2	(2-13	v	334.6	/4	9
98	R138	226	In Board	Single	Diag.	N. Strain	2	AIA	v	334.6	/	•
18	R13C	226	Cunder Deck	Single	Trans.	N. Strain	2	C RSB	v	334.6	/	9
82	R144	226	CStbd Tunnel	Single	Long.	N. Strain	2	C 2-13	v	334.6	/	•
83	8148	226	Out Board	Single	Diag.	N. Strain	2	YIA }	v	334.6	/	•
*8	R14C	226	Under Deck	Single	Trans.	N. Strain	2	L RSB	o	334.6	/	•
85 (1)	LVB						7	1	۵			
98	TGFS1	244	Pud Top	Single	Trans.	N. Stress	2	7	a	10038	PSI	•

					TABLE	TABLE II (Continued)						II
					SEN	SENSOR LIST						-
				distant.	2/73 Season	72/73 Season and Calibration						5
Sensor No.	Sensor Nom.	France	Location (2)	Confie	Orient	Sensitive	Percondar)	Wode	Full	Thefre	Circuit
100	WICCT	280	e c.de 11 pm	64-01		2000		100		10000		
	-			argure	rong.	N. 311688	•		•	8000	15.	0
=	TCFS2	244	Nd Bot.	Single	Trans.	N. Stress	2	9	0	10038	PSI	9
8	HLSSB	289	S Side I' ATT	Single	Long.	N. Stress	2	3 (8)	Α	10038	PSI	9
06	TGFS3	242	Aft Bot	Single	Trans.	N. Stress	2	,	۵	10038	PSI	9
16	HLSPT	289	P Side 1' BT	Single	Long.	N. Stress	2	3,	9	10038	PSI	9
92	TCFS4	242	Aft Top	Single	Trans.	N. Stress	2	\$	۵	10038	PSI	. 9
9.3	HLSPB	289	P Side 1' ATT	Single	Long.	N. Stress	1	\$ (6)	A	10038	PST	•
76	TCHS1	196	Pud Gird. Top	Single	Trans.	N. Stress	2	۰	٥	10038	PSI	•
95	TCMS2	196	Pud Gird Bot.	Single	Trans.	N. Stress .	2	,	0	10038	PSI	9
96	TCHS3	194	Aft Gird Bot.	Single	Trans.	N. Stress	2		4	10038	PSI	•
97	TORS4	194	Aft Gird Top	Single	Trans.	N. Stress	2	6	0	10038	PSI	9
86	TOWN	194	Pud Gird Mid	Single	Trans.	N. Stress	2	(e) 9	4	10038	PSI	9
66	TCHS2X	195	Bot Gird Mid	Single	Trans.	N. Stress	2	3,	•	10038	PSI	•
100	TCMS3X	761	Aft Gird Mid	Single	Trans.	N. Stress	2	(e) e	۵	10038	PSI	9
101	TGIS4X	195	Top Gird Mid	Single	Trans.	N. Stress	2	9 (a)	0	10030	154	•
102	TGSSIX	196	Pud Gir Q Top	Shear	Trans.	Shear	2	(e) 9	۵	2000	PSI	•
103	TGSS2X	196	Pud Gir Q Bot	Shear	Trans.	Shear	2	7.6	۵	2000	PSI	,
104	TCSS3X	194	Aft Gir Q Bor	Shear	Trans.	Shear	7	€ .	0	2000	PSI	,
105	TCSS4X	194	Aft Gir Q Top	Sheer	Trans.	Shear	2	(e) 6	4	2000	PSI	7
106	TCAS1	08	Pud Top	Single	Trans.	N. Stress	2	10	٥	10038	ISA	•
101	TCAS2	80	Pud Bot	Single	Trans.	N. Stress	2	11	۵	10038	PSI	•
108	TCAS3	78	Aft Bot	Single	Trans.	N. Stress	2	12	۵	10038	PSI	9
109	TCAS4	78	Aft Top	Single	Trans.	N. Stress	2	13	۵	10038	PSI	•

TABLE II (Continued)

TABLE II (Concluded)

SENSOR LIST

72/73 Season and Calibration

LVBS is Recorded on Channel 1 of Both Recorders in All Modes
To Nearest Frame
Slant Range: Deckhouse to Wave
Calibration Step 28 (± 18 from zero) 5993 Notes:

Abbreviations: Sensor Nomenclature - See Table II

Sensitive to -

Position - ATT is Above Tank Top

NA is Neutral Axis; BT is Below Tunnel

FR is Frame; Q is Quarterpoint

S is Starboard; P is Port; CL is Centerline (longitudinal)

S is Starboard; P is Port; CL is Centerline (longitudinal)

S is Starboard; P is Port; CL is Centerline (longitudinal)

H.T. Shear is Horizontal and Torsional Shear

N. Stress is Normal Stress (as opposed to shear stress)

V. Accel., T. Accel., L. Accel. is Vertical, Transverse, Longitudinal, Acceleration, respectively

Channel - (a) Denotes alternate channel assignment.

TABLE III

SENSOR AND SIGNAL NOMENCLATURE

ADHL	After Deck House Longitudinal (Acceleration)
ADHT	After Deck House Transverse (Acceleration)
AR ₁₋₄ (#)	Aft Rosettes, (%) denotes gage element:
	A is longitudinal orientation
	B is diagonal (45°) orientation
	C is transverse (athwart) to longitudinal
BGSB	Box Girder Shear Bottom
BCST	Box Girder Shear Top
YAV	Forward Acceleration Vertical (Hull)
PAT	Forward Acceleration Transverse (Hull)
YDHT	Forward Deck House Transverse (Acceleration)
PDHV	Forward Deck House Vertical (Acceleration)
MLSPB	Hull Longitudinal Strain Port Bottom
HLSPT	Rull Longitudinal Strain Port Top
MUSSB	Hull Longitudinal Strain Starboard Bottom
MLSST	Hull Longitudinal Strain Starboard Top
LHB	Longitudinal Horizontal Bending (Combination of LHBP and LHBS)
LHBP	Longitudinal Horizontal Bending Port (Stress)
LHBS	Longitudinal Horizontal Bending Starboard (Stress)
LSBP	Longitudinal Stress Bottom Port
LSBS	Longitudinal Stress Bottom Starboard
LSMP	Longitudinal Stress Mid Port
LSMS	Longitudinal Stress Mid Starboard
LSTP	Longitudinal Stress Top Port
LSTS	Longitudinal Stress Top Starboard
LVB	Longitudinal Vertical Bending (Combination of LVBP and LHBS)
LVBP	Longitudinal Vertical Bending Port (Stress)
LVBS	Longitudinal Vertical Bending Starboard (Stress)
MAT	Midship Acceleration Transverse (Hull)
HAV	Midship Acceleration Vertical (Hull)
R ₁₋₄ (2)	Rosettes (Forward), (2) denotes gage element:
	A is longitudinal orientation
	B is diagonal (45°) orientation
SAP	C is transverse (athwart) to longitudinal Shear Aft Port
SAS	Shear Aft Starboard
SPP	Shear Porverd Port
575	Shear Forward Starboard
TGAS	Transverse Girder Aft Starboard (Strain)
TGFS	Transverse Girder Forward Starboard (Strain)
TOPS 1-4	Transverse Girder Midship Starboard (Strain)
TGHS _{1X-4X}	Transverse Girder Midship Starboard (Strain, midpoints)
TGSS _{1X-4X}	Transverse Girder Shear Starboard (Midships, vertical quarterpoints)
TSH	Torsional Shear Midship (Combination of TSMP and TSMS)
TSIP	Torsional Shear Midship Port
TSMS	Torsional Shear Midship Starboard
2	

Sketches summarizing the locations of the strain gage sets are presented in Figures 2 and 3. It should be noted that the single-element strain gages used are installed in various configurations which have different properties. These are described in detail in Reference 1, but can be summarized as follows:

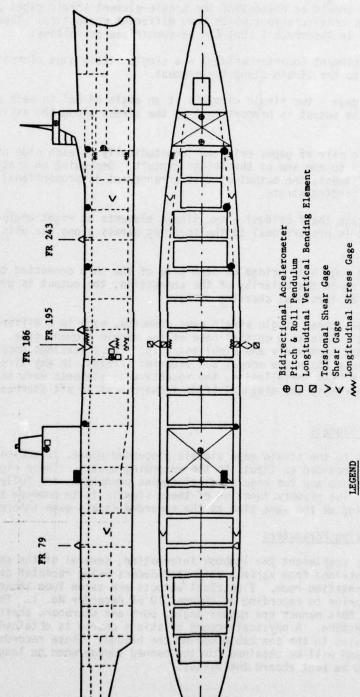
- a. Single element (quarter bridge) a single strain gage element. Its output is proportional to the strain along the element.
- b. Dyadic gage two single elements at an angle of 56° to each other. In this configuration the output is proportional to the stress along the axis of symmetry.
- c. A dyadic pair of gages oriented longitudinally on each side of the ship, each pair connected to one arm of the bridge circuit. Depending on whether the arms are opposite or adjacent, the output of this arrangement is proportional to the vertical or horizontal bending stress.
- d. Shear gage (half bridge) two single elements at right angles to each other. The output is proportional to the shearing stress along the axis of symmetry.
- e. A shear gage half bridge on each side of the ship connected to form a full bridge. Depending on the polarity of the connection, the output is proportional to the vertical or torsional shearing stress.
- f. Rosette three single strain gage elements, each in a different direction, near a point. This is a special case of the single element gage. Each signal output is recorded separately and simultaneously. These readings completely define the state of strain (both the normal and shearing strains, in any direction) at this point. In the McLEAN installation, the rosette gage elements were oriented in a longitudinal, athwartship and diagonal (from forward port to aft starboard) direction.

2. Transducer Signals

In addition to the strain gage signals discussed above, 10 additional transducer signals are provided as inputs to the recording system. These signals, eight linear accelerometers and two angular displacement pendulums, are fully described in Table IV. The primary function of these signals is to provide a record of ship motions occurring at the same time as the recorded strain gage information.

3. Ship Operating Parameters

In order to supplement the logbook information, several of the ship operating parameters are obtained from various ship transducers using repeater devices located in the instrumentation room. Electrical outputs are taken from these devices and multiplexed prior to recording on Channel 10 of Recorder No. 1. The five parameters obtained in this manner are rudder angle, port and starboard shaft RPM, and wind speed and direction. A physical record of ship's course is obtained from an analog recorder located in the sea cabin behind the bridge. These records are available at any time and will be obtained for the manned voyage when no longer required by regulation to be kept aboard the vessel.



ww Longitudinal Stress Gage △ Transverse Girder Gage

Three Arm Rosette
 Midship Torsional Shear Element
 Longitudinal Horizontal Bending
 Hull Longitudinal Strain

GENERAL SENSOR LAYOUT FIGURE 2

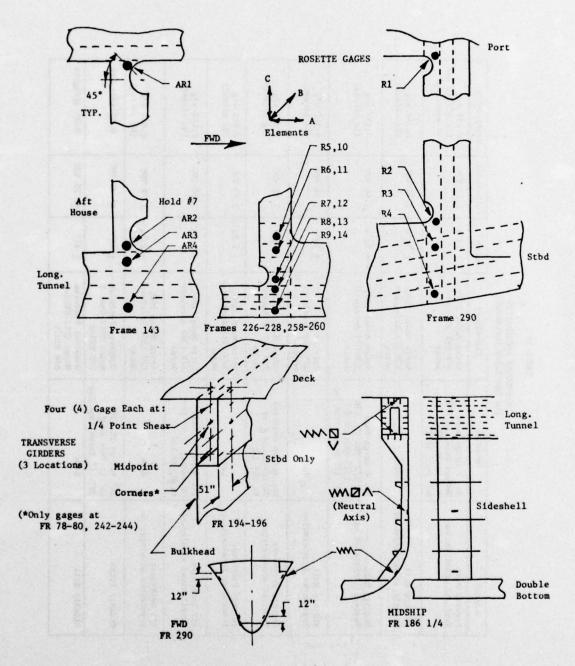


FIGURE 3
DETAILS OF STRAIN GAGE LAYOUT

TABLE IV

TRANSDUCER INFORMATION (As Initially Installed)

Signal	Location	Transducer	Range	Full-Scale	Sensitivity
Forward Hull Vertical Acceleration	No. 2 Cargo Hold Second Deck, 14 1/2" Fwd of FR. 290, 40" Port of €	Setra Model 100, S/N 068 Accelero- meter	+ 58 s	1.49 VBC	0.298 v/g (1g offset due to mounting)
Forward Hull Transverse Acceleration	Same	Setra Model 100, S/N 071. Accelero- meter	+ 5g's	1.72 VDC	0.344 v/g (No offset)
Midship Hull Vertical Acceleration	No. 6 Cargo Hold 23 1/2" Pwd FR. 178 11 1/2" Port of € 30' 11" Above Tank Top	Setra Model 100, S/N 072 Accelero- meter	+ 58'8	1.66 VDC	0.332 v/g (1g offset)
Midship Hull Transverse Acceleration	Same	Setra Model 100, S/N 070 Accelero- meter	s, 8c +	1.58 VDC	0.317 v/g (No offset)
Porward Deckhouse Vertical Acceleration	Wheelbouse Overhead O4 Level, on £ at FR 307 1/2	Setra Model 100, S/N 069 Accelero- meter	s, 85 -	1.55 VDC	0.317 v/g (1g offset)
Forward Deckhouse Transverse Acceleration	Same	Setra Model 100, S/N 1361 Accelero- meter	± 2.5g's	1.70 VDC	0.678 v/g (No offset)
Aft Deckhouse Longitudinal Acceleration 05 Level, 1" to Port of £, FR 130	Fan Room Overhead OS Level, 1" to Port of €, FR 130	Setra Model 100, S/N 1362 Accelero- meter	+ 2.58'8	1.60 VDC	0.642 v/g (No offset)
Aft Deckhouse Transverse Acceleration	Same	Setra Model 100, S/N 1360 Accelero- meter	± 2.5g's	± 2.58'e 1.72 VDC	0.686 v/g (No offset)
Midship Pitch	26" Pud of FR 178 26" to Port of € 30' 11" Above Tank Top	Humphrey Pendulum Model CP17-0601-1 S/N H3390	*5 + +5*	±2.25 VDC	0.05 w/degree
Midship Roll	Same	Humphrey Pendulum Model CP17-0601-1 S/N H2075	÷ 42.	±2.25 VDC	0.05 #/degree

4. Wave Height Radar

One parameter which has always presented a problem to the researcher is the measurement of the actual wave condition in a continuous manner. A new attempt to solve this problem has been made by including an "Ocean Wave Height Radar System" (OWHRS) developed by the Naval Research Laboratory as part of the instrumentation package. This device was operational for several voyages during the past season and the data, in the form of slant-range information, was recorded on Channel 3 of Recorder 1.

The signal, as recorded, contains the components of the various ship motions. These parameters must be removed before the true sea profile can be reproduced. No detailed analysis of this information will be presented in this document, but several samples of the data will be presented in subsequent sections.

5. Tucker Wave Meter System

A second attempt to achieve wave data has been made in this program by the inclusion of a Tucker Wave Meter aboard the vessel. This British device, which consists primarily of pressure cells and accelerometers mounted both port and starboard, was installed at the end of the first season's operation. Evaluation of data from this device will be one of the tasks undertaken when reducing second-season data.

6. Scratch Gages

As a supplementary program, mechanical scratch gage installations at a midship location have been installed on all eight vessels of the class. The device consists of a simple extensometer with mechanical amplification which causes a stylus to mark on sensitive paper. The paper is advanced once every four hours and the record thus obtained shows the maximum positive to maximum negative excursion of the stylus in a four-hour period. One scratch gage is located in each ship's starboard tunnel near the midship frame except for the McLEAN, which has one scratch gage in each tunnel. Data tapes are being sent directly to the Ship Structure Committee after collection by Teledyne. No data analysis is presently being undertaken by TMR, nor is the data presented in this report.

7. Logbook

An important adjunct to the data recorded on the two magnetic tape recorders is the data logbook kept by the instrumentation observer. Figure 4 shows typical logbook entries. Environmental conditions are noted here along with information to index the tape recordings. All sea, wind and wave conditions reported in this document are derived from this source.

8. Quick-looks

The data reduction process actually begins with "quick-look" playbacks made aboard the ship. Each tape is played back on an oscillograph at a relatively high speed, with a low paper speed. This produces a compact hard-copy record for review. Signal peaks, relative levels and overall variations may be judged from these records but details of the waveform cannot be seen.

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DATA LOG

Figure 4-A

198	WATCH FER FALSE START	Change of Course, Change of	Speed, Change of Ballast, Slamming, Change Tape, Reel Number) (Wave buoy launching)	RIB=1,2,3 4 - 63B=1,2,3 x	FOH ACCEC. & F.T.G.			Swite PITCHING IN LONG.	FIRST TIME SEEN THISTYPE		GPRAY TRON TOP OF BOW		RSB-5-6-7-8 & 446			IND THEE 21 \$ 22	START TAPE # 23 \$ 24	
		8	Initials	£78 "	-119-1	4.5			v. \				70					
		2	Weather	CLDY RAIN	SCAST	677	PCLBY	O'CAS!	o'cast	Kerst	6622	درمع	O'CAST	6000	1872 20/20	PTCCBY	PTCLDY	O'CAST
		7	Air Temp.	48/34	36/5	37/25	81/2 Péles	53/52	2-1/55	2.5/45	15/25	23/25	52/55	1,40	62/20	64/63		
		[2]	Sea Temp.	5.5	5.2	27	42	89	19	57		42	42	47	49	49	97	99
SEA -		Z	Barometer Reading	30.10	30.08	30,30	29.97	29.93	29.80	29.77	29.63	29.48	29.52	29.38	29.48	29.50	25.571	25,63
		21c	Relative Direct.	014	45.E	15.P	42.P	356	16 P	32P	37.P	312	3/2	先がん	375	53.5P	37.6	55.2
J	21 SWELL	41Z	Avg. Length	siene	5400,	,009	000	2.7	009	009	200	009	2009	200	300	3,00	3,00	225
		218	Avg. Height'	2-3	,01	101	10-12	21-91	12-15	12.15	12-15	10-12	10-12	21-01	31-8	8-10	8-10	8-7
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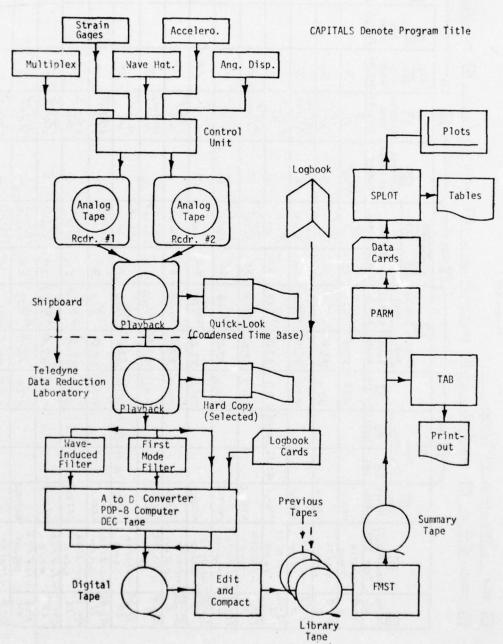


Figure 5 SCHEMATIC OF DATA FLOW

In sum, shipboard data gathering produces analog magnetic tapes of the recorded data from two tape recorders running simultaneously. In addition, a manual logbook record is maintained which correlates the magnetic tape data with the conditions existing at the time of the data. Quick-look records are also produced for on-site quality control purposes, but these have little application to most data analysis procedures except for scaling an overall maximum value for each interval.

B. Data Analysis Operations at TMR

1. Hard-Copy Analog Records

As shown in Figure 5, the preponderance of data reduction takes place after the recordings are removed from the ship. After review of the logbook records and taking into account the notes of the on-board observer, certain sections of data are played back onto hard-copy oscillographic records. Details of this operation depend on the type of analysis being done; it may be desired to compare one channel relative to another for a long period, or only the response for a short period around some event such as a slam. Examples of hard-copy analog records are presented in later sections.

2. Filtering and Digitizing

Most large-magnitude stress records, especially those associated with slamming and similar dynamic events, can be separated into two components: wave-induced, and first mode ("whipping", or "springing"). Each component is characterized by its frequency. First-mode frequencies are typically on the order of 1 Hz, while wave-induced components are lower in frequency (i.e., longer in period). Separation of these components is accomplished by passing the electrical signal representing the stress level or sensor output through electrical filters adjusted for the appropriate bandpass frequencies. The resulting filtered signal (or the original combined signal) may then be reproduced on an oscillograph to produce a hard copy, or it may be digitized in order to change its format for further processing.

Certain channels are selected for digitizing and further processing into library tapes. The details of this process are presented in Reference 2. In this step the logbook record is collated with the corresponding stress or motion data. In addition to a digitized data record, this operation also computes numbers characterizing each data interval, such as the maximum peak-to-trough, root-mean-square (RMS), number of peaks, etc. Some of these data have been used further in various analyses described below.

The library tapes can be further summarized by deletion of the complete digitized record. This summary tape can provide a computer-generated listing of environmental and characteristic data. Examples of these data are provided as a separate Appendix to this report. The summary tape also provides the data base for the parametric studies discussed below. Header block and data summary block formats for summary tapes are given in Tables V and VI, respectively. It should be noted that summary tapes do not contain data on which to base spectra, nor, as presently structured, do they contain computed values for the original waveform. Values reported are only for the wave-induced (maximum, RMS) and first-mode (maximum only) components.

A general summary of the SL-7 data formats currently available is presented in Table VII.

	TABLE V DIGITAL TAPE HEADER BLOCK FORMAT	
Byte	Information	Format
1 - 134	Tape Identification	8-bit EBCDIO
135 - 138	Number of Voyages on Tape	32-bit binary
139 - 142	First Voyage Number	8-bit EBCDIO
143 - 146	No. Intervals in First Voyage	32-bit binary
147 - 150	Second Voyage Number	8-bit EBCDIO
151 - 154	No. Intervals in Second Voyage	32-bit binary
155 - 158	Third Voyage Number	8-bit EBCDIO
159 - 162	No. Intervals in Third Voyage	32-bit binary
	and so forth	
	unused bytes zero-filled	

-21-TABLE VI INTERVAL SUMMARY BLOCK FORMAT

Byte	Information	Format	Byte	Information	Format
1-7+11-12	Analog Tape Number	8-bit	119- 128	Blanks	8-bit
8- 10	Voyage Number & Direct.	EBCDIC	129- 157	Comments	EBCDIO
13- 15	Logbook Index Number		158- 256	Zeros	
16- 18	Interval Number		257- 260	No. Wave Induced Cycles	32-bit Binary
19- 26	Date				
27- 30	Time (Eastern Std.)		261- 264	No. of Bursts of Wave- Induced Stress	
31- 37	Latitude				
38- 45	Longitude		265- 268	RMS Wave-Induced Stress, psi	
46- 48	Course	25 86/100	and Miles	Toront extrator	
49- 52	Ship Speed (MPH)		269- 272	Max. P-T Wave- Induced Stress, psi	
53- 56	Shaft RPM		273- 276	Max. P-T 1st Mode Stress, psi	
57- 58	Beaufort Sea State	AP PER	370 S S S S S S S S S S S S S S S S S S S		
59-1-62	Relative Wind Dir.				
63- 64	Relative Wind Vel. (knots)		277- 280	Mean Relative Stress Level	1
65- 66	True Wind Velocity (knots)		401- 404	lst Wave-Induced P-T Detected	32-bit Binary
67- 70	Relative Wind Dir.	190	405- 408	2nd Wave-Induced P-T Detected	
71- 72	Wave Height (feet)		CARLO DATA CARLO		
73- 74	Wave Period (sec.)		409- 412	3rd Wave-Induced P-T Detected	10/192
75- 77	Wave Length		marie Rose V		
78- 81	Relative Swell Dir.				
82- 84	Swell Height (feet)				
85- 88	Swell Length (feet)			•	
89- 93	Barometric Press, "Hg		2273-2276	469th Wave-Induced P-T Detected	
94- 95	Sea Temp. (°F)				
96- 98	Air Temp. (°F)		2277-2280	470th Wave-Induced P-T Detected	+
99- 118	Weather				

TABLE VII

SUMMARY OF CURRENT DATA FORMATS

Format	Characteristics
Analog Tapes	Recorded at 0.3 ips, FM IRIG low-band, 270 Hz center frequency13 data tracks, 1 compensation tracktape l" wide, 0.001" thick, 3600 feet on 10 1/2-inch reels. Each 30-minute interval preceded by zero and calibration signals.
Oscillograph Records	Quick-looks reproduced aboard ship at 200:1 speed up3 to 4 tracks per recordall tracks reproduced30 minutes occupies about 3 inches of record.
	Expanded time-histories of selected tracksused for instantaneous comparisons.
Digital Library Tape*	12,000 data points at 10 samples/second (real time) (unfiltered) from each interval of selected transducers on Recorder No. 1, plus logbook data, plus computed values-approximately 700 intervals.
Summary Tape*	The Digital Library Tape with the digital record deleted, leaving computed results and logbook data. One Summary Tape contains data from the entire season from one transducer.
Logbook	Environmental and ship operational data manually entered by system operator. Data is coded and entered on Digital Library Tape.
TAB Printout*	All logbook data plus computed data characteristics for each transducer, from the Summary Tape.
PARM Data Cards*	RMS and maximum data values plus selected logbook data for parametric studies.
SPLOT Output	Plots of data means vs. any parameter (such as Beaufort Number), classified into families of five subgroups. Tabulations also available (see Appendix B).

*See Reference 2-b.

III. RESULTS

In general, the results of the first season of manual data acquisition were gratifying. Large quantities of high-quality data were recorded. In any equipment of this complexity operating over an extended period, some failures or breakdowns are expected. However, due to the presence of the observer/operator, the effects of these were minimized and they were quickly corrected. His presence also assured proper correlation of the vital environmental data.

A. 1972-1973 Operating Season

It was originally planned to have the system operational in time to take part in both builder's and owner's sea trials. Unfortunately, due to the number of additional passengers scheduled during these tests, it was not physically possible to have Teledyne engineers aboard the vessel. At the time of the first trial, the system had been fully installed but had not had its final adjustments completed.

Manned Operations

Two Teledyne engineers met the vessel in Rotterdam upon her return from her first sea trials on September 16, 1972. These engineers worked aboard until September 28, 1972 when the vessel went on its second trial. It was decided that it was still impossible for Teledyne engineers to take part in the trials, although the system was operational and ready to record data. The ship left on Sunday, October 8, 1972, for New Jersey with two Teledyne engineers aboard. Recordings began on that date and continued throughout the westbound leg of Voyage 1. Both engineers rode the vessel to New Jersey. During this voyage and subsequent roundtrip Voyages 2 and 3, two Teledyne engineers rode the vessel. This manning scheme allowed TMR to have four engineers trained in system operation, and provided the additional manpower required during the system start-up.

2. Voyage Summaries

A summary of the voyage and data as recorded by dates and tape number is listed in Table VIII. With the exception of the westbound leg of Voyage 5, the vessel was manned by TMR personnel during each crossing from Voyage 1 in October, 1972 to Voyage 12 in April of 1972. Manning was terminated for the season when the ship returned to Rotterdam for drydocking in April, 1973.

3. Logbook Data

During each crossing the operator kept a data log in which he made indicated entries once every four hours. Logbook index numbers begin at No. 1 for each crossing and typically there are 30 to 32 entries per crossing.

The recording plan during the past season was to record for two out of every four hours when operating in the automatic mode. Thus, there are normally four data intervals associated with each log index entry, and, since a tape can run for a maximum of 40 hours real time and each data interval is 30 minutes in length, it is theoretically possible to have 80 intervals per tape. In practice, the operators have changed tape in each machine at the beginning of each voyage. These first tapes normally contain 68 to 72 intervals, allowing for unused tape at the beginning and end of each reel. Usually a little more than half way across two new tapes are loaded. These second tapes have varying numbers of intervals dependent on such items as the ship's speed, associated progress, and just when the system is secured. This

TABLE VIII

ANALOG TAPE AND VOYAGE SUMMARY

Voyage	Direction	Data Collection Dates	Produced (Tape Numbers)	Number of Tapes	
1	West	10/8/72 to 10/13/72	1,2,3,4	4	
2	East	10/15/72 to 10/19/72	5,6,7,8	4	
2	West	10/23/72 to 10/27/72	9,10,11,12	4	
3	East	10/29/72 to 11/2/72	13,14,15,16	4	
3	West	11/6/72 to 11/10/72	17,18,19,20	4	
4	East	11/12/72 to 11/16/72	21,22,23,24	4	
4	West	11/19/72 to 11/24/72	25,26,27,28	4	
5	East	11/26/72 to 12/4/72	29,30,31, 32,33,34	6	
5	West	Vessel Not No Data Collec	fanned		
6	East	12/29/72 to 1/4/73	35,36 One Recorder Time-Shared	2	
6	West	1/7/73 to 1/12/73	37,38 One Recorder Time-Shared	2	
7	East	1/14/73 to 1/19/73	39,40,41,42	4	
7	West	1/24/73 to 1/29/73	43,44,45,46	to 4 wisse A	
8	East	1/30/73 to 2/4/73	47,48,49,50	4	
8	West	2/8/73 to 2/13/73	51,52,53,54	4	
9	East	2/15/73 to 2/20/73	55,56,57,58	7.7 X-100 x 2	
9 11	West	2/24/73 to 3/1/73	59,60,61,62	il: 4 ventant	
10	East	3/3/73 to 3/8/73	63,64,65,66	grave sono e Statura ana	
10	West	3/11/73 to 3/15/73	67,68,69,70	n I Menson and T	
11	East	3/19/73 to 3/24/73	71,72,73,74	redan adınır da Androdaya	
11	West	3/26/73 to 3/30/73	75,76,77,78	tilans enough as foldinger	
12	East	4/1/73 to 4/5/73	79,80	2	
		the lifest made	mina allert a	ylithous is	

past season an average of 48 to 50 intervals are found on the second tapes. In summary, during each crossing 2 tapes are usually recorded on each tape machine. The interval numbers on each tape can run from 1 to 80 and these intervals are associated with logbook indexes 1 to 32 for each crossing.

4. Sea State Profiles

To assist in understanding the distribution of sea states encountered during the first data season, Figure 6 has been prepared. This figure depicts the occurrences of the various Beaufort Numbers reported divided into eastbound and westbound voyages. The basis for these data is the logbook entry for sea state recorded once every four hours by the operator. A total of 623 entries were made during the recording season; 324 during eastbound crossings and 299 during westbound. Normally, four data intervals (30-minute recording periods) are associated with each log entry. Thus, to obtain the total number of data intervals available at each sea state, it is necessary to multiply the number of logbook entries by four. The dominant Beaufort Numbers are in the range of 3 to 7, with the most entries obtained at Beaufort 4.

A summary of the more important logbook data is presented in Appendix A. This listing contains the following data:

- a. Voyage Number and Direction
- b. Recorder No. 1 Tape Number
- c. Interval Number
- d. Index Number
- e. Date
- f. Time (GMT)
- g. Ship Speed in Knots
- h. Beaufort Number
- i. Relative Wave Direction
- j. Weather Observation
- k. General Comments

5. Static Calibration

In order to obtain verification of the accuracy of the instrumentation system operation a static calibration test was performed on the vessel at the loading terminal in Rotterdam on April 9 and 10, 1973. This test sequence, by judiciously controlling the unloading sequence, was designed to create known, or at least calculable levels of bending and torsional stresses. By comparing calculated values with system outputs a judgment of instrumentation system performance is obtained. The results of this experiment are not reported here but have been issued as a separate document (see Reference 3). However, the following general conclusions can be drawn based on the data gathered during the calibration experiment:

- a. The maximum observed normal stress for the calibration loadings occurs in the hatch corner doublers (Hatch 9) just forward of the aft house in a direction parallel to the deck and at an angle of 22 degrees to the ship centerline. Other hatch corners, at stations where hatch width changes are encountered, exhibited high shear stresses near the stress relief cutouts.
- b. The maximum calibration stresses are one-eighth to one-half of the maximum peak-to-trough stress observed under normal seaway conditions. To put it

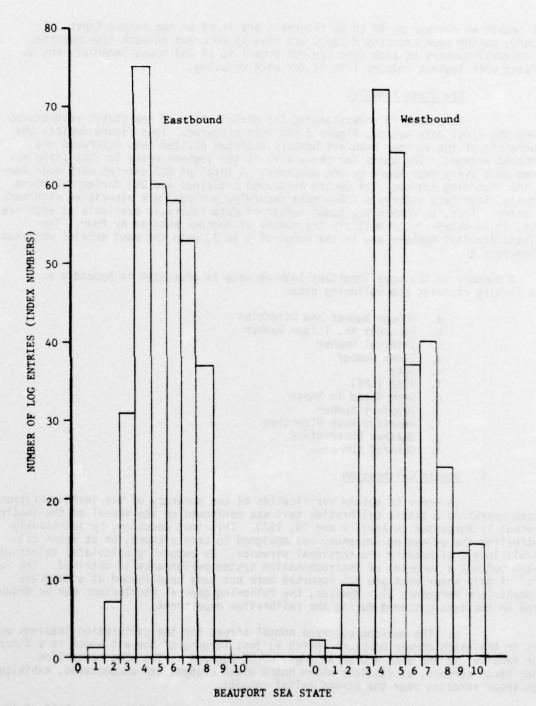


FIGURE 6
Sea State Profiles 1972/73 Season

another way, the applied calibration loads, or load distributions are approximately one-eighth to one-half of those generated in a seaway for most gages.

- c. Due to the low strain levels induced and the temperature differences encountered during the calibration, thermal effects could account for a substantial portion of most measured strains.
- d. The midship transverse girder is a more sensitive indicator of torsion than the midships torsional shear sensor installation.

6. System Reliability and Performance

System performance during the first season was consistent with that expected from an installation of this magnitude. No strain gage circuits experienced any failures. During Voyage 6 and part of Voyage 7 tape recorder problems were encountered which required the time-sharing of one unit until an additional machine could be obtained and the defective unit repaired. It should be pointed out that most of the equipment in the system is not new and has seen previous sea duty on both the ABS "Large Tanker Program" and two years of operation aboard Sea-Land's S.S. BOSTON.

Several data amplifiers did fail but on-board spares permitted replacement within a short time. In addition, failure of several of the accelerometer units were experienced. By selective switching of units, it was possible to keep the signals of primary interest operational during most of the data intervals.

In general, system performance was good and the fact that it was operator-controlled contributed to its overall excellent reliability.

The system was re-energized in the Fall of 1973 prior to the first manned voyages of the second season.

B. Data Presentation

1. General

As listed in Table VIII, 80 analog data tapes were produced during the past operating season, 40 from each recorder. A data summary book has been prepared for reference wherein every interval on every tape is identified by transducer.

During the first season, Voyage No. 4 presented some of the most interesting data from the standpoint of exhibiting the heaviest weather with a variety of relative sea directions. Since some characterization of the response data from all transducers was desired, but the volume of data available was large, this voyage was chosen for presentation in detail. Parametric studies were undertaken for all voyages, however.

2. Parametric Studies

Starting with the Summary Tapes, eight Recorder No. 1 data channels were selected for processing by the parametric studies computer program (see Reference 2 and Figure 5). These channels were:

- a. Channel 1 Longitudinal Vertical Bending (LVB)
- b. Channel 2 Torsional Shear Midships (TSM)
- c. Channel 4 Roll
- d. Channel 5 Pitch
- e. Channel 8 Forward Vertical Acceleration (FAV)
- f. Channel 11 Longitudinal Horizontal Bending (LHB)
- g. Channel 12 Shear Forward Port (SFP)
- h. Channel 13 Shear Forward Starboard (SFS)

The RMS and maximum peak-to-trough wave-induced component of each of the above parameters was plotted against Beaufort Number (although this is a wind scale, the number reported corresponds generally to a well-defined sea condition) in various families of ship speed or relative sea directions. In order to derive a single characteristic value within each Beaufort Number, the mean of both the maximum and RMS values per interval were plotted. These results are presented in Appendix B. Three types of data presentations are included for each data set:

- a. A dot-plot of all values, interval RMS or maximum peak-to-trough.
- b. A mean value plot of interval data set against ship speed or relative wave direction groups.
- c. A tabular listing giving the number of points upon which the curves are based and the set of standard deviations.

Extensive tabulations of digitized stress, motion, and logbook data are available to those interested through the Ship Structure Committee.

3. Maxima Observed on Recorder No. 2, Voyage 4

In order to present a sampling of the extreme data seen by Recorder 2, all of the data for Voyage 4 (E&W) was played back on an oscillograph, annotated, and scaled. In this manner a maximum peak-to-trough value was measured for each transducer for each interval. These data are presented in Table IX. As noted previously, Recorder No. 2 data are monitored in four consecutive modes. Some of these modes are switched, however, to record other data. This is reflected in Table IX. It should also be noted that the various maxima listed for any one interval did not necessarily occur at the same time.

4. Simultaneous Response Data

It is often useful to compare a response waveform occurring at one spot with that occurring at another spot at the same time. The complete records (all Recorder No. 1 and No. 2 signals recorded at the selected instances) from four examples of high sea state conditions are presented in Figures 7, 8, 9, and 10, each representing a different relative sea direction; i.e., head, broad-on-the-bow, quartering and following.

5. Averaged Midship Maximum Stresses, Voyage 4

Six longitudinal strain gage arrays are located at midship, on the top, mid and bottom sideshell, port and starboard. These are some of the most interesting

(Text continued on Page 105)

TABLE IX

Sheet 1 of 8

VOYAGE 04 EASTBOUND TAPE 22 RICORDER #2

					1	יופלן קייין וייין ויין וייין ויייין וייין ויייין ויייין ויייין ויייין וייין וייין וייין וייין וי	TO THE PARTY OF TH	101010	a now	(psr)			3	(6,5)
Index No.	Interval No.	State	LSTS	LSMS	LSBS	LSTP	LSMP	LSBP	SAP	SAS	BGST	BGSB	FWD HOUSE VERTICAL	FAD HOUSE TRANS.
1	1	4	2017	629	1281	2746	484	1236	1111	1200	277	333	.18	.12
7	5	3	4852	1648	2014	4504	1260	1977.	2333	2333	777	599	07.	.12
~	6	7	1049	2636	2197	6921	1744	1977.	3333	3000	833	733	.53	.16
7	13	9	6866	2966	7486	6688	2423	5850	3722	9907	833	733	.71	.20
2	11	1	9430	7767	5218	9338	3392	8240	9997	5466	1277	799	.98	.34
9	21	80	10712	6592	5676	10986	4362	8157	5166	5266	1222	1066	1.16	97.
1	25	1	7690	4065	3021	5273	3199	5932	3055	2800	833	999	68.	.34
00	29	1	5310	3076	2563	4724	2423	4120	2333	2133	999	888	.71	.38
6	33	9	8697	3296	4577	8433	2617	6427	4111	4333	576	733	.89	07.
91	37	1	5493	2526	3112	4504	1938	3213	1777	2600	611	533	.93	.28
111	41	2	5584	2856	3387	5053	2035	3625	2277	2266	833	599	.62	07.
12	45	9	5127	2966	2746	4174	1841	3296	2000	2666	833	995	.67	.34
13	67	2	7324	3405	3662	8789	2423	4532	2555	2800	888	997	.76	77.
						TAPE	54	RECORDER #2	1,2					
14	1	2	7873		3939	6921	2472	5022	3222	3600	833	533	.67	.32
15	5	2	5493		2929	5822	2197	4316	2222	2733	777	999	.67	.32
16	6	2	5218		3204	4065	1831	3845	1944	2666	611	733	67.	.26
11	13	2	4303		2655	4065	1831	3139	2333	1866	722	997	67.	.28
13	17	4	4852	2417	2197	3845	1464	2982	2055	2066	777	333	.58	.20
19	21	1	4211		2014	3735	1648	3139	1555	1733	777	700	67.	.22
20	25	2	2838		1922	2746	1556	2354	1611	1733	555	995	.53	.26
21	29	9	3204		2472	3296	1464	2197	1166	2200	777	400	.36	.30
22	33	9	3021		2014	2856	1556	2040	1277	1600	999	997	.22	.26
23	37	0	4303		4211	4394	2288	2511	1722	2400	888	007	.22	.26
77	17	9	2380		2197	2307	1007	1412	1111	1133	388	266	.13	.20

TABLE IX (Continued)
VOYÀGE 04 EASTBOUND
TAPE 22 RECONDER #2

Sheet 2 of 8

(pst)
VALUE
SIGNAL
PEAK-TO-TROUGH
MAXIMUM

"B" MODE

Index	Interval	Sea												
No.	No.	State	AR, A	AR, B	ARIC	AR2A	AR2B	AR2C	AR3A	AR3B	AR3C	AR4A	AR, B	AR,C
1	2	7	1896	4015	1003	2141	826	903	2788	1338	557	1873	699	699
7	9	9	4015	8030	1896	3346	1535	1806	4572	2409	1003	3078	1115	936
3	10	4	8030	11242	3457	5755	2598	3513	7361	4015	1673	5353	1673	1606
4	14	9	10038	12447	4349	8298	3306	5019	10595	5487	2007	7896	2453	2409
2	18	7	12491	14990	5799	11777	5904	8130	10939	9770	2899	10305	3234	2944
9	22	00	12268	18336	6022	10439	4723	6926	12268	8164	2788	11242	3680	3613
1	26	7	6134	12580	2788	5353	2361	3011	6915	3747	1449	4818	1673	1606
00	30	7	8699	13380	3011	8164	3542	4316	10818	5353	1673	6825	2007	2007
6	34	9	6468	11644	2899	7093	2716	2911	9368	4684	1338	6424	2007	1873
10	38	7	6580	11777	2230	5219	2598	2107	6692	3747	1338	5487	1673	1606
11	42	7	5799	7066	2565	6290	2598	3513	7807	4282	1003	4282	1338	1338
12	97	9	6692	10439	2230	4684	2243	3412	5911	3346	1449	3613	1338	1472
13	20	5	6245	12045	2788	6695	2479	3714	7807	7897	1561	3747	1784	1338
														-
						TAP	TAPE 24 R	RECORDER	#2					
14	2	2	5793	8030	2565	5755	2119	2868	7138	3747	1226	4416	1449	1472
15	9	2	5688	10573	3011	5353	2119	3346	6245	3613	1338	3078	1561	1472
16	10	S	6357	10573	2342	5621	1896	2294	6692	3613	1449	4282	1338	1472
11	14	2	7897	8967	2788	5353	2119	3250	6022	3479	1115	3479	1115	1333
18	18	4	3680	8298	2230	5487	1561	2581	6692	3613	1115	3078	892	936
19	22	7	3792	5219	1449	3479	1449	2007	4126	2007	699	2275	892	803
50	26	2	4238	6156	1784	4684	1673	2294	5799	3212	892	2676	893.	936
21	30	9	3457	6424	1784	4282	1784	2485	5019	2944	780	2542	780	803
22	34	9	2788	6022	1449	3479	1449	2007	4126	2275	699	1873	780	803
23	38	2	7687	7227	2342	5085	2230	3059	6022	3479	892	2409	1003	803
24	42	9	2453	4952	892	2944	1226	1338	3680	1873	699	2275	699	803

TABLE IX (Continued)
VOYAGE 04 EASTROUND
TAPE 22 RECORDIN #2

Sheet 3 of 8

No. State R ₁	"5 _"	" MODE				MAXIMU	MAXIMUM PEAK-TO-TROUGH SIGNAL VALUE (pst)	-TROUGH	SIGNAL VA	LUE (pst	•				
1	Index No.	Interval No.	Sea	RIA	8,3	R1C	R2A	R ₂ B	R2C	R3A	R 3.8	R3C	RA	R, B	R,C
1	1	3	7	2342	1338	557	2141	1417	502		803	699	1204	780	535
11	2	7	3	2899	1738	699	4015	2834	602		1338	1003	1606	1115-	803
15	2	11	4	4507	2676	892	8565	6022	903	1	2810	1673	3212	1338	1070
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4	15	9	9034	4282	1561	13517	8857	1606	8922	4149	2453	5621	2453	1739
23 8 10372 5487 1896 14856 10864 1706 9034 4818 131	2	19	7	9480	6717	1784	11911	8975	1606	8922	4282	2676	5353	2453	1739
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	9	23	80	10372	5487	1896	14856	10864	1706	9034	4818	3122	6825	3011	2275
31 7 9926 4952 1449 12714 8857 1806 7026 4015 $\frac{1}{3}$ 56 9257 3831 1226 96.36 7203 1505 5465 3078 $\frac{1}{3}$ 57 1896 936 1784 1606 2598 1204 3346 5353 47 1896 936 2109 1739 3306 1003 2899 4818 $\frac{1}{3}$ 7 1896 936 2107 1472 3306 1003 2899 4818 $\frac{1}{3}$ 7 1896 936 2007 1472 3306 1003 3346 5755 $\frac{1}{3}$ 7 1894 803 2230 1873 3122 956 2899 4684 $\frac{1}{3}$ 7 184 803 2230 1873 3122 956 2899 4684 $\frac{1}{3}$ 7 1561 936 1286 1070 2342 1051 3234 6022 $\frac{1}{3}$ 7 1561 936 1226 1070 2119 860 $\frac{1}{3}$ 803 163 803 1895 1561 $\frac{1}{3}$ 803 1895 $\frac{1}{3}$ 803 1896 $\frac{1}{3}$ 803 1896 $\frac{1}{3}$ 803 1896 803 1561 $\frac{1}{3}$ 803 1896 803 1561 $\frac{1}{3}$ 803 1896 803 1561 $\frac{1}{3}$ 803 1896 803 1561 $\frac{1}{3}$ 803 1896 803 1896 $\frac{1}{3}$ 8040 803 1896 803 1896 $\frac{1}{3}$ 8040 803 1896 803 1896 803 1896 $\frac{1}{3}$ 8040 803 1896 803 1898 803 1898 803 1898 803 1898 803 1898 803 1898 803 1898 803 1898 803 1898 803 1898	7	27	7	12268	4952	1449	13250	2776	2007	6915	4149	3569	5487	2342	1739
35 6 9257 3831 1226 9636 7203 1505 5465 3078 85.4	60	31	7	9926	4952	1449	12714	8857	1806	7026	4015	2788	4550	2119	1739
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	6	35	9	9257	3831	1226	9636	7203	1505	2465	3078	2565	3747	1784	1472
39 7 1561 936 1784 1606 2598 1204 3346 5353 43 7 1896 936 2119 1739 3306 1003 2899 4952 51 5 1896 1070 2230 2007 3306 1003 3346 5755 3 5 1784 803 2230 1873 3122 956 2899 4684 7 5 1561 936 1896 1472 2342 1051 3234 6022 11 5 138 803 2896 1896 1472 2342 1051 3234 6022 15 5 1561 936 138 810 810 4128 8126 1070 8126 2899 4684 15 5 1338 803 669 803 1671 764 2840 15 5 1338 803 803 <t< td=""><td></td><td></td><td></td><td>RSA.</td><td>RSB</td><td>RSC</td><td>ReA</td><td>ReB</td><td>R, C</td><td>RyA</td><td>R, B</td><td>R,C</td><td>RRA</td><td>80 00 00</td><td>R₈C</td></t<>				RSA.	RSB	RSC	ReA	ReB	R, C	RyA	R, B	R,C	RRA	80 00 00	R ₈ C
43 7 1896 936 2119 1739 3306 1003 2899 4952 51 5 1896 1070 2230 1472 3306 1003 2899 4818 51 1896 1070 2230 1873 3122 956 2899 4684 7 5 1561 936 1896 1472 2342 1051 3234 6022 11 5 1561 936 138 803 1673 764 - 2810 15 5 1561 936 138 803 1673 764 - 2810 19 4 1338 803 893 1693 1673 764 - 2810 23 4 1338 803 892 803 1896 764 - 2409 15 5 1338 803 892 803 1896 764 - 2409	10	39	7	1561	936	1784	1606	2598	1204	3346	5353	1784	4416	2565	1338
\$ 1896 936 2007 1472 3306 1204 2899 4818 1896 1070 2220 2007 3306 1003 3346 5755 1896 1070 2220 2007 2007 3306 1003 3346 5755 2899 4884 2899 4884 2899 2230 1873 3122 956 2899 4684 2899 4884 2899 2230 2342 2	11	43	7	1896	936	2119	1739	3306	1003	2899	4952	2007	3613	2342	1204
51 5 1896 1070 2230 2007 3306 1003 3346 5755 TAPE 24 RECORDER #2 3 5 1784 803 2230 1873 3122 956 2899 4684 7 5 1561 936 1896 1472 2342 1051 3234 6022 11 5 1338 936 1226 1070 2119 860 - 2810 19 4 1338 803 803 1896 764 - 3078 23 4 1338 803 869 803 1561 573 - 2676 35 6 1449 1070 669 803 2007 573 - 2676 39 5 1896 936 669 803 2007 573 - 2676 43 6 1226 669 669 803 1338 573 1115 2007	12	47	9	1896	936	2007	1472	3306	1204	2899	4818	2230	4416	2899	1338
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	13	51	8	1896	1070	2230	2002	3306	1003	3346	5755	1784	4952	2342	1204
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								1	NUER #2						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	9	5	1784	803	2230	1873	3122	956	2899	7897	1896	3881	2230	1070
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	1	S	1561	936	1896	1472	2342	1051	3234	6022	1673	4416	2453	1070
11 5 1338 936 1338 803 1673 764 - 3346 155 5 1561 936 1226 1070 2119 860 - 2810 199 4 1338 1204 1003 803 1896 764 - 3078 23 4 1338 803 669 803 1561 573 - 2409 23 24 2409 23 24 24 24 24 24 24 24				R10A	R10B	R10C	R11A	R11 B	RIIC	R12A	R ₁₂ B	R ₁₂ C	R13A	R13B	R,3C
15 5 1561 936 1226 1070 2119 860 - 2810 23 4 1338 1204 1003 803 1896 764 - 3078 27 4 1338 803 699 803 1561 573 - 2542 31 6 1561 1070 669 803 1784 573 - 2409 35 6 1449 1070 780 803 1673 669 2676 39 5 1896 936 1226 936 2676 699 1226 2944 43 6 1226 669 669 803 1338 573 1115 2007	16	11	2	1338	936	1338	803	1673	764		3346	11115	3747	11115	1070
19 4 1338 1204 1003 803 1896 764 - 3078 23 4 1338 803 669 803 1561 573 - 242 27 5 1338 803 892 803 1784 573 - 2409 35 6 1561 1070 669 803 1673 669 - 2676 39 5 1896 936 1226 936 2676 694 1226 699 1226 2944 43 6 1226 669 669 803 1338 573 1115 2007	17	15	2	1561	936	1226	1070	2119	860		2810	1226	3747	1226	1070
23 4 1338 803 669 803 1561 573 2542 27 5 1338 803 892 803 1784 573 2409 31 6 1561 1070 669 803 2007 573 2676 35 6 1449 1070 780 803 1673 669 2676 39 5 1896 936 1226 936 1226 669 803 1338 573 1115 2007	18	19	7	1338	1204	1003	803	1896	764	1	3078	892	4282	1003	1070
27 5 1338 803 892 803 1784 573 - 2409 31 6 1561 1070 669 803 2007 573 - 2676 35 6 1449 1070 780 803 1673 669 1226 2810 39 5 1896 936 1226 936 1326 2944 43 6 1276 669 669 803 1338 573 1115 2007	19	23	4	1338	803	699	803	1561	573		2542	892	2810	1003	699
31 6 1561 1070 669 803 2007 573 - 2676 35 6 1449 1070 780 803 1673 669 - 2810 39 5 1896 936 1226 936 2676 669 1226 2944 43 6 1276 669 669 803 1338 573 1115 2007	20	27	S	1338	803	892	803	1784	573	,	5409	1338	2810	892	803
35 6 1449 1070 780 803 1673 669 – 2810 39 5 1896 936 1226 936 2676 669 1226 2944 43 6 1276 669 669 803 1338 573 1115 2007	21	31	9	1561	1070	699	803	2007	573		2676	1226	2409	1003	699
39 5 1896 936 1226 936 2676 669 1226 2944 43 6 1276 669 669 803 1338 573 1115 2007	22	35	9	1449	1070	780	803	1673	699	1	2810	1115	2810	892	803
43 6 1276 669 669 803 1338 573 1115 2007	23	39	S	1896	936	1226	936	2676	699	1226	2944	1338	2676	1003	936
	24	43	9	1276	699	699	803	1338	573	1115	2007	1003	2810	699	803

TABLE IX (Continued)

VOYAGE 04 EASTBOUND TAPE 22 RECORDER #2

MAXIMUM PEAK-TO-TROUGH SIGNAL VALUE (ps1)

"D" MODE

Sheet 4 of 8

Index	Interval	Sea	. 0204	5000	-	7 0000			0 0000					
	.00.	1	1019-1	10101	1012-3	1653-4	TONS-I	16/15-2	TGMS-3	TGMS-4	TGAS-1	TGAS-2	TCAS-3	TGAS-4
-	4	7	2007	1873	11115	2007	2125	1806	1226	2409	11115	1070	1226	1472
7	80	3	5242	3881	1784	4149	3306	2810	1673	4282	2788	2275	2230	2810
3	12	7	5353	5487	3011	7361	6022	4416	3346	6669	3792	3212	2788	6015
4	16	9	6692	9502	5576	12045	8620	6825	5019	10841	6580	5353	4349	6156
~	20	7	9814	9101	3680	12714	8575	6022	4684	9636	8141	6558	4572	6569
9	24	00	14945	7066	6468	13785	12399	8030	5799	11510	7584	6022	4907	6989
1	28	7	11153	8833	4684	10305	7794	5420	3903	7495	5019	4015	4015	5755
00	32	7	8365	5621	4126	8030	6495	4215	3346	6692	3903	2944	2788	2944
0	36	9	7361	4952	3011	6569	7321	4316	3792	7628	3349	3078	2676	3613
			HLSS-1	HLSS-2	HLSS-3	HLSS-4	TCNS-1X	TGMS-2X	TGMS-3X	TGMS-4X				
10	07	7	3011	3881	3234	4282	2834	803	780	1070	2899	2810	34.57	4684
11	777	7	3903	4884	3903	4952	2834	803	892	1070	4238	3212	3569	7684
12	84	9	3792	4550	3680	4282	3138	803	1003	803	5576	4282	3569	5487
13	22	S	2899	4149	3792	7684	3070	803	892	1070	1975	4149	3680	5353
					7 1	TAPI	TAPE 24 RECORDER #2	DER #2						
14	4	2	3011	3747	3680	3881	3457	764	892	936	3792	3212	2453	3479
15	80	5	3346	4149	7461	4416	3569	699	892	936	3569	3747	3011	4149
			TGFS-1	TGFS-2	TGFS-3	TGFS-4	TGSS-1X	TGSS-2X	TGSS-3X	TGSS-4X				
16	12	2	7138	5888	3011	7093	1277	1714	1388	2133	5242	4149	3569	5487
17	16	2	7138	4416	2768	6022	1166	1285	1055	1933	3903	3212	2342	3747
18	20	4	6803	4684	2899	5888	1338	1285	888	2066	2565	2007	2342	3212
19	24	4	6803	4818	2788	6022	1055	1142	576	1666	2565	2542	1896	2944
20	28	S	5019	4550	3234	6669	1166	857	833	1866	2676	3346	1784	2409
21	32	9	5638	3747	3122	6692	1333	857	576	2133	3680	2810	1896	3078
22	36	9	6468	4282	2899	6290	1166	714	777	2000	2899	2141	1561	2141
23	07	5	5465	3613	2788	5888	1166	999	833	2000	3903	2810	1449	2676
24	77	4	8267	2011	2110	1,60%								

TABLE IX (Continued)
voyace 04 WESTBOUND
TAPE 26 RECORDER #2

"A" MODE	35				A.M.	MALMUM PEAK-10-IRCOUR SIGNAL VALUE (PSI)	TOT-V	1000	TOTAL THE	1-11		Contract of the last of the la		
Index	Interval	Sea											END HOUSE	(G's)
No.	No.		LSTS	LSMS	LSBS	LSTP	LSMP	LSBP	SAP	SAS	BGST	BGSB	VERTICAL	TRANS.
-	1	7	1854	629	732	1098	079	863	555	999	222	200	.13	.10
7	2	7	3399	1867	1464	3076	1464	3060	1666	1400	999	700	.18	.18
3	6	89	5974	2746	1831	4724	2380	4708	2388	2333	611	888	67.	.16
4	13	6	16995	3076	9338	16919	2472	7847	7777	8399	1111	1066	1.07	.18
2	17	10	20806	5273	11261	17249	4852	8240	7777	6668	1555	1466	1.20	.30
9	21	10	16583	7567	10712	16809	6997	9181	7222	9996	1611	1133	.93	.36
1	25	10	17510	4724	13550	16919	3936	8318	8611	8999	1777	666	1.20	.30
00	29	10	15141	3735	10528	17029	4028	8867	6722	8466	1388	1133	1.11	.28
6	33	6	10815	4384	1599	11755	4120	5100	4388	5599	1333	866	.89	.30
10	37	2	7906	4384	8972	12854	4120	6748	5277	5733	1722	566	.98	.34
11	17	4	7416	3296	45.77	7141	2563	2982	3111	3666	833	733	.80	.30
12	45	S	3914	2966	3662	4284	2197	3060	1944	1933	777	995	.53	77.
13	67	7	5562	3735	5676	6921	2929	4080	2611	3000	1111	599	*/*	09.
14	53	7	6386	5493	6317	. 9887	3753	5493	3222	3333	1722	999	67.	06.
15	57	80	5768	3296	5493	8459	2838	4551	3333	3600	776	599	.53	.62
9	19	1	9699	4204	6042	9338	3479	4002	3388	3600	1111	865	07.	.52
17	65	1	7107	3186	4760	7800	2563	2100	3666	2600	1000	999	.27	.56
							TAPE 28	RECORDER	R #2					
80	1	1	6500	3405	5035	7622	3112	3221	2777	3333	1055	599	.22	.42
61	2	7	5765	2417	3662	7416	1831	2254	3277	3666	722	533	.13	97.
20	6	7	6134	4724	4028	4738	3753	6367	3055	3466	1055	999	67.	07.
21	13	2	11352	5163	4028	9476	3622	6891	5111	5133	1000	1133	.80	.36
22	17	4	8056	3625	6408	7906	2838	5168	3777	4600	1222	1133	.58	.36
23	21	9	6225	2746	4303	7210	2380	3071	2555	2666	1111	533	.58	07.
54	25	7	4577	2966	2746	4429	2014	2621	2555	2600	833	665	77.	.38
25	29	6	6266	3515	5676	9682	2929	5693	5555	6199	1277	1200	.27	.54
56	33	6	10437	4065	7599	13493	3753	5618	6111	9999	1777	1133	67.	. 99.
27	37	10	6266	6152	8972	12669	5035	7715	6055	6733	1888	999	67.	76.
23	41	10	6266	5163	0692	15450	2288	6891	5666	6333	1277	666	.53	.68
29	45	10	5493	4504	6042	8034	1648	7677	3333	0005	1333	533	.53	. 52
30	67	80	3479	3296	3845	4635	3570	2322	1277	2333	888	533	.31	.28
31	53	s	3021	2197	2288	2575	3936	1573	888	1333	555	700	.22	.24
32	57	2	1,556	1648	1281	1339	1007	1348	833	666	388	995	.22	.24

TABLE IX (Continued)
VOYAGE 04 WESTBOUND
TAPE 26 RECORDER #2

"B" MODE	30				MAX	MAXIMUM PEAK-TO-TROUG	TO-TROUG	H SIGNAL	SIGNAL VALUE ((pst)				Sheet 6 of
Index	Interval	Sea												
No.	No.	State	AR, A	AR B	AR, C	AR2A	AR ₂ B	AR2C	AR3A	AR3B	AR3C .	AR4A	AR, B	AR4C
-	7	7	1380	2275	699	1070	557	573	1338	803	334	752	977	401
~	0	7	4391	6424	1673	3747	1449	1912	4238	2542	892	2509	780	936
2	10	80	4015	7351	1673	2676	11115	1720	3569	2007	892	2258	699	803
*	14	6	15809	22083	3457	15391	6468	7074	15057	10707	2788	12547	4461	4015
2	18	10	14555	22217	4349	16462	7138	6883	18291	11510	2342	12296	4572	3881
9	22	10	12547	21146	4461	17131	7361	6883	18403	12045	2453	11920	4238	3479
1	56	10	14304	22227	3457	16328	8365	8317	18960	13651	2230	11543	3903	3747
00	30	10	11794	20511	3346	15926	6803	7074	18626	10974	2342	12171	4349	3747
6	34	6	12672	16691	3234	16462	7026	6022	18960	11108	1673	10665	3569	3479
10	38	2	7020	13517	3011	12447	4684	4588	16395	8565	1226	7653	2788	2542
11	42	4	6022	10573	2342	6558	2788	3250	8030	4550	1338	3387	1226	1204
12	97	2	9495	9234	2565	5621	2230	3346	7138	3881	1226	3136	1338	1204
13	20	7	8155	14187	3011	6558	2899	3919	8365	4952	1673	4642	1673	1472
14	54	7	1069	12045	3122	7361	3122	4302	9257	5353	1449	4391	1561	1606
15	58	00	7062	15257	4126	8030	3680	4971	10484	5621	1896	4642	1449	1472
16	62	7	1030	13651	2899	6692	3122	4397	9480	4684	1784	4642	1673	1338
17	99	1	80	15123	3903	7093	3346	3537	8922	7495	1561	4893	4572	1739
						TAPE	28	RECORDER #	2					
18	2	1	6803	15793	3457	7152	3346	4380	9480	5353	1673	4391	6771	1472
19	9	1	1	1	1	1	1	ı		1				
20	10	7	0876	20879	4572	7277	3346	6022	9368	5219	2230	5395	1673	1739
21	14	2	8141	17666	3346	8155	3346	3741	11487	6022	1561	6148	2119	2007
22	18	7	9034	16060	4015	7528	3346	5110	9591	5219	1673	5144	1784	1472
23	22	3	5242	10573	2565	2646	2565	2920	7918	4149	1226	3889	1561	1070
24	26	7	4238	8565	2453	4266	1673	2098	5799	2810	1115	3011	11115	1070
25	30	6	8698	18202	4461	8281	3680	5110	10038	6022	2342	5897	2007	2007
56	34	6	11934	23957	5353	12547	4907	5292	17399	9368	2453	9159	2788	3078
27	38	10	12603	23020	4572	12045	5576	6387	16395	8164	2676	7904	3122	2944
28	42	10	11487	22083	4572	11669	2565	4197	15280	8565	1896	5897	2565	2007
53	95	10	7918	17533	4461	7403	1338	4927	11153	5888	1561	4768	1561	1338
30	20	80	4795	9770	2342	5019	4349	3376	6134	3881	1226	2007	1338	936
31	54	S	2565	6022	1226	2634	3903	1551	3122	2007	892	1505	780	803
32	58	~	1673	3346	892	1882	892	1186	2119	1472	699	1505	699	699
-	-					-	1							

TABLE IX (Continued)
VOYAGE 04 WESTBOUND
TAPE 26 RECORDER #2

Index	Interval	Sea												
No.	No.	State	RIA	RB	RIC	R2A	R2 B	R2C	R ₃ A	R ₃ B	R3C	RA	R, B	278
1	3	7	3011	1204	446	2409	2119	573	1338	936	892	1254	699	535
2	7	7	4768	2007	892	4015	3680	926	2342	1472	1338	2509	1449	936
3	11	80	10038	7897	1338	9234	6357	1434	4795	2676	4015	4266	2330	1606
7	15	6	8406	2810	2007	9502	5799	2390	6915	2944	1896	5771	1896	2007
2	19	10	15558	8030	3457	12447	7807	3728	7472	3613	4795	6524	4015	5409
9	23	10	12547	6692	2230	11376	8253	2963	5465	3881	3903	6273	2899	2542
1	27	10	12547	5487	2119	12179	8141	2963	6468	3881	3346	6273	2119	2275
00	31	10	11041	4684	1896	9368	6915	2103	4907	3078	2565	4768	2342	1338
6	35	6	12672	5487	1784	10171	7695	2007	5353	3346	2453	4015	2119	1338
0	39	2	13927	5621	1449	12714	8588	1912	6915	4015	3346	4391	2342	1472
1	43	7	13551	5621	1449	13384	9034	1720	7026	4015	3346	4391	2565	1739
			R ₆ A	R B	Rec	RA	R ₇ B	R,C	RRA	RSB	Rec	RgA	RgB	RgC
2	47	5	2509	3881	1338	3747	6022	2390	3903	3346	1449	3513	2676	1204
13	51	7	3262	6825	1784	4684	7584	3250	5353	9175	1673	4015	3346	1338
7	55	7	2760	5487	1561	4684	6915	2868	5353	4015	1449	3513	3011	1070
5	59	80	2760	4952	1673	5755	8922	3346	5576	4282	1449	3136	2342	1204
9	63	1	2258	4416	1673	4015	6915	3154	3680	3212	1784	3513	2342	1070
1	67	1	2007	3881	1673	3881	8979	2676	4126	3212	1784	4266	2230	1739
						TAPE	28 REC	28 RECORDER #2						
18	3	1	2007	4550	1561	4015	8979	3011	4795	3346	1561	3513	2676	1338
			RITA	R, B	R, C	R, A	R, , B	RIC	RAZA	RIZB	RIJC	RICA	RILB	RICC
0	1	1					1	1					-	
0	11	1	1338	3747	1226	2007	3346	1277		1873	1784	5897	2007	2007
1	15	5	1449	2944	1561	2634	4349	1551	•	2275	2230	6775	1673	2275
22	19	4	1338	3078	1115	1756	3792	1733		1873	1673	3889	1226	1472
3	23	3	892	1873	699	1505	3346	1186	1	1204	1115	3262	1115	1338
7	27	1	1226	2944	1003	1882	4015	1551	5130	1338	1338	4893	1338	1338
2	31	6	1561	3078	1784	3136	6022	1916	8365	2275	2230	1069	1784	2275
9	24	6	1449	3487	2342	3638	7695	1825	9703	2810	2675	8030	2453	2676
1	39	10	1449	6692	2119	3387	6134	1916	9480	2676	2676	7403	3122	2676
00	43	10	1449	5085	1784	2509	3346	2463	8979	2141	2119	8019	2230	2141
	17	10	1115	4149	1115	2007	2119	2372	5242	1739	1115	4391	1784	1070
	51	80	1115	3346	780	1380	8199	1642	3457	1338	892	1882	1338	1070
	55	2	892	1873	557	1003	4126	1095	2230	916	800	1631	780 -	803
	**								000	200	200		200	

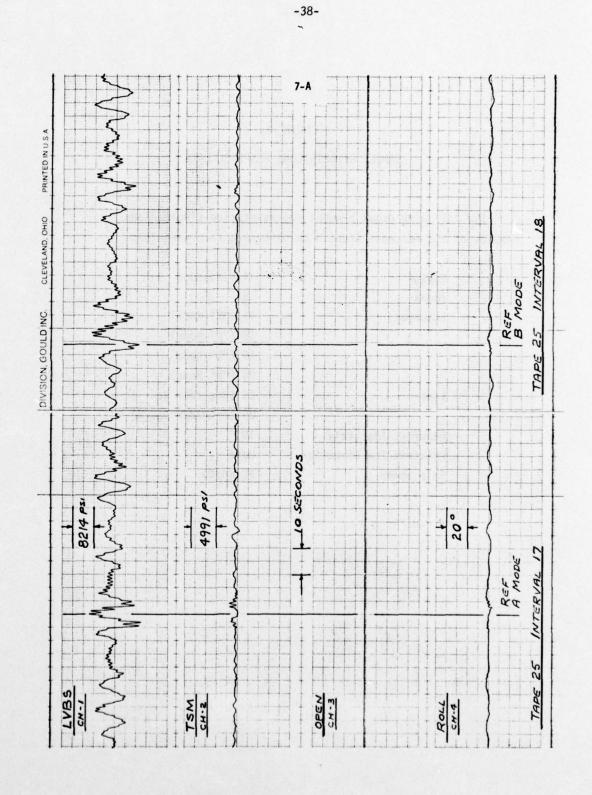
VOYAGE 04 WESTBOUND
TAPE 26 RECORDER #2 TABLE IX (Concluded)

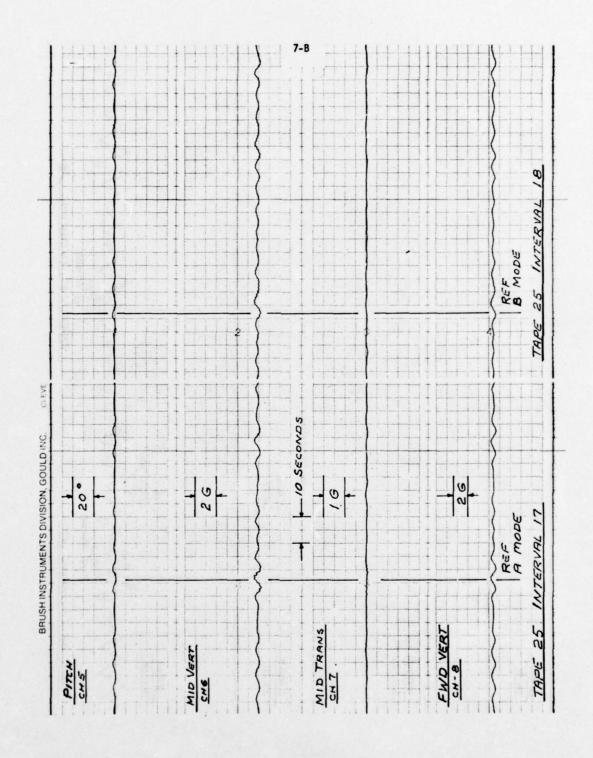
"D" MODE	30				MAXIMUM	PEAK-TO-TR	MAXIMUM PEAK-TO-TROUGH SIGNAL VALUE (psi)	. VALUE (p.	(15			S	Sheet 8 of	00
Index	Interval													
No.	No.	State	HLSS-1	HLSS-2	HLSS-3	HLSS-4	TCMS-1	TGMS-2	TCMS-3	TCMS-4	TGAS-1	TGAS-2	TGAS-3	TGAS-
-	7	7	1882	1606	1673	1739	2230	1720	1226	2676	1896	1631	0771	2676
7	00	1	3764	3212	3122	4416	7584	6309	4572	9368	5576	1627	3000	5755
2	12	80	3764	4952	4907	4550	6693	3824	2788	5255	4572	3513	2707	1037
4	16	6	6524	6558	5911	6699	9703	6883	6765	11108	4576	5570	2000	1001
5	20	10	7659	6693	6590	6000	19161	9655	7007	00000	200	2000	7700	1001
9	26	10	61/8	17.00	2009	7700	1577	2000	1001	10378	6250	6779	2709	1777
, ,		2.	0110	1433	5000	1000	1202/	9339	9409	13919	9/10	6273	5911	6569
	97	2	0717	2888	2465	4952	12491	7265	6022	13116	9591	1069	3792	6693
0	32	. 10	7528	10707	7249	7628	13941	9273	6915	15123	7249	6775	5576	149
6	36	6	3889	7762	8979	6290	10372	6118	8030	10305	0876	7152	7897	780
10	07	2	3638	5487	4349	4952	7918	5353	4126	8967	6915	7715	3457	200
11	77	7	3387	4952	3903	4416	5576	3824	3122	6558	6022	4140	2230	777
-													200	
1			TGFS-1	TGFS-2	TGFS-3	TGFS-4	TGMS-1X	TGMS-2X	TCMS-3X	3X TGMS-4X	X4-			
12	87	5	14555	8699	\$019	11376	3011	860	780	1070	6767	3613	27.63	33,
13	52	1	21958	13115	8141	15026	5277	986	1116	2001	6404	2000	5433	115
14	98	,	16060	10430	5700	13617	7570	220	500	1204	66/6	4391	2453	428
10	200		00001	10439	2039	1331/	4347	1511	768	10/01	3457	3262	2899	374
2:	00	10	16939	10439	6580	15257	1977	1147	1115	1338	6357	4517	2788	401
10	50	1	15057	10701	6022	14722	4126	1051	1115	1204	6692	4517	2899	7687
17	89	7	12547	8164	8019	11242	3680	926	1115	1204	5019	3513	2676	4282
E						TAPE 28	RECORDER	02						
18	7	7	11599	8565	7897	11041	3569	638	1115	936	4795	3011	2342	3613
-			HLSS-1	HLSS-2	HLSS-3	HLSS-4	TGSS-1X	TGSS-2X	X TGSS-3X	-3X TGSS-4X	-4X			
19	80	7	1	1	1	1	1	1	1	•	1	1		-
20	12	7	5019	6692	6357	6022	1722	1772	2111	3666	7026	4893	4572	6693
21	16	2	3680	5755	4572	5144	2277	2000	2333	3200	6693	4893	7027	6050
22	20	7	4126	5755	4349	4266	1888	1409	1555	3200	5353	4768	3657	SOBOS
23	24	3	2899	4952	3680	3513	1277	1500	1222	2000	42.67	3262	9976	70107
24	28	7	3234	4015	3792	3638	1333	1318	1888	2000	3603	2500	2230	3170
25	32	6	4461	7762	7695	4768	2722	1909	3000	7007	23.00	5067	5010	2017
26	36	6	6803	10305	8699	7152	2500	3181	2500	5466	22.49	5305	6136	8699
27	07	10	2692	11108	11153	7026	2333	2818	2611	5199	6134	6524	7472	10171
28	77	10	5576	8164	727.9	1069	1500	2045	2000	4466	7026	5019	3234	7227
53	78	10	6355	6424	5911	5395	1000	1863	1888	3933	5130	3764	2565	4282
30	52	00	3122	3881	2788	3011	2722	606	1166	2600	3680	3011	1673	3356
31	56	2	2007	2275	1449	1882	2222	757	722	1333	2230	2000	277	25.36
32	09	5	1115	1472	1784	1380	995	316	111	000	25.50	1000	655	0/07
			-	7/17	1017	1300	200	010	111	444	1001	7790	/80	1338

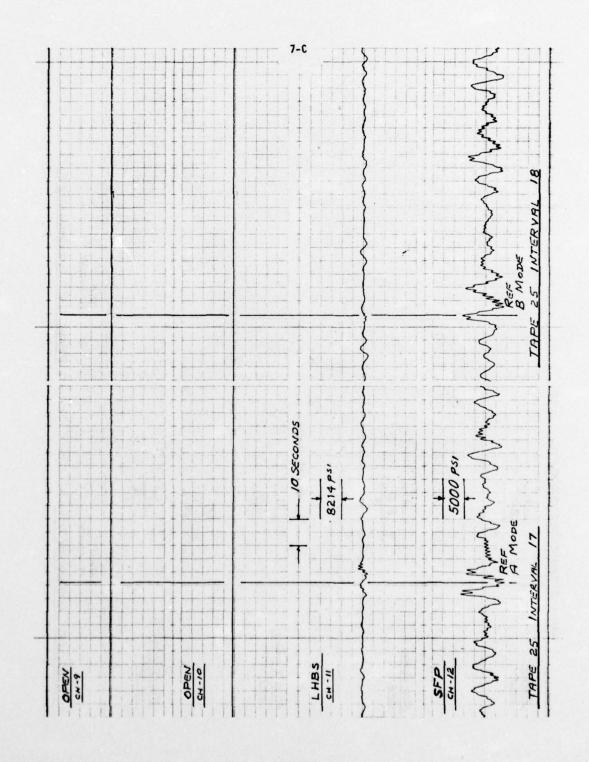
FIGURE 7 SAMPLE SIMULTANEOUS RESPONSE DATA

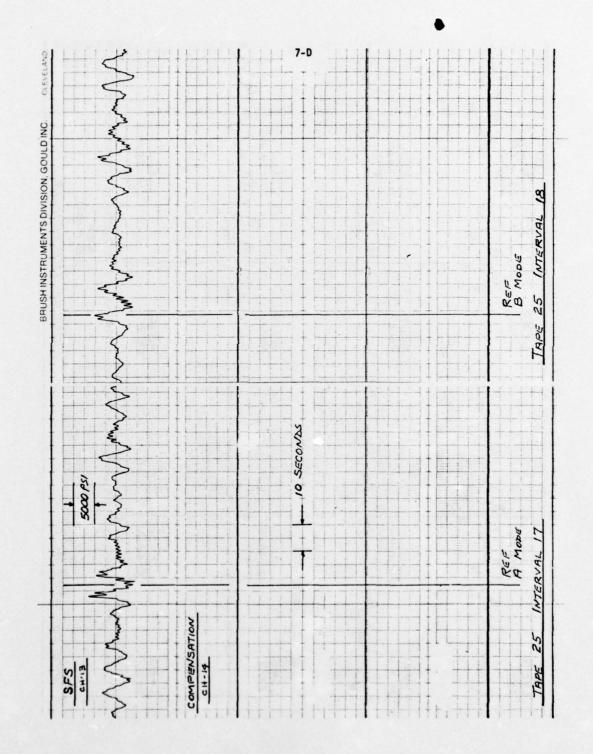
The following pages present representative simultaneous samples of all recorded signals on both tape recorders for:

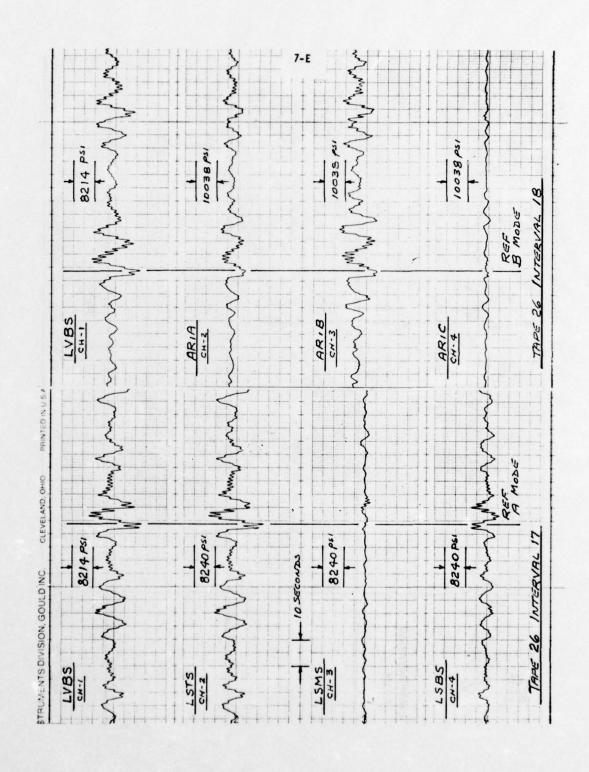
Voyage	4 Westbound
Index	5
Interval	17 ("A" Mode)
	18 ("B" Mode)
	19 ("C" Mode)
	20 ("D" Mode)
Tape	25 (Recorder No. 1)
	26 (Recorder No. 2)
Beaufort Sea State	10
Relative Sea Direction	Head
Ship Speed	22 Knots

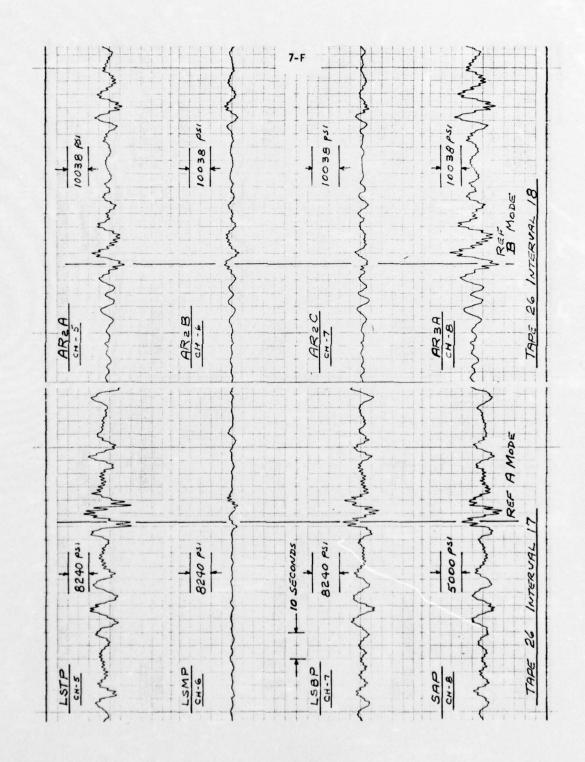


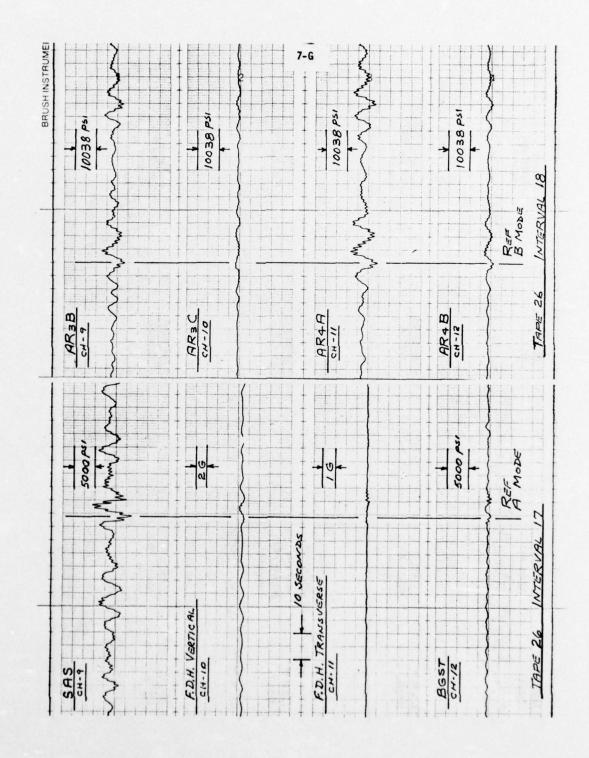


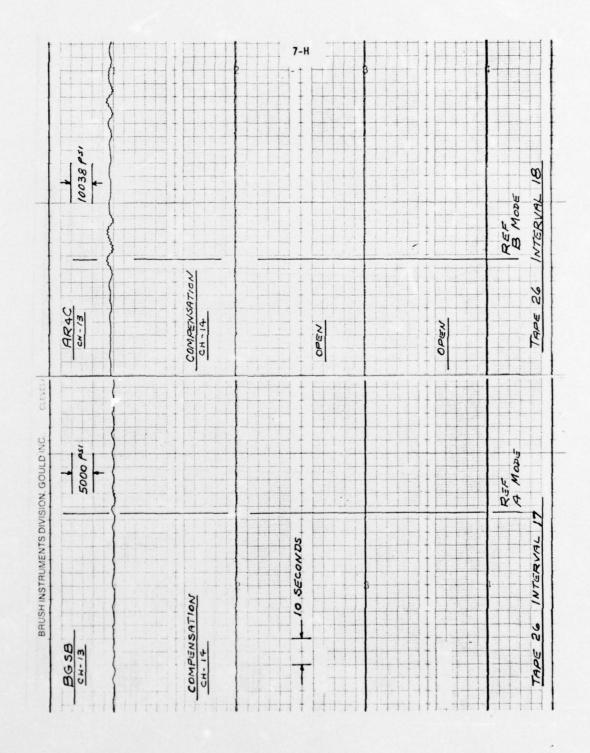


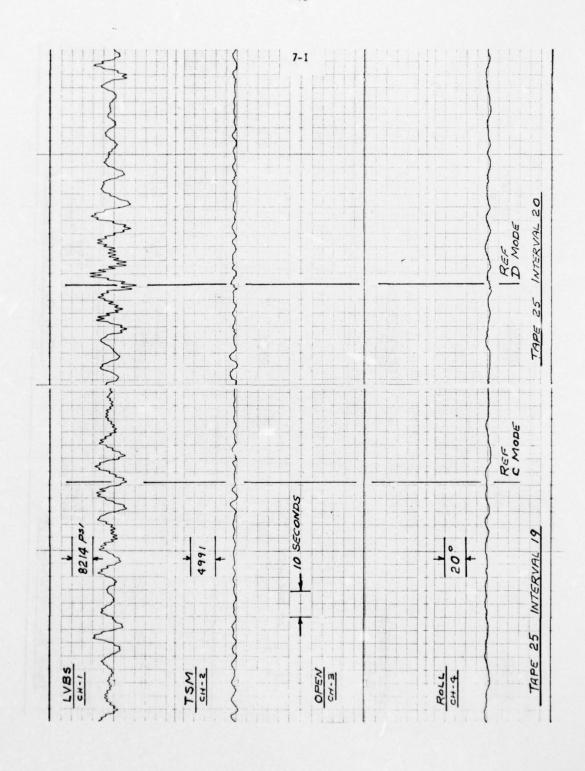


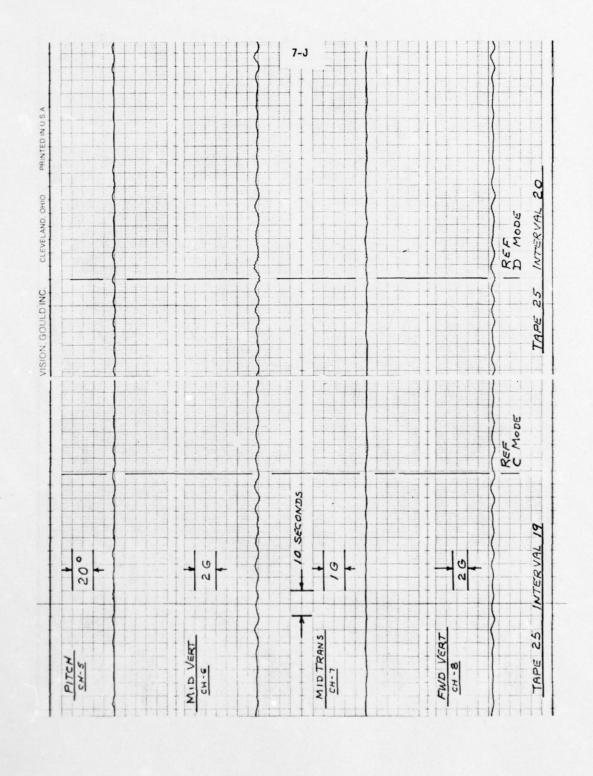


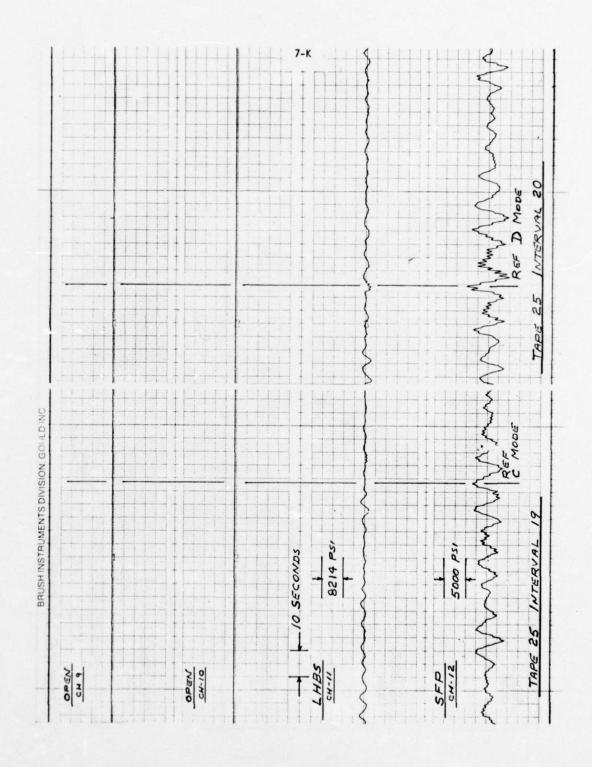


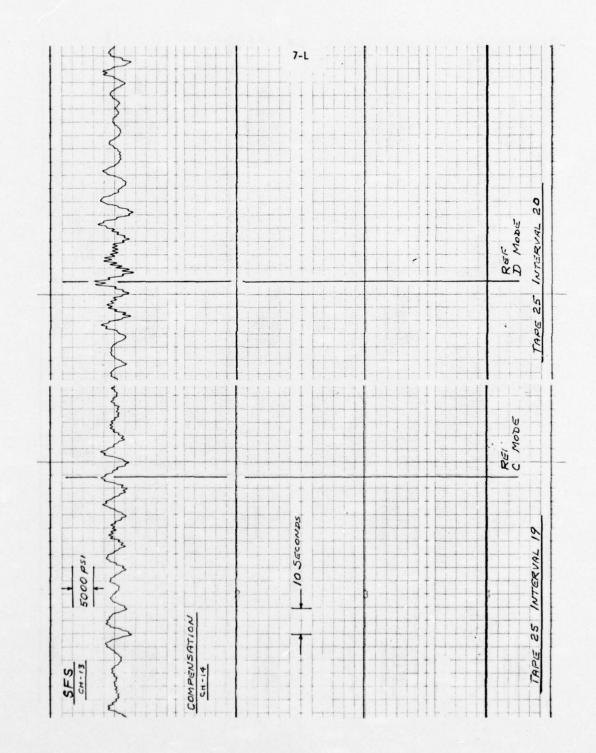


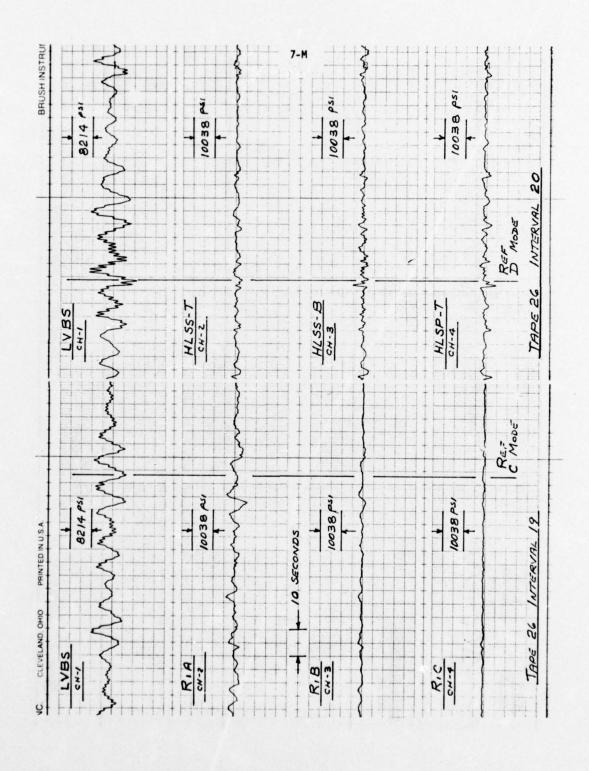


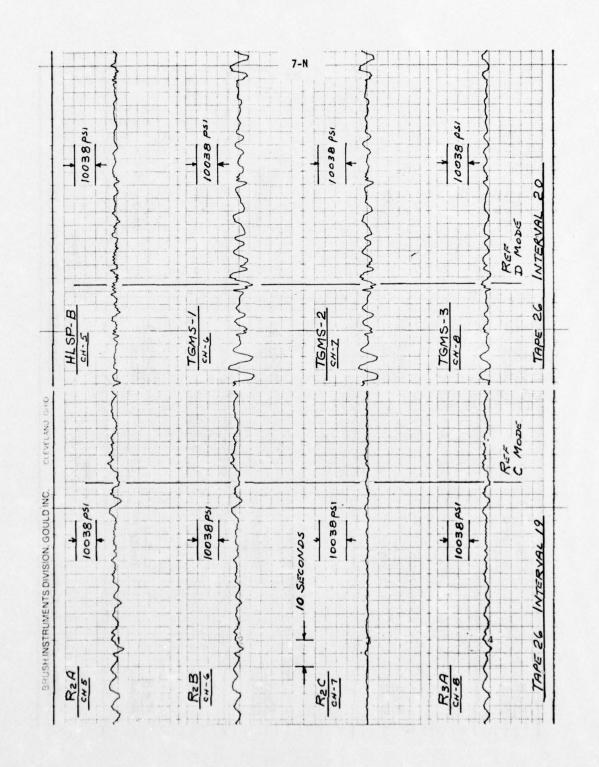


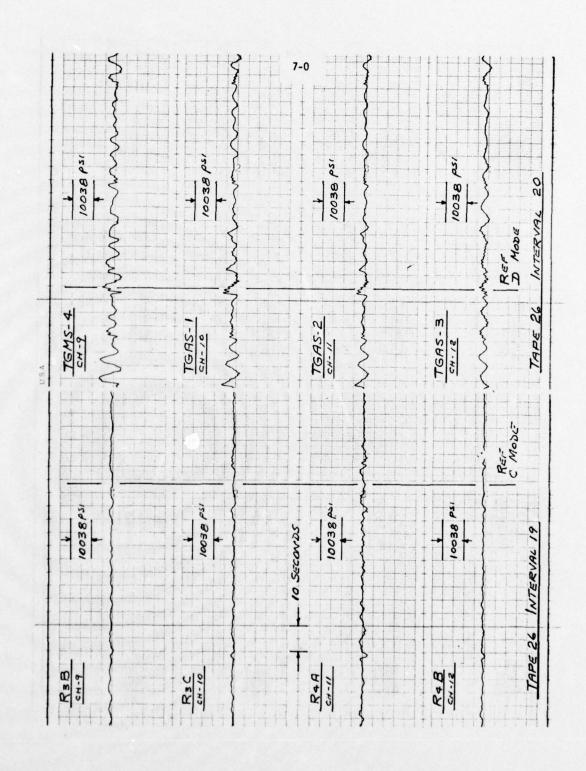












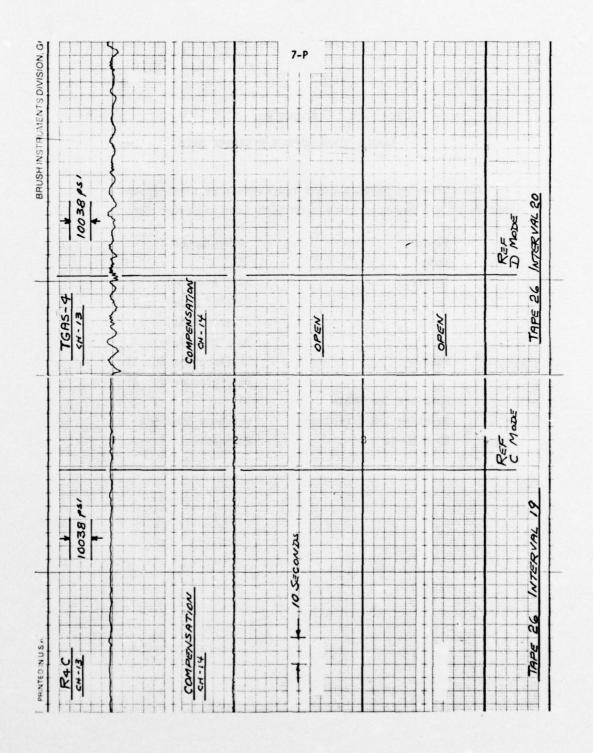
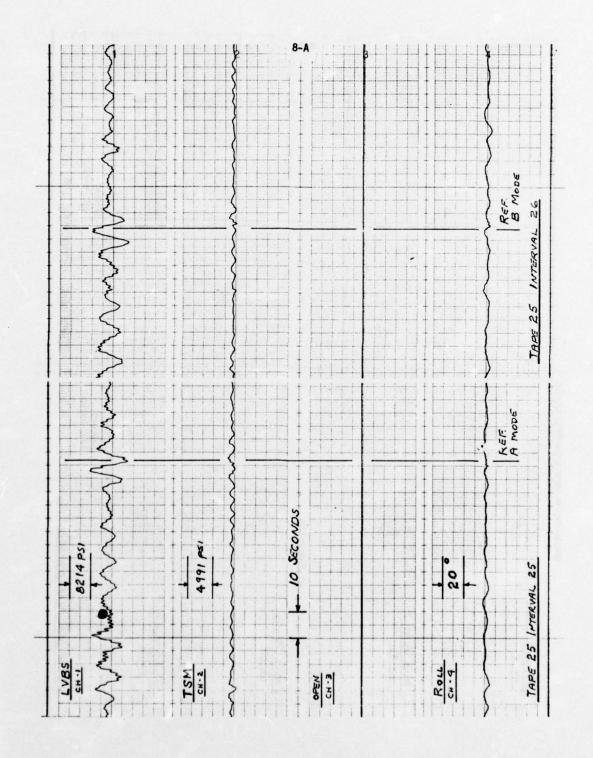


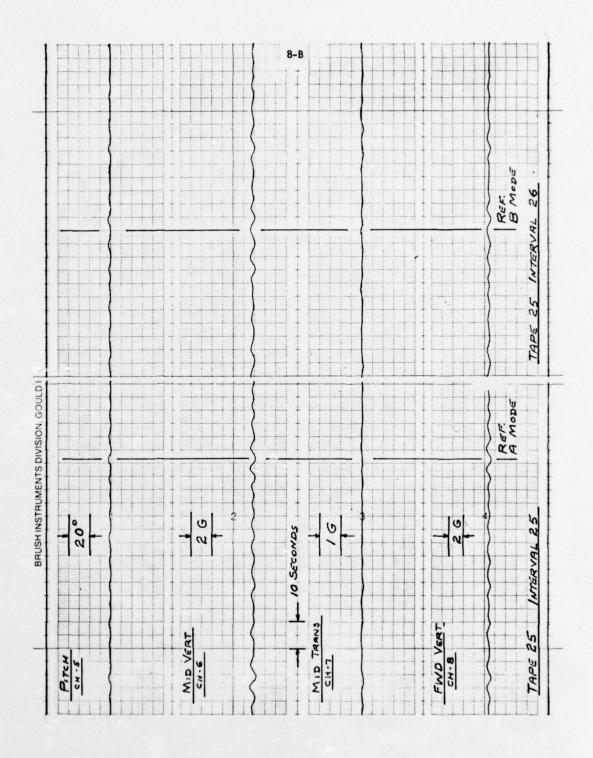
FIGURE 8

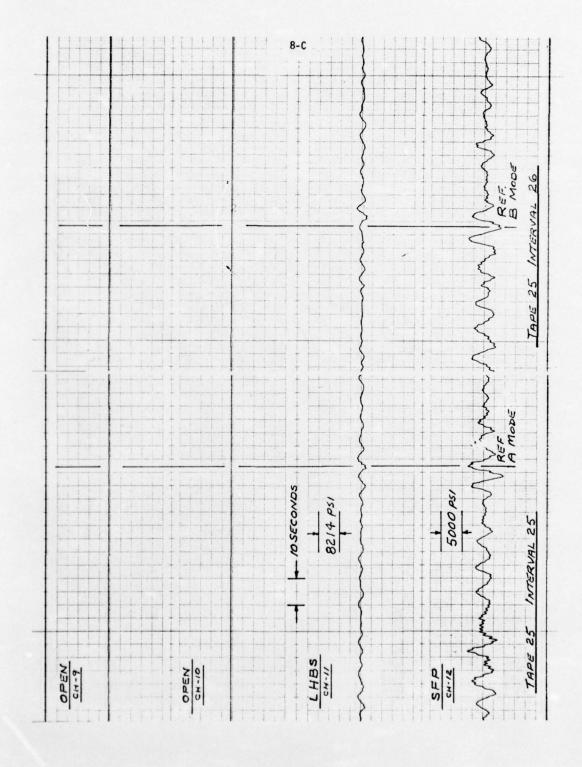
SAMPLE SIMULTANEOUS RESPONSE DATA

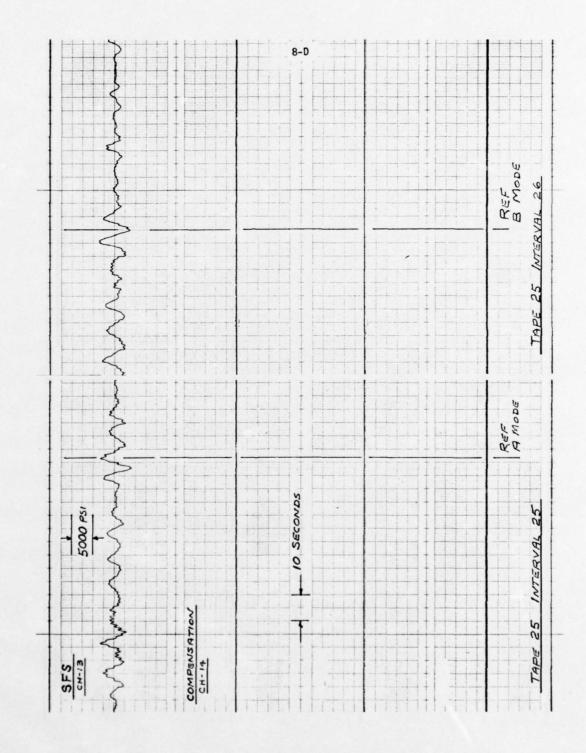
The following pages present representative simultaneous samples of all recorded signals on both tape recorders for:

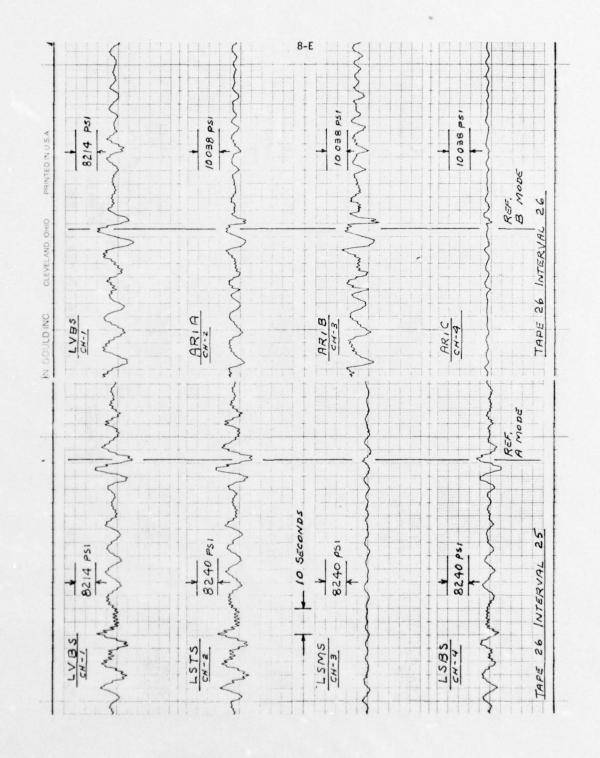
Voyage	4 Westbound
Index	7
Interval	25 ("A" Mode)
	26 ("B" Mode)
	27 ("C" Mode)
	28 ("D" Mode)
Tape	25 (Recorder No. 1)
	26 (Recorder No. 2)
Beaufort Sea State	10
Relative Sea Direction	Broad on Stbd Bow
Ship Speed	20 Knots

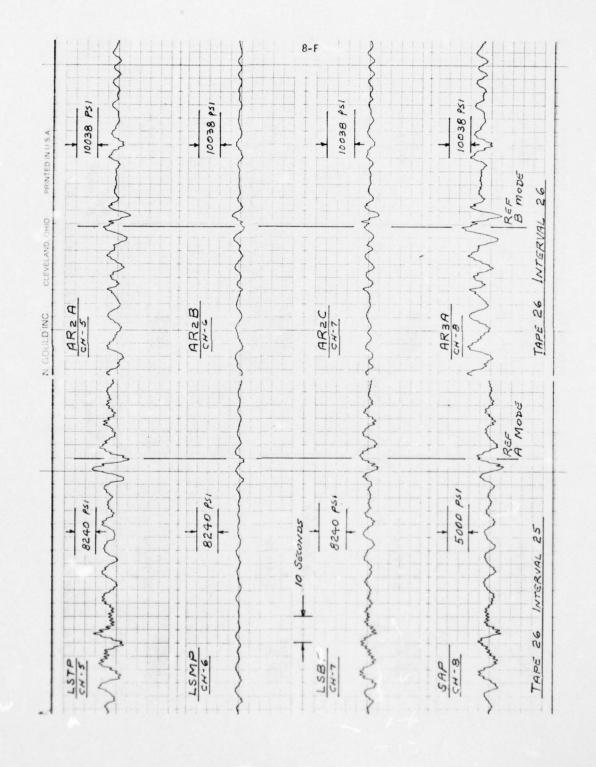


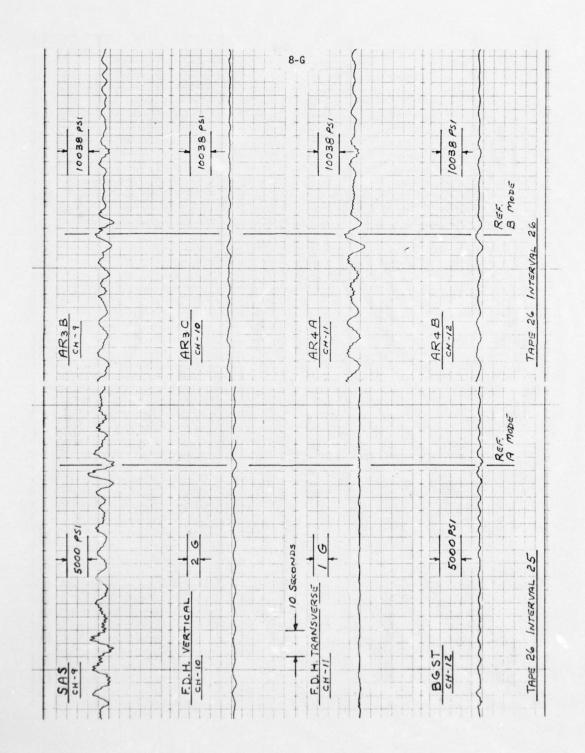




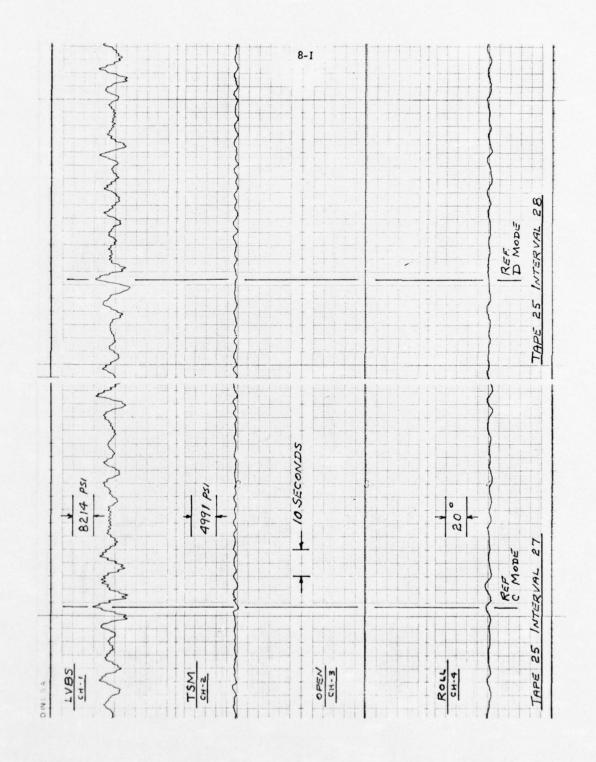


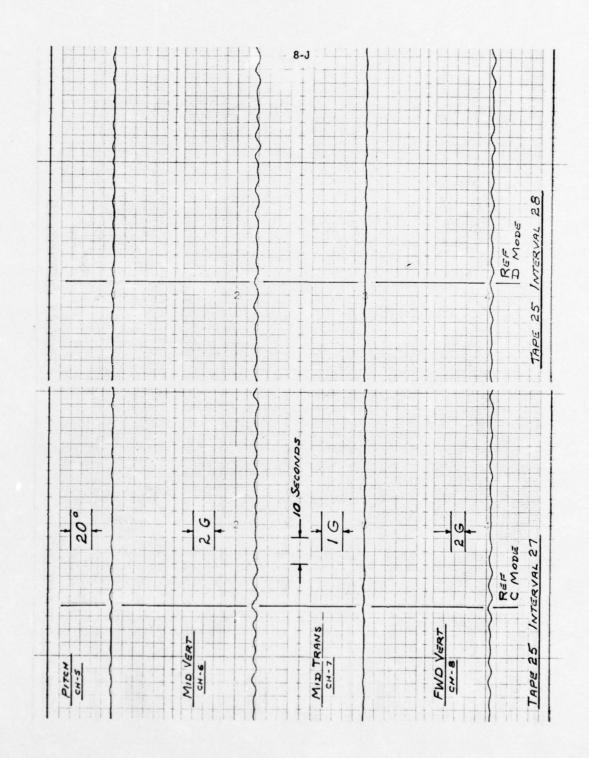


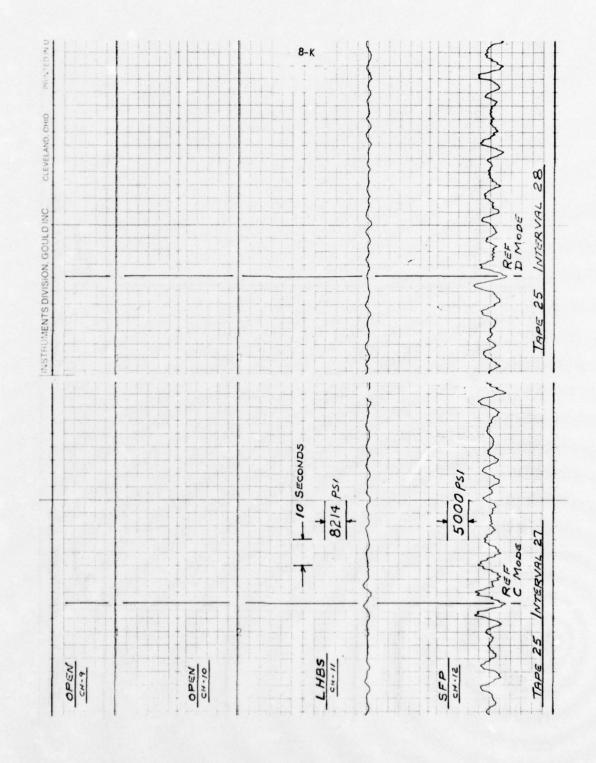


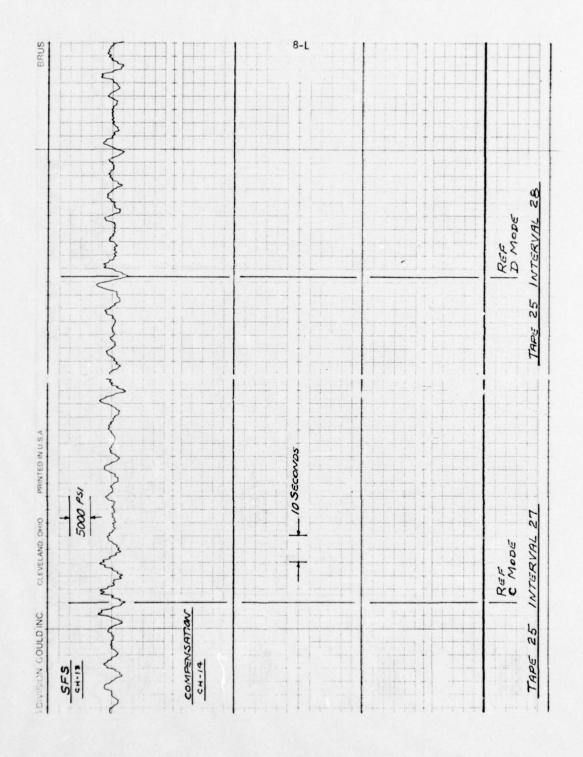


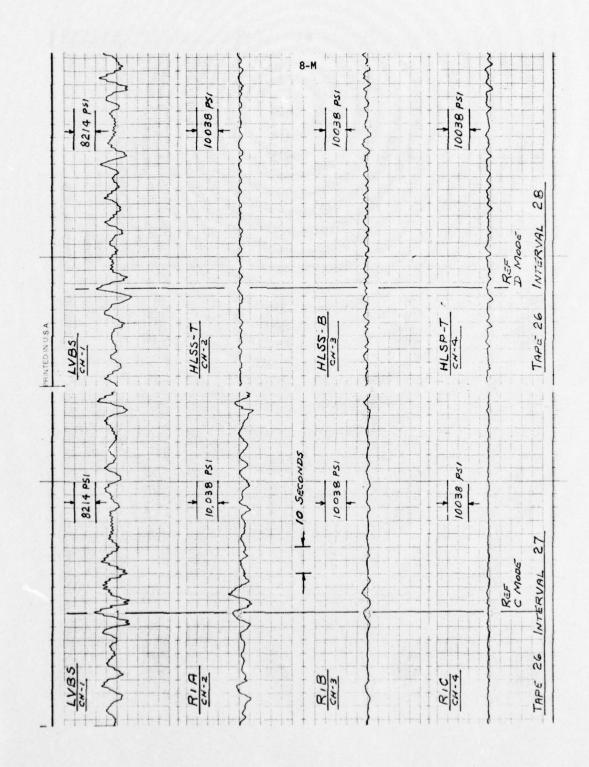
		8-н		
10038 PS/				REF. B Mode 26
	NoiTE			TAPE 26 INTERVAL
AR4 C	CMPENSATION	OPEN	OPEN	TAPE 26
				REF A Mode
\$000 Ps1		SONOS		25
	NOV	- 10 SECONDS		INTERVAL
BGSB	COMPENSATION CN-14	T		7APE 26

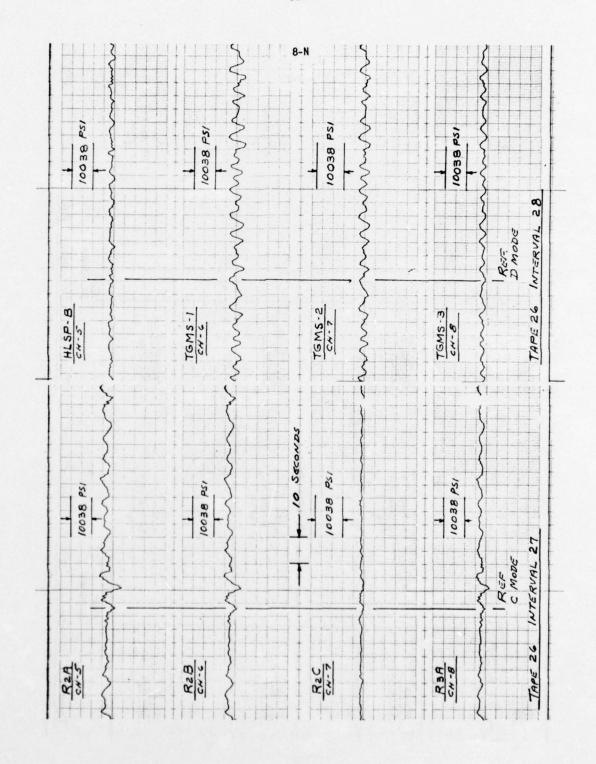


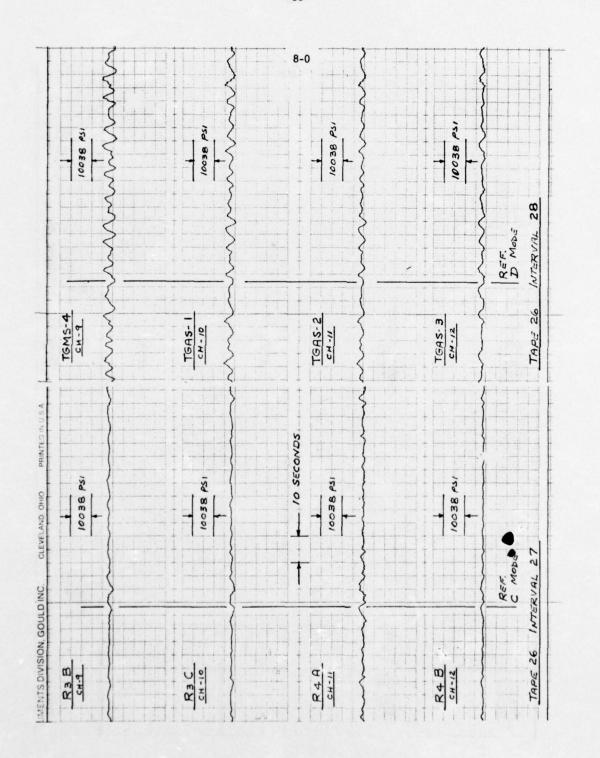












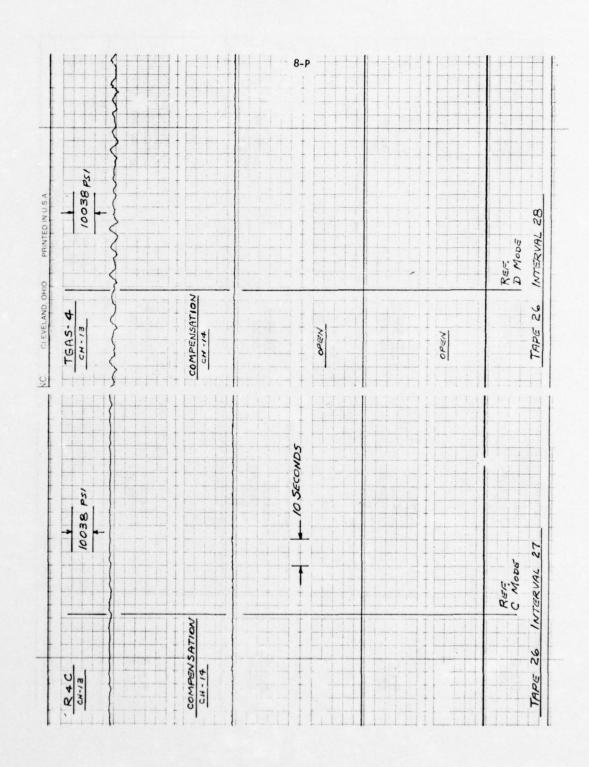
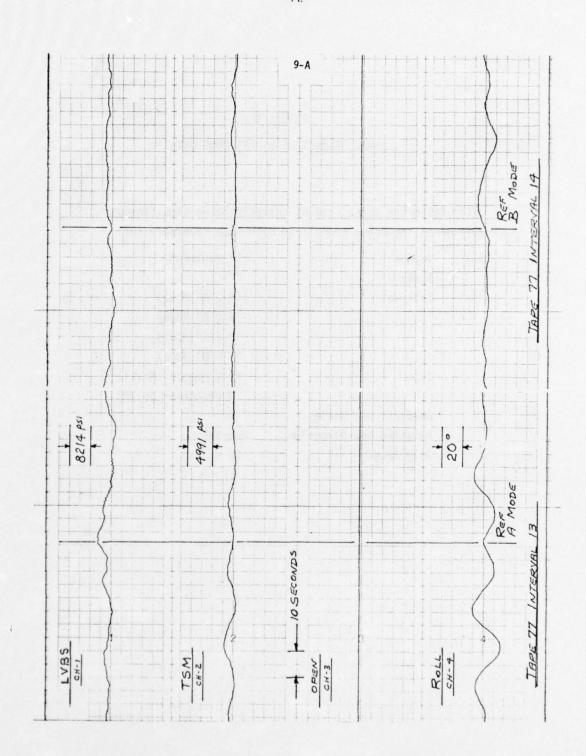


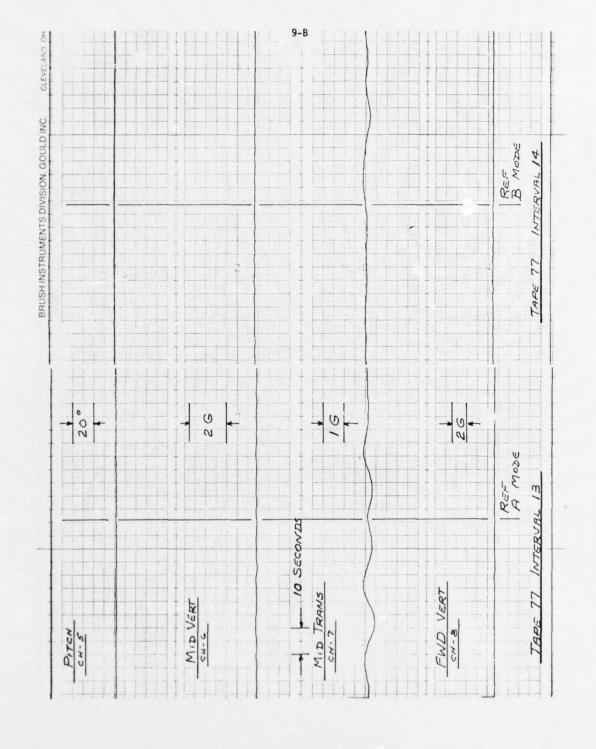
FIGURE 9

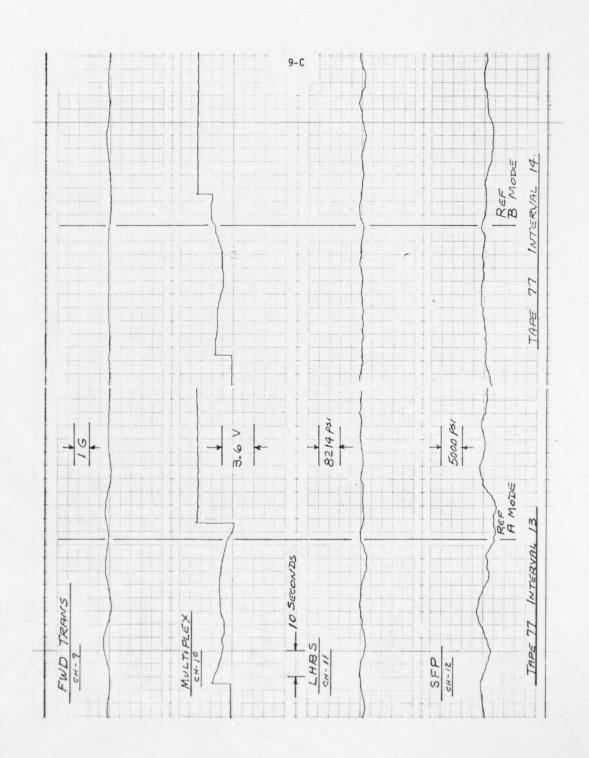
SAMPLE SIMULTANEOUS RESPONSE DATA

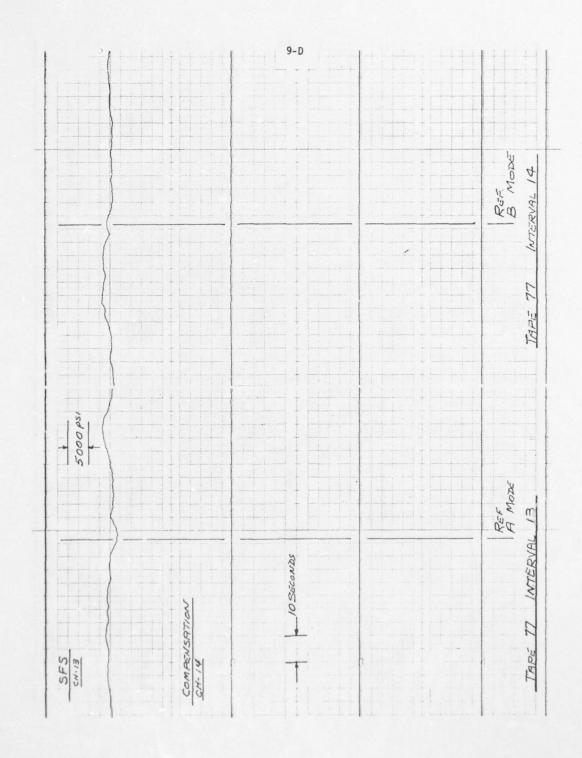
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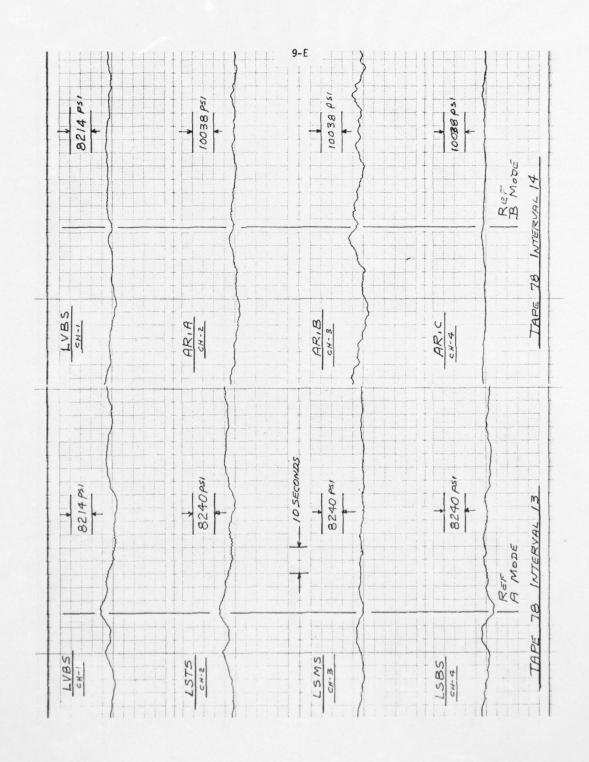
Voyage	11 Westbound
Index	22
Interval	13 ("A" Mode)
	14 ("B" Mode)
	15 ("C" Mode)
	16 ("D" Mode)
Tape	77 (Recorder No. 1)
	78 (Recorder No. 2)
Beaufort Sea State	8
Relative Sea Direction	Quartering
Ship Speed	29 Knots

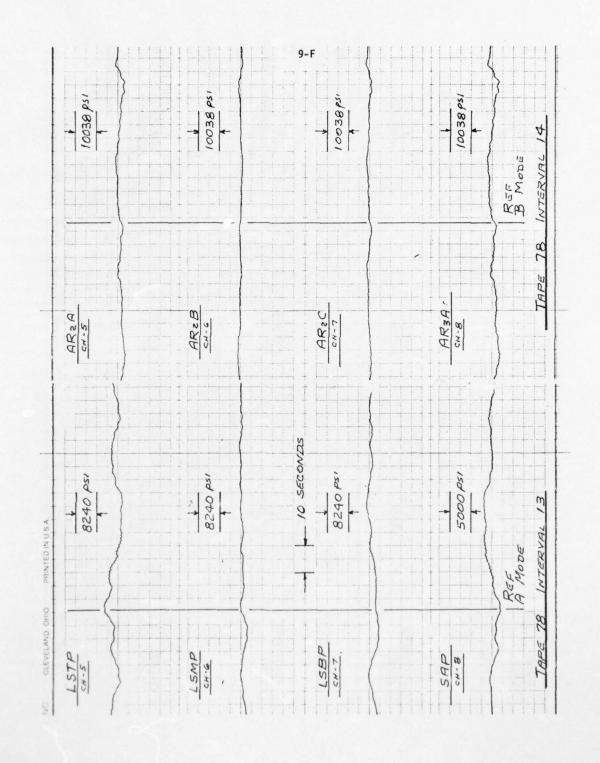


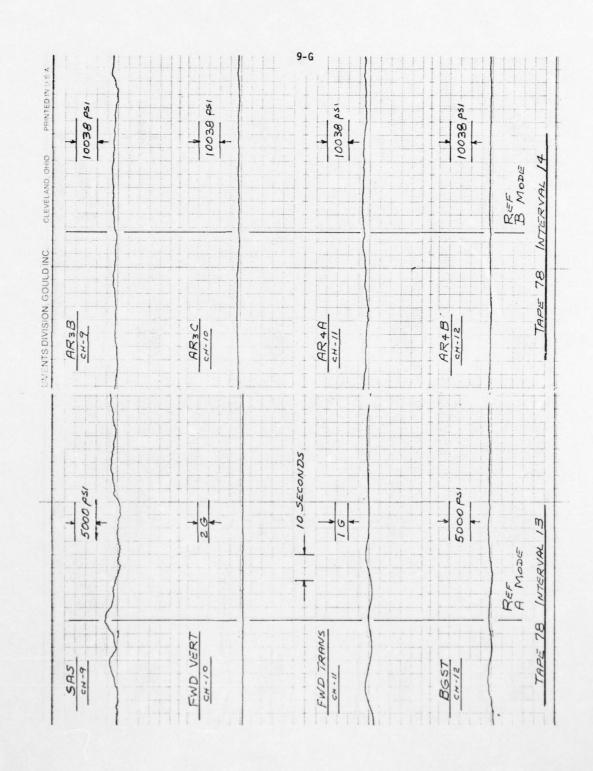


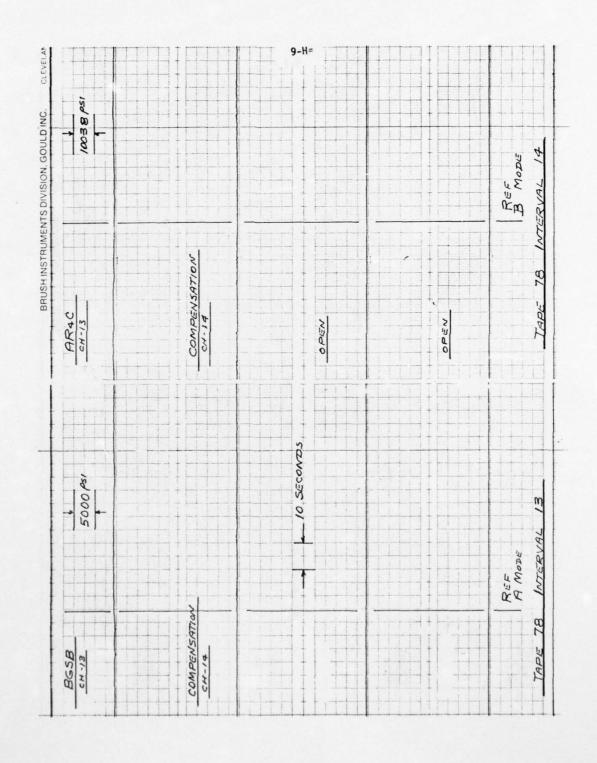


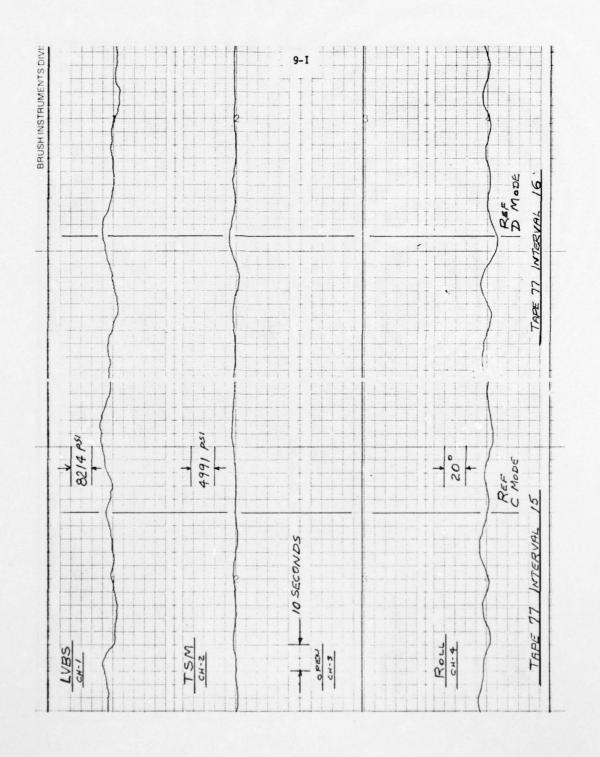




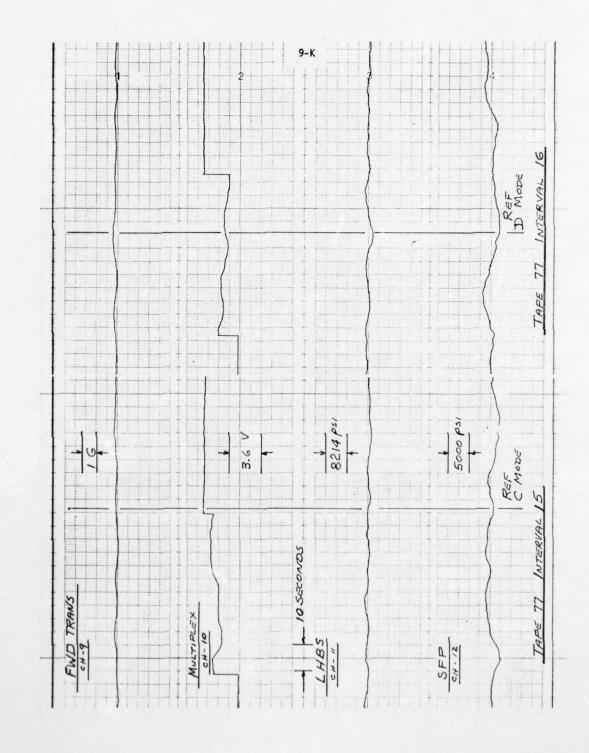


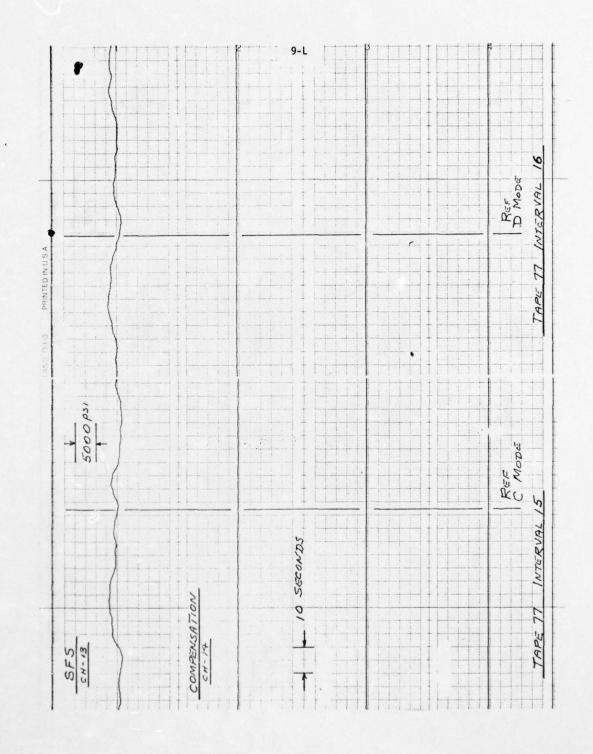


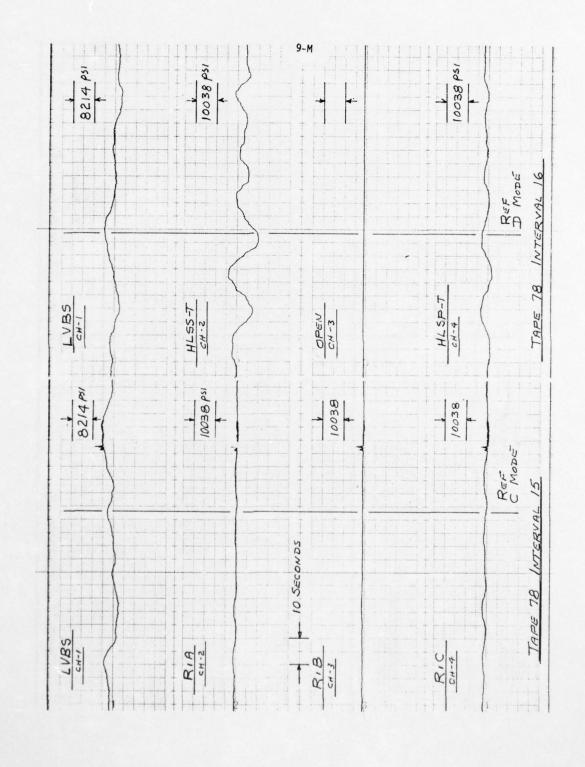


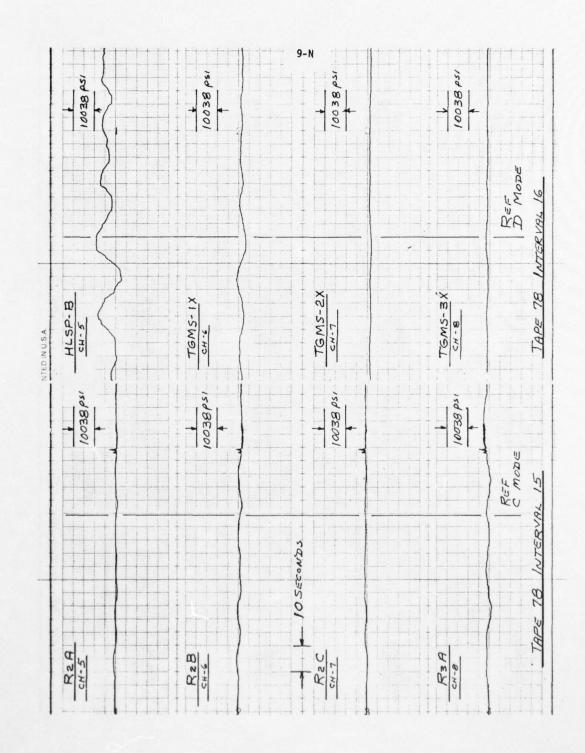


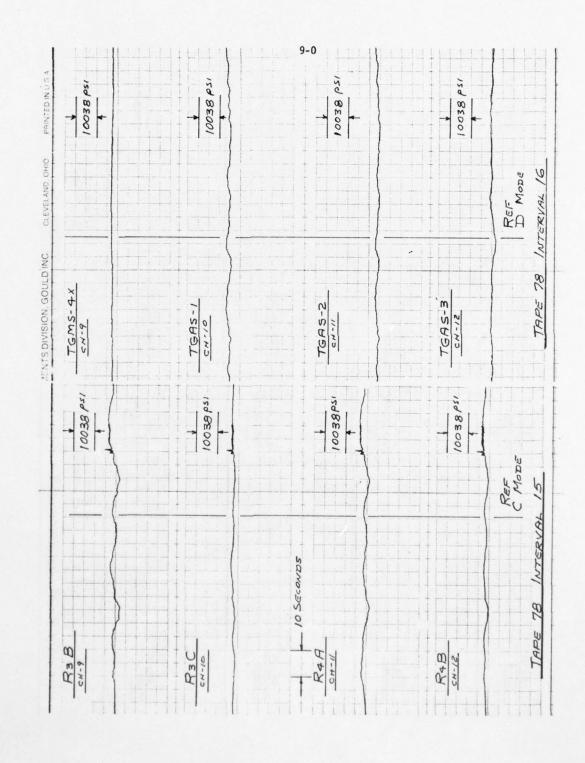
	2	9-J		REF DE MODE TAPE 17 INTERVAL 16
200	9 -	37	26	REF C MODE
P)rcH	MID VERT	MID TRANS CH-7	FWD VERT	TARE 77 INTERVAL











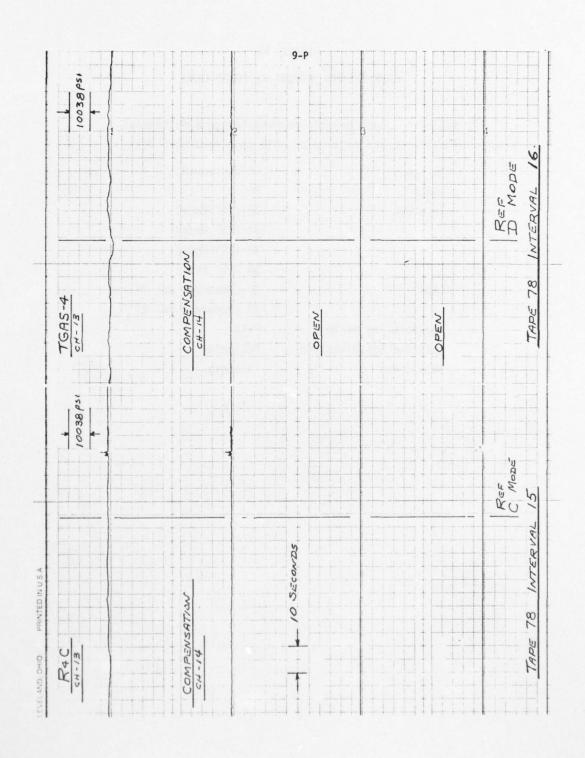


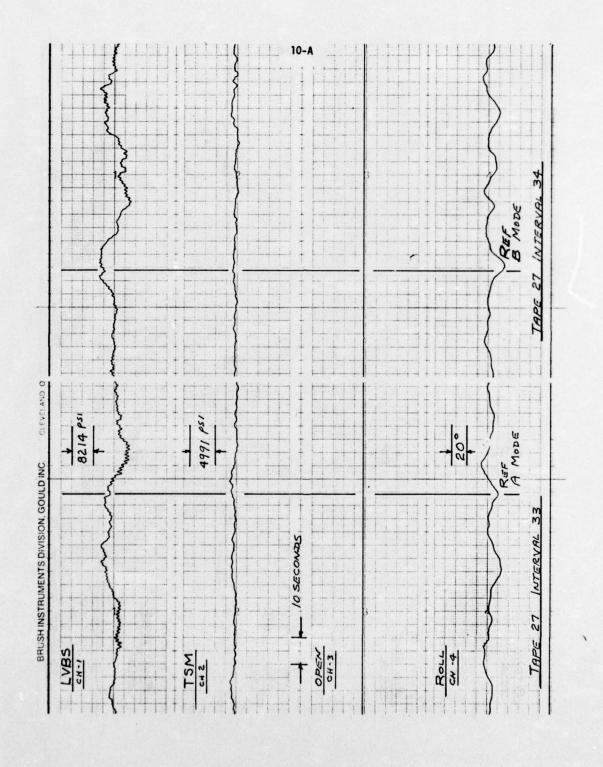
FIGURE 10

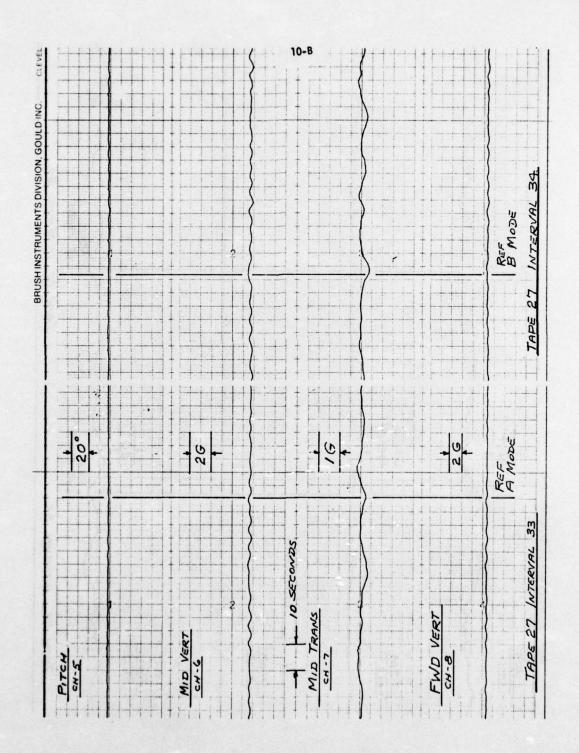
SAMPLE SIMULTANEOUS RESPONSE DATA

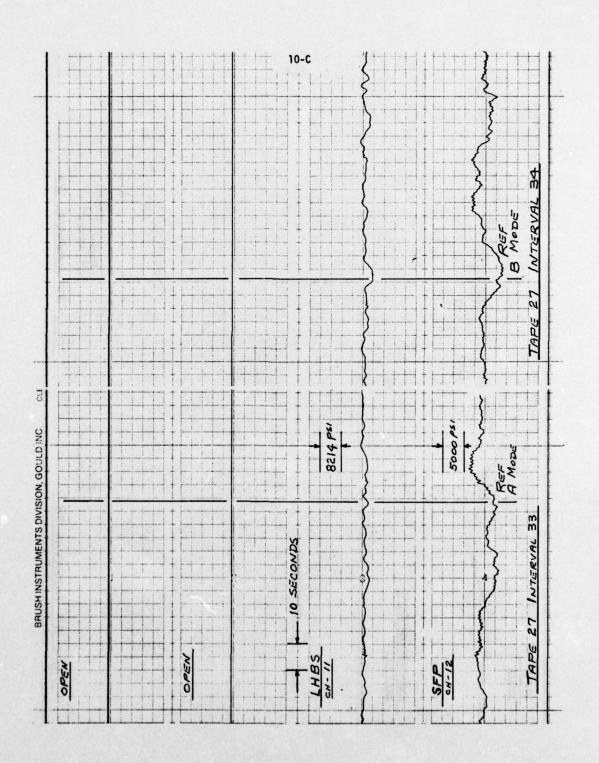
The following pages present representative simultaneous samples of all recorded signals on both tape recorders for:

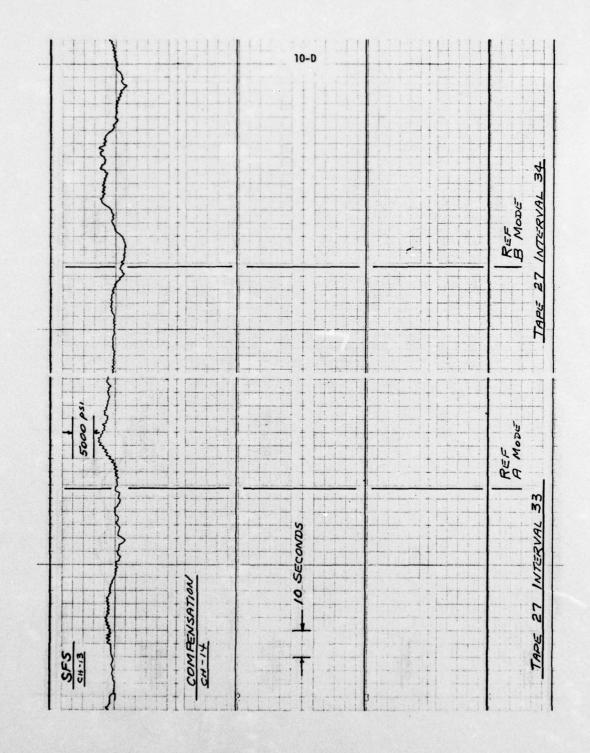
Voyage	4 Westbound		
Index	26		
Interval	33 ("A" Mode)		
	34 ("B" Mode)		
	35 ("C" Mode)		
	36 ("D" Mode)		
Tape	27 (Recorder No. 1)		
	28 (Recorder No. 2)		
Beaufort Sea State	9-10		
Relative Sea Direction	Following		
Ship Speed	29 Knots		

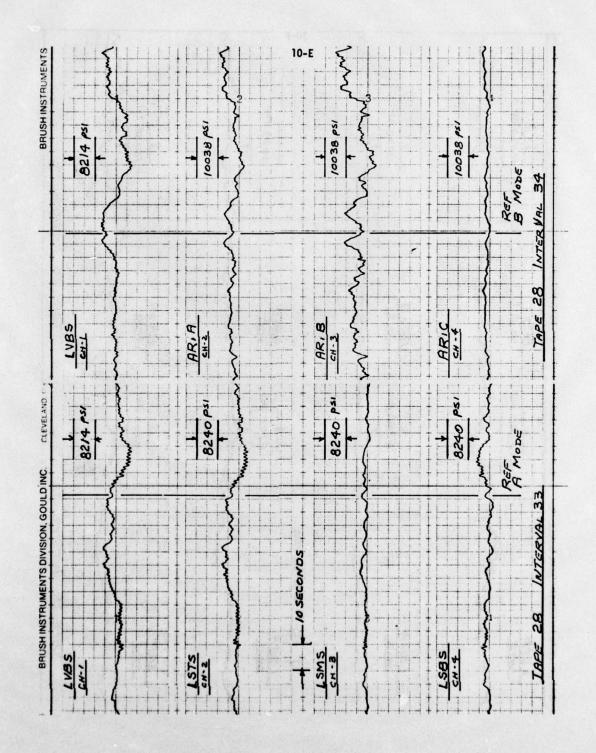
AD-A039 752 TELEDYNE MATERIALS RESEARCH WALTHAM MASS F/6 13/10 FIRST SEASON RESULTS FROM SHIP RESPONSE INSTRUMENTATION ABOARD --ETC(U) SEP 76 R R BOENTGEN, R A FAIN, J W WHEATON N00024-73-C-5059 UNCLASSIFIED SSC-264 NL 2 oF 3 AD 39752

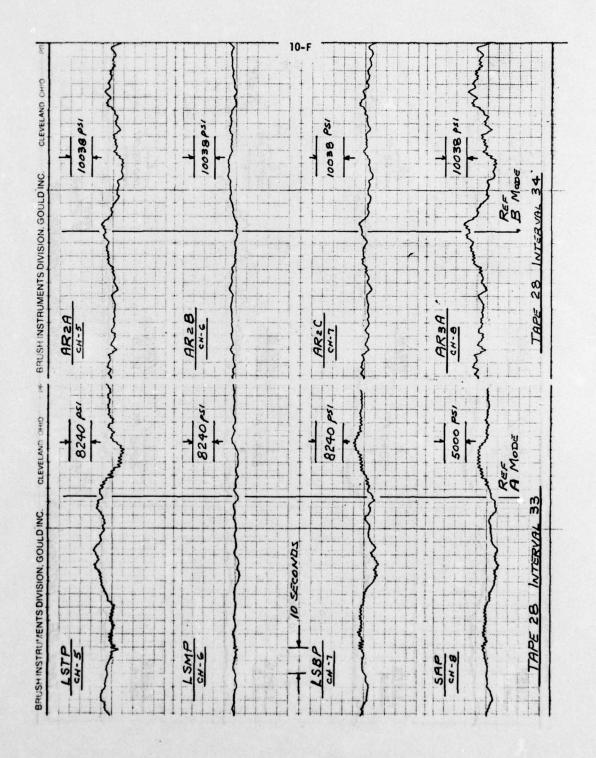


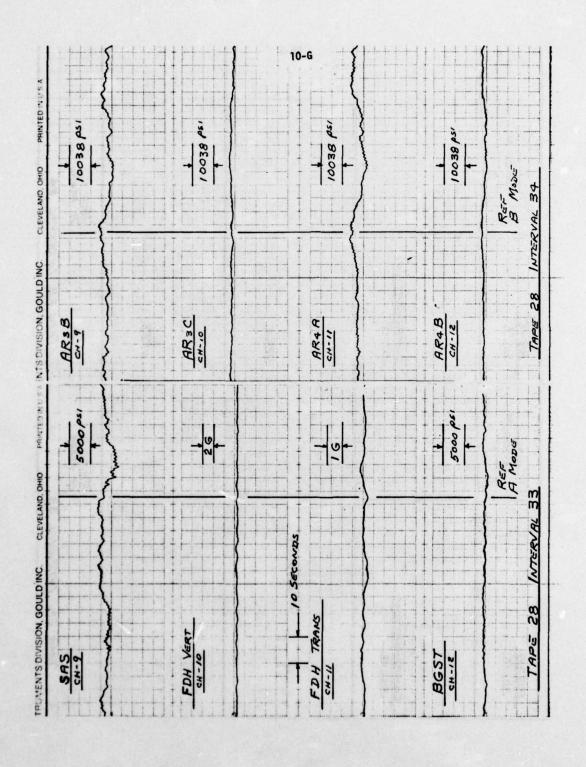




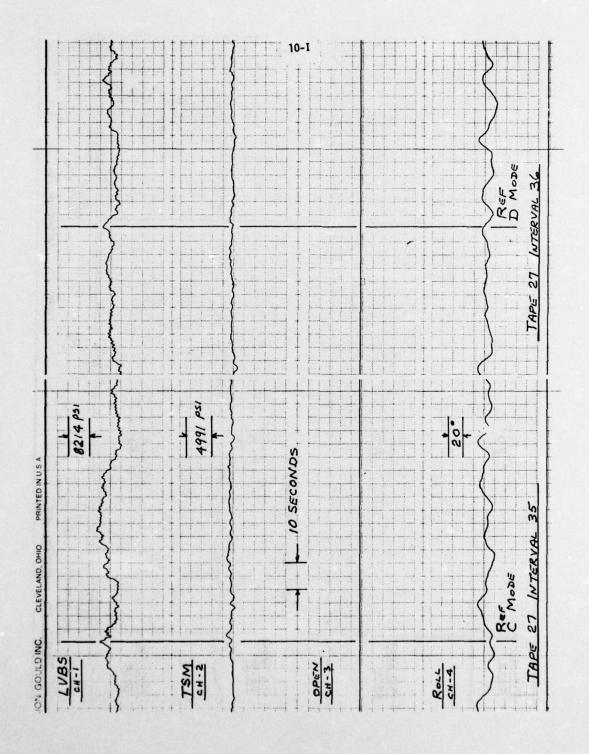


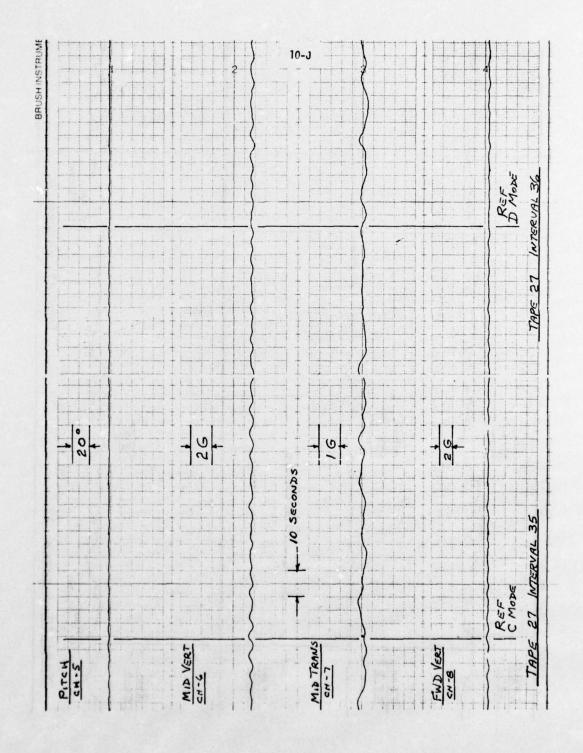


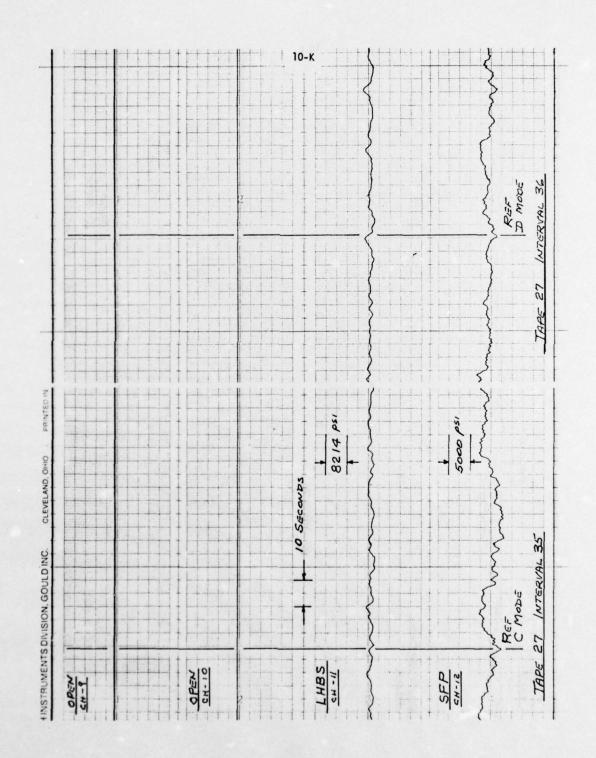


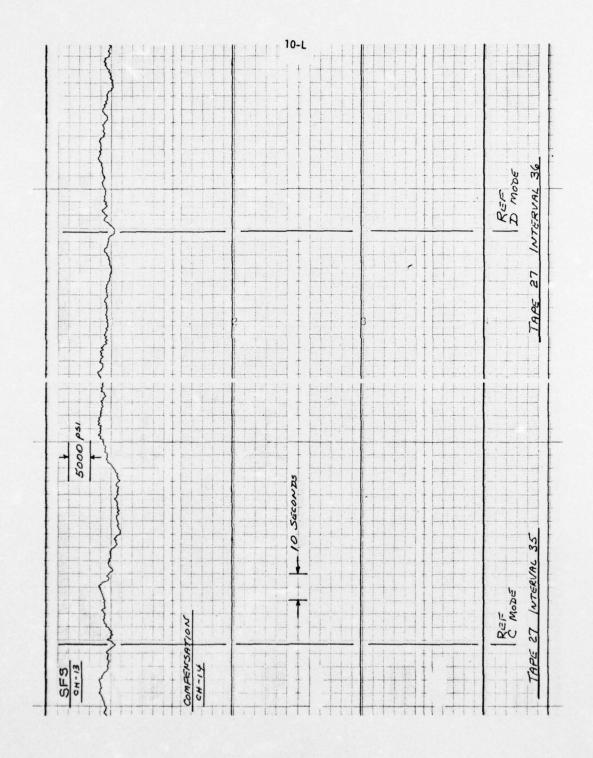


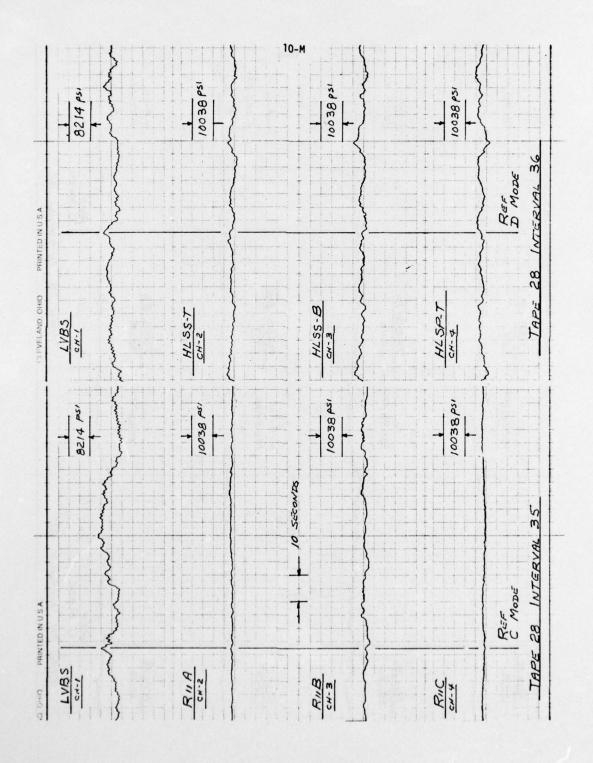
) Na 65 00/					REF B Mode
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865 <u>8</u>	ComParisor Tool	50/003E 0/			00 001

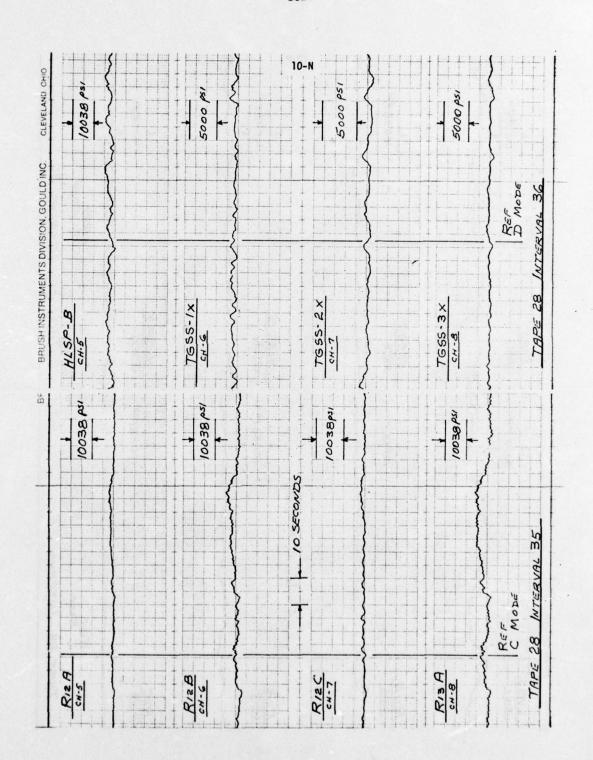


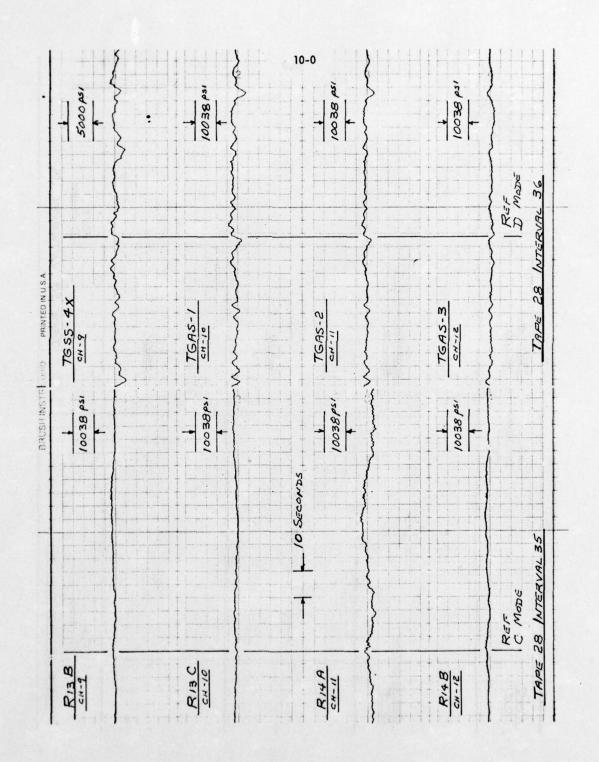












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CH-13	COMPENSATION		Res	TAPE 28 IN

gages recorded on Recorder No. 2. The maximum peak-to-trough combined values were scaled from oscillograph records for each interval on Voyage 4, separated into sets by Beaufort Number, and the maximas averaged and plotted. Figures 11-A and 11-B present the results from this process. For general comparison, the averaged results from the Longitudinal Vertical Bending (LVB), the Longitudinal Horizontal Bending (LHB), and the Torsional Shear Midship (TSM) stress gages have been plotted against Beaufort Number in Figure 12. These results are from the wave-induced digitized data.

6. Wave Height Radar Data

As part of the continuing effort to obtain accurate information as to the exact nature of the waves incident to the vessel, a wave height radar system was installed aboard the SEA-LAND McLEAN. The output, in the form of a slant range signal, is provided for recording on Channel 3 of Recorder No. 1. The antenna for the device is at the bridge level on the outboard starboard side. The signal, of course, contains components of ship motions. Figure 13 compares the slant range signal with Vertical Bending Stress, Bow Vertical Acceleration, and Roll Sensor outputs.

7. Torsional Response Data

The simultaneous waveforms have been used to develop data plotted in Figure 14, which shows the relationships between strains at the upper corners of the midship transverse girder, and overall midship torsional shear.

8. <u>Simultaneous Comparison of Longitudinal Gages</u>

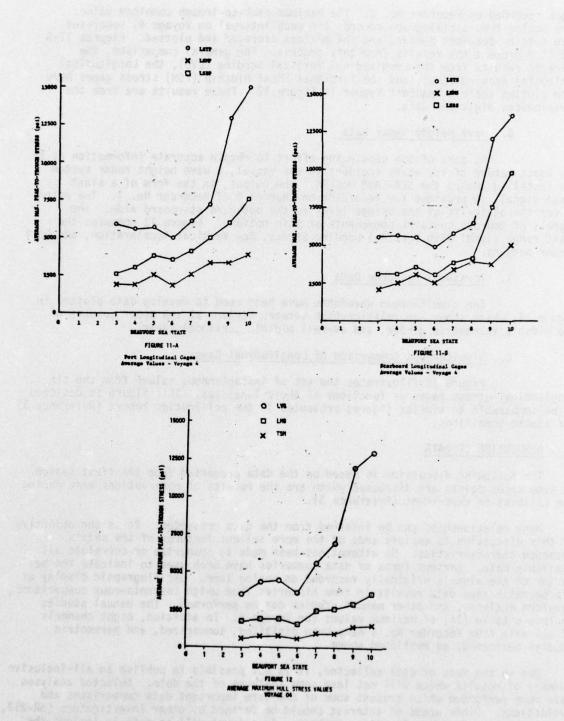
Figure 15 illustrates the set of instantaneous values from the six longitudinal stress gages as functions of their locations. This figure is designed to be comparable to similar figures presented in the calibration report (Reference 3) for static conditions.

IV. DISCUSSION OF DATA

The following discussion is based on the data presented from the first season. In some cases points are discussed which are the results of observations made during the calibration experiment (Reference 3).

Many relationships can be inferred from the data presented. It is the objective of this discussion to explore some of the more salient features of the ship's response characteristics. No attempt has been made to summarize or correlate all available data. Various forms of data summaries have been used to indicate the behavior of the signals originally recorded on analog tape. Oscillographic display of the magnetic tape data results in time histories from which instantaneous comparisons, waveform analyses, and other manual studies can be performed. The manual studies include a table (IX) of maximum values for Voyage 4. In addition, eight channels of all data from Recorder No. 1 have been digitized, summarized, and parametric studies performed, as mentioned above.

Due to the mass of data collected, it is not possible to publish an all-inclusive summary of results which will not lose some features of the data. Selected analyses have been performed which present some of the more important data comparisons and evaluations. Other areas of interest should be defined by other Investigators (SR-217, for example) or Advisory Committee members. An attempt will be made to include the



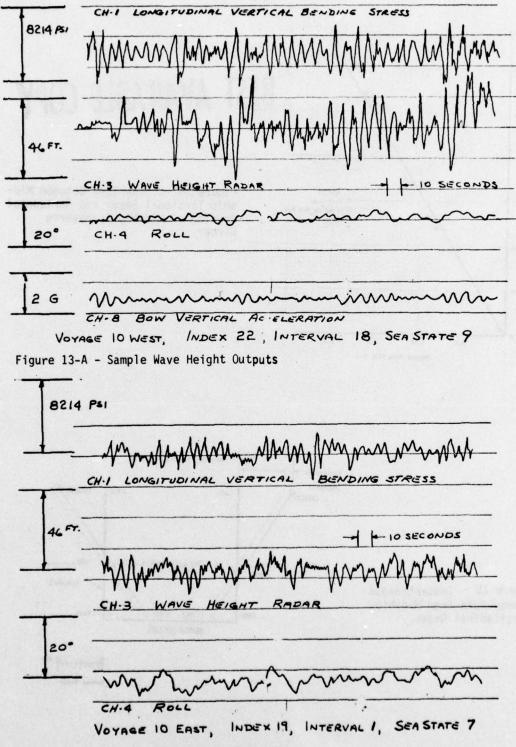
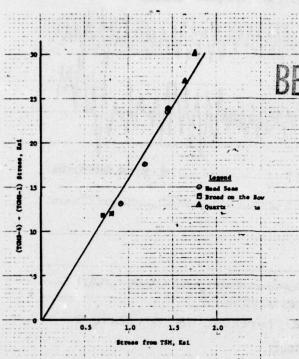


Figure 13-B - Sample Wave Height Outputs



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Figure 14 - Comparison Between Midship Torsional Shear and Horizontal Bending of Midship Transverse Girder.

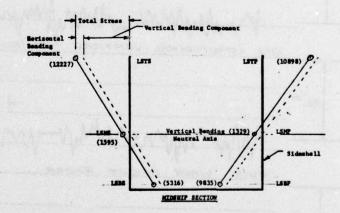


Figure 15 - Instantaneous Seaway Data from Midship Longitudinal Gages.

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desired data or format in future reports or, if the need is pressing, to issue appropriate supplemental reports.

A. Voyage 4 Simultaneous Response Data

As indicated by Figure 6, no sea conditions in excess of those corresponding to Beaufort 9 were encountered during eastbound voyages, and only two indexes had Beaufort Numbers of 9. In either direction the most commonly reported Beaufort Number was 4, whereas the median value was 5. During westbound voyages Beaufort Numbers of 9 and 10 were reported about equally. Westbound voyages are, therefore, used for high-sea-state, instantaneous data presentations. Voyage 4 had the highest average and peak sea states. It was, therefore, used to provide simultaneous response data for signals assigned to Tape Recorder No. 2 for Figures 7, 8, 9, and 10.

Figures 7, 8, 9, and 10 present recorded high sea state response data for head, broad-on-the-bow, quartering, and following relative sea conditions. Ship speed is reduced from about 30 knots to about 20 knots in the head and broad-on-the-bow cases.

As expected, the most obvious difference between the four sets of data is the period of the wave-induced (long period, low frequency) responses. In the head or broad-on-the-bow data, the 8-9 second wave encounter period is obvious along with the constant 0.8 Hz first-mode structural frequency. For the quartering or following sea cases, a much larger and less well defined wave-induced stress period is present along with the 0.8 Hz first mode response. The magnitude of the peak-to-trough longitudinal vertical bending stress (LVB) is dependent on and approximately equal for similar sea state numbers.

1. Head Seas

An example of slamming is exhibited during Interval 17 (Mode A) of Tape 25 (head sea). A fairly clean hogging stress is followed by sagging and high first mode stresses. The first mode stresses gradually decrease over a period of 40 seconds. Vertical accelerations at the midship and forward deckhouse accelerometers are also evident and closely follow the vertical bending stress curve. At the same instant there are similarly shaped but opposite longitudinal stresses in the top and bottom hull sideshell gages (LSTP, LSBP, LSTS, LSBS, all on Recorder No. 2, both port and starboard) with virtually no stress exhibited at the vertical bending neutral axis (LSMP and LSMS). The bottom stresses are lower than those measured by the top gages because they are closer to the neutral axis.

The small differences, port to starboard, between the respective midship top, neutral axis (mid) and bottom sideshell gage outputs are due to horizontal longitudinal bending components. This component, along with the longitudinal warping stress, also contributes to the nonzero output of the mid sideshell gages. Neutral axis shear gages (SAP and SAS) show similar responses with the opposite polarity (due to the port and starboard wiring convention).

Another example of slamming is shown near the reference lines of the "B" Mode (Interval 18) of the same tape. In this case the aft rosette responses are monitored on Recorder No. 2. Although AR-1 and AR-2 are located in similar positions but opposite sides, they nevertheless exhibit dissimilar responses in magnitude for the longitudinal and transverse gages (elements A and C, respectively).

In comparing the diagonal gage outputs, however, it should be kept in mind that these elements are parallel to each other and are not symmetric about the ship's longitudinal centerline.

It is interesting to note that although the response period of these gages is similar to that of the longitudinal vertical bending stress gages, their peaks are more rounded and the waveform lags the bending sensor output slightly. The largest output for this gage group is exhibited by the longitudinal element of AR-4 which is located in the starboard longitudinal tunnel top. It reflects the longitudinal bending stress at this location.

Intervals 19 and 20 (Modes "C" and "D" of the same index) present similar sea conditions and similar responses on the respective Recorder No. 1 sensors. The longitudinal element of rosette R1 (located aft of the forward house) exhibited the largest stress of the rosettes in this group. Second largest was the longitudinal element of the similarly placed gage on the opposite (starboard) side. Virtually identical stresses were measured by the diagonal element of this gage and the longitudinal element of the gage located in the tunnel top (R3). A still lower stress was present in the longitudinal element of the outboard tunnel top gage (R4). To summarize, the line load seems to be dropping off towards the outboard sides with the forward house a significant factor in the transmission of bending stresses.

Only moderate stresses were recorded in the mid and aft transverse girder corners (in the transverse direction). It is interesting to note that response exhibited by the mid girder gages are predominantly wave-induced, while the aft responses contain obvious first-mode components. The tensile stresses on the forward plate of the transverse girder, coupled with compressive stresses on the aft (bulkhead) plate, indicate a horizontal bending mode. Notice also that the midship torsional shear sensor indicates some small torsional stresses of a similar shape.

2. Broad-on-the-Bow Seas

On the whole, the major characteristics of ship responses to this condition are similar to that for head seas. Vertical bending stress is somewhat reduced while torsional shear, horizontal bending, and roll are slightly increased. The pronounced first-mode slamming stresses are gone from the sample record.

All of the remaining sensor records are at or below the levels for the head sea conditions. Although both sets of intervals were recorded at Sea State 10, the present set is followed by a Sea State 9, and it is possible that the sea state had, in fact, moderated to a small degree. Other studies of the overall Voyage 4 data indicate that the maximum peak-to-trough stresses are very strong functions of sea state for levels of eight, and above. This may well explain the reduction in stress magnitude. Logbook entries of the observer for this Index indicate spray over the ship but no slamming. This is probably the result of the reduction in sea state and not the change in relative sea direction.

3. Quartering Seas

The most obvious characteristic of the quartering and following sea conditions is the long-period wave-induced responses. Another striking difference is the indicated roll + 13 degrees in Interval 13 ("A" Mode). This is accompanied by virtually no pitch or vertical acceleration, but significant transverse acceleration in phase with the roll. In this case the longitudinal neutral axis stress midships is not negligible, but is composed primarily of horizontal bending. Note

the out-of-phase relationship port and starboard, and the similarity to the longitudinal horizontal bending stress sensor output. It should be noted that although torsional stresses may contribute to this signal, the period of the torsional shear sensor output is different from that exhibited by the neutral axis or horizontal bending sensors.

Of the aft rosettes only the diagonal element of AR-1 (port side, near hatch cutout) showed significant strains, probably due to its being aligned with a stress trajectory from the aft house around the hatch opening.

The measured roll period does not correlate to the vertical or horizontal bending or torsion sensors. Roll does, however, correspond generally to the forward hull longitudinal strain sensors (HLSP/T-T/B).

Only small stresses were recorded for mid and aft transverse girders. The forward and aft signals seem to be uniformly out of phase.

4. Following Seas

The sample record presented for the following sea condition has a higher associated sea state than the preceding quartering condition. Many more instances of first-mode excitation are present on all traces. In general, the peak-to-trough stress levels are higher than for the quartering sea case. This is due, however, to the increased sea state rather than the relative sea direction. (A later section in this discussion will present data to affirm this assertion.)

Another characteristic of this data set is the nonperiodic nature of most output traces. This feature makes comparisons of phase behavior among the responses difficult.

The vertical bending sensor shows some evidence of slamming (a relatively clean hogging moment followed by first-mode excitation and an increasing sagging moment.) As would be expected from the following seas, very little torsional shear is present. Roll motions were significant at 20 degrees peak-to-trough. This trace is not a smooth sinusoid as in the case of the quartering sea, but reflects a continuous forcing function application without a steady state or decaying component.

Although virtually no pitch is present, a midship vertical acceleration in excess of 0.1g (peak-to-trough) was present, indicating a heaving translation. A decoupled (i.e., not at the same or harmonic frequency) transverse acceleration component of about 0.4g peak-to-trough was also exhibited. The horizontal bending signal correlates reasonably well with the roll angle. It can also be seen that the forward shear sensors correspond closely to the midship longitudinal stress sensors (available only in the "A" mode) including phase, indicating that these shears are generated mainly by overall vertical bending.

A large (approximately 20 Ksi, peak-to-trough) stress was again present in the diagonal element of the port aft rosette (AR-1). However, there again was no correspondence between the longitudinal and lateral elements of this gage and the symmetrically placed elements on the starboard side. This may be due to the nature of the cargo loading. If the net load in each hold has a port or starboard component the static and dynamic effect of this offset may be to induce these types of stresses.

Gages located in the longitudinal tunnel exhibit the largest stress in the longitudinal direction both forward (gages R-13 and R-14) and aft (gages AR-3 and AR-4). In all cases these stress outputs closely follow the midship vertical bending sensor output.

B. Extreme Variations with Sea State

All maximum peak-to-trough values (combined wave-induced and vibratory) of the six longitudinal stress sensors have been averaged for each Beaufort Number of Voyage 4 and plotted in Figures 11-A and 11-B. In addition, Figure 12 shows similar averages for the LVB, LHB, and TSM transducers taken from the digitized wave-induced records. In all cases, each average contains all ship speeds and relative wave directions.

Average vertical bending and individual midship longitudinal stresses (port and starboard, top and bottom) all increase with increasing sea state. However, at Beaufort Numbers of eight and above, they increase at a faster rate. This situation does not seem to hold for the Torsional Shear Midship or Longitudinal Horizontal Bending sensors. The midship longitudinal neutral axis gages (port and starboard), which see the combined horizontal bending and restraint-of-torsional-warping stresses, similarly do not exhibit the marked stress increase above Beaufort 8. It is therefore probable that the vertical bending stress increases are real and not due to a systematic error in Beaufort Number estimation.

The stresses measured by the six longitudinal gages include components from vertical, horizontal, and torsional loads. The values for the neutral axis pair (X's in Figures 11-A and 11-B) are relatively insensitive to vertical bending, however, so the moderate increase with increasing Beaufort Number must be an indication of increasing horizontal and/or torsional loads. This is confirmed by inspection of Figure 12, which shows an equally moderate increase in those components. The fact that the individual stresses at the bottom on each side are consistently lower than the comparable deck stresses is because of the location of the neutral axis at about 44% of the depth, measured up from the baseline. The significantly higher values for vertical bending at Beaufort Numbers above eight are probably the result of the existence of waves, or combinations of waves and swells, considerably higher and longer than those observed at the lower sea states. Inspection of the logbook data for Voyage 4 in Appendix 4 shows many intervals of reduced speed operation with pitching and slamming noted.

C. Sample Wave Height Signals

Two intervals of wave height radar outputs are presented in Figure 13. This instrument measures the slant range from a position on the forward house to the ocean surface at a constant relative bearing. A minimum of two corrections are required in order to correlate these data to the wave height. Although the angle between the ship's vertical axis and the radar transmission axis is constant, ship's roll alters the angle between the transmission axis and the ocean surface. This, in turn, changes the slant range. In addition, the vertical height above the ocean changes due to pitching and heaving. This also changes the slant range. Some of the required correction signals are available from the instrumentation system. Roll angle can be utilized directly. A double integration of the forward vertical acceleration signal will yield the change in vertical height of the radar from any reference level.

In reviewing the output traces of the wave height radar some correlation can be seen between the roll and radar output. Although this correlation could be due to the waves affecting the ship's roll, it is probable that the reverse is true; the roll is affecting the measured wave height. A lesser correspondence is seen between the vertical acceleration and the radar output. In some instances, however, the periods of these two signals coincide.

(This discussion has ignored the second-order effect on true wave height from changes in angular relationships due to the accelerometers being mounted in the strap-down configuration.)

D. Torsional Stress Indicators

One of the conclusions of the Calibration Report (see Reference 3), is that the midship transverse girder gages (TGMS) are a more sensitive indicator of torsional loading than the midship torsional shear sensor (TSM). Seaway data provide an additional reinforcement of this assertion. Figure 14 presents a plot of the torsional shear sensor output against a measure of the horizontal bending in the midship transverse girder. Each point represents a randomly-selected peak-to-trough stress reading with ordinate and abscissa values taken at the same instant in time. The data from which these points were drawn represent the higher sea states. The difference between the signals from the upper (fore and aft) corner gages in the transverse girder is taken as the measure of horizontal bending in the girder. Since the output of these gages is 180 degrees out of phase, their algebraic difference results in their absolute values being additive. A pure horizontal bending component is thus generated with twice the sensitivity of a single gage. (This bending results in an "S" curved transverse girder with the ends at each longitudinal tunnel acting as fixed.)

It can be seen from Figure 14 that the horizontal bending stress generated in the transverse girder is higher, by a factor of approximately 16, than the corresponding torsional shear stress for all sea directions.

E. Midship Longitudinal Gages

The odd behavior of the six midship longitudinal stress gages during the calibration experiment (see Reference 3) raised some questions as to the correctness of the instrumentation system with regard to these gages. Seaway data can be used to verify their proper operation under the assumed conditions.

Figure 15 presents a plot of the output from these six midship gages for an instant in time. A head-sea condition was chosen so as to minimize the torsion-al contribution to longitudinal stress which cannot easily be separated from the horizontal contribution. As shown in the figure, the stresses are well behaved and what one would expect of a vertical bending condition with a small horizontal component. This representation is typical of that which was observed in many instances for the seaway data. It thus affirms the proper operation and configuration of these gages.

F. Parametric Studies (Appendix 3)

To aid in the interpretation of the results of the parametric studies (which are, in effect, a presentation of the entire season's data from eight of the most important transducers), the plots and tables from the Longitudinal Vertical Bending (LVB) stress data will be considered in some detail.

Figure B-l is a "dot-plot" of the RMS stress value from the LVB transducer by Beaufort Number for the entire season. There are 2,078 points shown. The great scatter in each Beaufort Number is caused by the fact that these points are from all relative wave directions and all ship speeds. Figure B-2 has been plotted from these basic data points analyzed into five classifications of ship speed. The classification nomenclature is given in Table B-II, and in all of the Tables B-III through B-XXXIV at the end of Appendix B. Again, the average values given for each ship speed also contain some range of relative wave direction. Figure B-2 shows that the highest mean values of RMS vertical bending stress were measured at Beaufort 10, at ship speeds between 20 and 25 knots. Note that at the next higher speed range the stresses were lower at the highest Beaufort Numbers, which is probably due to predominantly quartering or following seas. There are no reported cases of operation at full speed at Beaufort Numbers higher than 9.

Figure B-3 is a similar classification of the data by relative wave direction. The values for Beaufort 10 (which contain a range of ship speeds as shown in B-2) indicate that the highest stresses were experienced in head seas, the next highest at relative wave directions from 31 to 60 degrees, and the next highest in quartering seas. Beam seas produced the lowest vertical bending stresses at Beaufort Numbers 8 and above.

Figures B-4 through B-6 are organized in the same way except that they present the distributions of the maximum peak-to-trough stress variations. The stress amplitudes scales are doubled, but the general distributions are the same.

The tables following these figures in Appendix B present the basic data for the figures, and, in addition, the standard deviation of the mean values. These provide a measure of the scatter of the data.

Some brief comments can be made concerning the results of these parametric studies:

- 1. Horizontal bending stress is much lower than vertical bending stress, and is less sensitive to variations in ship speed and relative wave direction, although quartering seas appear to contribute significantly to higher stresses at Beaufort 10.
- Torsional Shear Midship is even lower, with less scatter at Beaufort
 quartering seas are a factor at Beaufort
- Forward Shear Port and Starboard results are essentially the same. The largest shearing stress variations occurred at Beaufort 8, in broad-on-the-bow and quartering seas.
- 4. The Roll results show more rolling at higher Beaufort Numbers with higher speeds. Quartering and beam seas cause the most rolling. A maximum dynamic roll of \pm 18° was recorded at Beaufort 10.
- 5. The maximum pitching angle was \pm 2.5 degrees at Beaufort 9. The most pitching occurred at head seas, the least at beam, quartering, and following.
- 6. The Forward Acceleration (Vertical) showed a maximum of \pm 0.45 g. Highest values were recorded in head seas.

V. POSSIBLE DATA FORMATS

This report presents data in a number of forms, those which seemed most appropriate for an overall survey of the data from the first season. Included are expanded time-histories, logbook tabulations, tabulations of maximum values scaled from compressed time-histories, and plots derived from parametric studies of digitized response and logbook data. Also available, but too voluminous for publication, are tabulations of response and logbook data for each interval, all season, for all eight digitized transducers. As a guide for the consideration of possible expansion, modification, or deletion of these data formats, Figure 16 has been prepared to indicate the various possible data presentation formats.

Of the formats illustrated, all but the spectral computations and manual tabulations of logbook data have been used in this report. From the standpoint of relative cost the manual formats shown at the top of the figure are least costly, but are cumbersome where a number of transducers are to be compared. An expanded time-history is essential for the instantaneous comparisons, since the digital data from different transducers have no common time base once a specific interval is defined.

Digitizing the data is relatively expensive, both in man-hours and in computer costs, but this method has great advantages for rapid tabulations and plots of both logbook and response data. At present the data is filtered so that RMS and maximum values are computed from essentially pure wave-induced response, for comparison with design data derived on the same basis. Vibratory components from slamming or other excitations are retained in the basic digitized record of 12,000 data points from 20 minutes of each 30-minute interval. Spectral computations are made from this record.

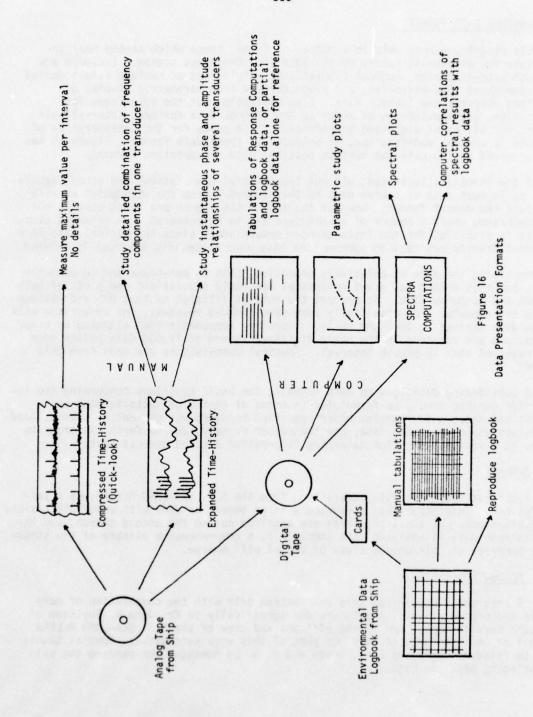
In considering decisions on data formats, the basic questions concerning the information desired should be formulated in terms of choice of instantaneous vs. statistical data, a few samples under specified condions vs. the entire season, need for future use of the same data, one transducer or many, and so forth, in order to arrive at a rational decision balancing information desired against cost.

VI. SUMMARY

The first season of data acquisition from the S.S. SEA-LAND McLEAN was a successful one. This report has presented a large amount of data with brief discussions and evaluations. As additional data are acquired during the second season, and the first season data is analyzed more completely, a comprehensive picture of the structural behavior of this unique class of vessel will emerge.

VII. ACKNOWLEDGEMENTS

A program as complex as this can succeed only with the cooperation of many people and organizations. Thanks are due specifically to Mr. John W. Boylston of Sea-Land Service, Inc., and to the officers and crew of the S.S. SEA-LAND McLEAN for all of their efforts to make our part of this work successful. Special thanks also to Teledyne engineers E. T. Booth and H. G. La Montagne for manning the ship and bringing back the data.



VIII. REFERENCES

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APPENDIX A

Partial Listing of Logbook Data First Season S.S. SEA-LAND McLEAN

Nomenclature

VOY = Voyage number, East or West

TP = Analog magnetic tape number

INT = Data interval number

IDX = Logbook index number

DATE = Month/Day/Year

Time = GMT

SPD = Ship speed, knots

BN = Observed Beaufort Number (appearance of sea)

RWVD = Relative Wave Direction (degrees, Port or Stbd)

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02w	1	1	018	051	10/26/72	2000		05	0945	CLDY		030		052	012	10/30/72	2400	11 7	40	0975	CCAST	SCHALL
02m	1	1	039	151	10/26/12	2000		05	0445	CLDY			-11	053	013	10/31/72	0400	31.7	06	0975	PICDY	SUUALLS -
02w	11	1	040	051	10/20/72	2000		05	0945	CLLY		036	13	054	011	10/31/12	0400	41.7	06	0975	PICOV	SQUALLS
	- 13	1	501	0.25	10146115	2400		04	0055	CLOY		036	13	055	015	10/31/72	0400	31.7	06	0475	PTCDY	SGUALLS
					10/26/12				0935	CLOY												SQUALLS
					10/20/15					CLOY		036	13	057	014	10/31/72	0800	31.8	00	0975	CLOY	
05=	11	1 1	044	045	10/54/15	2400				CLOY		036	13	058	014	10/51/77	0400	31.6	06	09/5	CLUY	
05m	11	!	045	055	10/27/72	0400		00		CLDA		-030	13	059	014	10/31/72	2000	31.A	06	0975	CLOY	
024	11	1	046	053	10/27/12	0400		00		CLDY						10/31/72						
024			347	971	10/5//15	2488		00		CFOA						10/31/72						
024	11		000	075	10/5/1/15	0400		00		CLDY	-					10/31/15						
434	-		050	054	10/27/77	0000		0.0		CLEAR						10/51/72						
02W	-11		051	054	10/21/12	0500		00		CLEAR						10/31/72						
024	11		520	054	10/27/72	0800		00		CLEAR			- ! ?	005	015	10/31/72	1 100	31.0	07	1275	OCAST	
OSE	13		017	005	10/29/12	2000	26.6	05	180	DENSE	FnG					10/31/72						
035	-13	1 (016	005	10/29/72	2000	26.4	03	180	DENSE	FOG					10/31/72						
0 3E	13	. (019	005	10/24/72	2000	24.6	05	100	DENSE	FUG	036	15	009	016	10/31/72	1600	31.9	05	1055	PICLOY	
03€	13	. (050	005	10/29/12	2000	26.6	0.5	180	DENSE	FOG					10/31/72						
€ 3€	-13	. (150	006	10/29/72	2400	28.7	04	0475	DCAST	SUUALLS					10/31/72						
03€	13		250	000	10/29/72	2400	24.7	04	0475	OCAST	SOUALLS					10/31/72						
036	13		053	000	10/50115	2400	7.AS	04	0475	DEAST	SOUAL S					10/31/72						
03F	13		950	900	10/29/72	2400	28.7	04	0475	UCAST	SQUALLS-					10/31/72						
0.36	13		650	007	10/10/12	0.100	15.0	07	1 345	DCAST	PAIN	036	15	015	016	10/31/12	1.00	31.0	05	1055	PTCLDY	
036	13		020		10/30/72	0400	35.4	07	1145	DEAST	HAIN HAIN	0.36	15	010	610	10/31/15	1000	31.0	05	1055	PTCLOY	
	-11		139	997	10/30/72	0400	32.9	07	1343	DEAST	OAIN		-15	-017	017	10/31/72	5100	31.1	00	1053	PICLOY	-
416	11		129	047	10/30/72	0400	12.4	07	1345	DEAST	HAIN					10/11/72						
. 16	- 13		0.50	006	10/30/72	0800	12 4	0.7	1149	DCAST		930	13	014	017	10/31/72	2100	31.1	00	1055	OTCLOY	
436	13		110	004	10/10/72	0400	12.0	0.7	1145	DEAST						10/31/72						
OSE	13		220	004	10/50/72	0800	12.0	07	1165	CEAST						10/31/72						
910	-13		035	009	10/10/72	1200	\$2.5	07	0945	CLUUDY	HUUGH					10/31/72						
ASE	13		034	009	10/30/12	1200	32.3	07	0945	CLOUDY	ROUGH					10/31/72						
03E	13		035	009	10/30/12	1200	12.5	07	0945	CLOUDY	HEIUGH					10/11/72						
93E	13		036	009	10/30/12	1200	\$5.5	07	0945	CLOUDY	ROUGH					10/31/72						
03€	13	0	357	009	10/50/72	1200	15.5	01	0945	CLOUDY	RITUGH	636	15	150	014	10/31/72	2400	31.7	05	1508	DEAST	
036	13	0	36	009	10/30/72	1500	32.3	07	0945	CLOUDY	HOUGH	036	15	950	010	10/31/72	2400	31.7	05	1508	CCAST	
					10/30/72								15	050	014	10/11/12	2400	\$1.7	05	12.3	DCAST	
036	13	0	40	009	10/30/72	1500	15.3	01	0 45	CLUMBA	HOUGH	036	15	030	018	10/31/72	2400	31.7	05	1503	CAST	
0.35	13	. 0	41	010	10/10/72	1000	31.7	40	0402	PICTOR		036	15	031	010	11/01/12	0400	51.5	05	150	CLDY	

. 404	TP	141	10x	DATE	TIME	SPO	81	RWVD	A-9	HEATHER	
950	15	032	019	11/01/72	0400	31.5	05	1505	CLDY		
035	15	033	019	11/01/12	0400	31.5	05	1505	CLDY		
-03E	15	034	019	11/01/72	0400	31.5	05	1508	LFDA		
0.25	13	0 22	0.0	11/01/15		21.4		1100	C. C. L.		
03E	15	030	050	11/01/72	0800	31.0	04	1725	CLDA		
				11/01/72							
036	15	038	050	11/01/12	0000	11.9	04	1728	CFDA		
036	15	034	050	11/01/15	0000	31.0	04	1729	CLOA		
0.36	15	040	050	11/01/72	0000	31,9	04	1723	CLUA		De-
476	15	041	0 7 1	11/01/72	1500	11.0	94	1/58	MEAST		The state of the s
036	15	042	051	11/01//2	1500	11.7	04	1728	COAST		The state of the s
-0.36	12	043	021	11/01/12	1200	31.9	04	1725	DEAST		P 1
035	12	044	021	11/01/12	1200	31.9	04	1725	DEAST		Street J
0 36	13	043	926	11/01//8	1600	31.4	04	1000	PICOY		(September 1
036	17	048	900	11/01/72	1000	31.4	94	100	PILOY		(3
	13	941	000	11/01/12	1000	****	04	Lune	PICOT		A COLUMN TO A COLU
	13	040	072	11/01/12	3000	11.7	04	1000	CLOUDY		()
				11/01/72							1
836	12	050	431	11/01/12	2000	31.4	0.4	LASP	CLOUDY		
- 416	-12	052	451	11/01/72	2000	31.7	0.4	1010	CL CHOY	-	
416	16	054	424	11/01/72	2000	***		1218	PIFLAN		lond- I
		454		11/01/13	2400	17 4			OTCION		and a
		001	001	11/00/72	1200	30.0	05	0225	DEAST.		The state of the s
	17	200	001	11/00/12	1200	30.0	05	0225	DEAST		Page 1
0.50	17	003	001	11/00/12	1220	10.0	05	0223	DCAST		and the second
	-17	004	001	11/06/12	1200	10 0	05	0225	DEAST		Comment
	17	005	002	11/06/72	1600		04	0225	FOG		
034	17	006	500	11/00/12	1600		04	0225	+06		7
05#	-17	007	500	11/00/12	1000	-	04	0725	+06 -		The second second
034	17	008	002	11/06/77	1600		04	0225	FRE		The state of the s
											No. or regard
-030	17	010	003	11/00/72	2000	31.3	04	0145	IICAST		
834	17	011	003	11/00/16	-000	31.3	0.4	0149	IIIC . ST		
034	17	914	105	11/00/72	2000	51.3	04	0198	CAST		NEW YORK OF THE PARTY OF THE PA
- 34	17	013	004	11/00/77	2400	31.9	04	026P	DCAST		
											The state of the s
03w	17	015	004	11/00/72	2400	31.9	04	059b	UCAST		
	17	010	004	11/00/72	2400	31.9	64	050b	OCAST		
03m	17	017	005	11/07/72	9400	15.0	03	059b	CLUMBA		
03W	17	018	005	11/07/72	0400	15.0	0.3	059b	CFDADA		Contractions.
-634	17	019	005	11/07/72	9460	25.0	65	050b	CLIMBA		1
634	17	050	003	11/0///5	4000	36.0	0.2	0500	CTUROL		The same of
634	17	120	006	11/07/72	0000	35.0	05	1095	TEAST		111
	17	220	076	11/07/12	4600	35.0	05	1442	OCAST	THE PERSON NAMED IN COLUMN 2 I	The state of the s
634	17	052	000	11/07/72	0800	35.0	05	1095	DEAST		
638	!!	920	006	11/07/72	0800	32.0	02	1093	DEAST		- Control of
-634	11	653	007	11/07/12	1500	31.9	100	1115	CAST		and the same of th
	::	43.	007	11/07/72	1200	21.4	06	113	OCAL!		
	11	96/	907	11/01/12	1500	31.4					

404	TP	INT	IDX	DATE	TIME	500	81	RWVD	A-10	HEATHER	VOY	10	INT	10×	DATE	TIME	SPD	84	RHVD	A-11	MEATHER
034	17	028	007	11/07/72	1200	31.0	06	1315	DEAST		-							-			
03m	17	050	004	11/07/72	1600	15.0	05	1315	CIMINA		034	19	200	050	11/09/77	1600	31.9	07	1575	DCAST	
424	17	030	000	11/07/72	1000	15.0	05	1515	CLUMBA		930	17	003	020	11/09/72	1600	31.9	07	1575	PEAST	
034	17	031	006	11/07/72	1600	15.4	05	1115	CFORDA		034	14	004	020	11/09/72	1600	11.0	07	1575	OCAST	
034	17	032	008	11/07/72	1600	37.0	05	1315	Chinhua		034	10	005	020	11/09/72	1600	11.0	07	15/5	DEAST	
624	14	033	004	11/01/72	2000	1.50	0.4	1545	CLUUDY		-014	10	007	050	11/09/12	1600	31.4	07	1575	DCAST	
				11/07/72							034	10	008	050	11/09/72	1600	11 0	0.7	1575	DEAST	
- 414	17	014	000	11/07/72	2000	13 1	0.4	1545	CLOUNT		034	19	009	150	11/04/17	2000	12.2	0.7	1629	DEAST	
	17	037	010	11/07/12	3000	11 0	0.4	1140	BICLOW!		-034	19	010	150	11/09/12	2000	32.2	07	1628	CCAST	-
				11/07/77							034	19	011	150	11/09/72	2000	32.2	07	1629	DEAST	
-010	17	014	010	11/07/12	2400	11 0	03	1100	PICLOU	17	034	19	012	150	11/09/72	2000	12.2	07	1624	MCAST	
03#	17	040	010	11/07/72	2400	11 0	03	1100	PICLOU) Y	-03#	19	013	150	11/04/12	2000	12.2	07	1020	DEAST	
034	17	041	011	11/08/72	0400	1.52	03	0000	PICLOU	*					11/09/12						
-034	17	042	011	11/08/72	0400	12.1	0.5	060P	PICLOU	· ·	034	19	015	150	11/09/72	2000	32.2	07	1620	MEAST	
03w	17	043	011	11/08/72	0400	1.58	03	060P	PICLOU	7	-030	19	016	150	11/09/72	2000	52.2	01	1424	ncest	-
03W	17	044	011	11/08/72	0400	1.56	03	9600	PICLOU	14					11/09/72						
-03m	17	045	012	11/08/72	0800	31.9	06	DASH	PICLOU	Y	03H	19	018	055	11/09/12	2400	52.0	07	0925	MEAST	
034	17	046	510	11/05/72	0000	31.9	06	OHSP	PICLOU	7	-03w	10	019	250	11/09/72	2400	12.0	07	0925	OCAST	
034	17	047	912	11/08/72	0800	31.9	00	ORSP	PTCLOU	Y	03W	19	050	055	11/09/72	2400	0.56	07	0925	CCAST	
-03H	17	048	912	11/08/72	0600	\$1.9	06	URSP	PTCI Hul	Y	034	19	150	250	11/09/12	2400	15.0	07	0925	DEAST	
03W	17	049	013	11/00/72	1200	31.7	06	967P	OCAST		-03m	19	250	250	11/09/72	2400	35.0	01	0923	DC 43T	-
034	17	050	015	11/08/72	1200	31.7	06	0679	NEAST		034	19	057	055	11/09/77	2400	52.0	01	0053	DCAST	
-03×	17	051	015	11/00/12	1200	31.7	06	9679	CCAST		_ 03M	19	024	055	11/09/72	2400	35.0	07	0923	UCAST	
03H	17	025	013	11/00/12	1200	31.7	06	06/P	CCAST		-03#	19	025	057	11/10/72	0400	31,5	00	0205	PICLDY	-
03m	17	055	014	11/08/77	1600	31.8	05	067P	OC45T		03*	14	050	053	11/10/72	0400	31.5	00	0502	PTCLD	
-03M	17	054	014	11/08/72	1600	31.4	05	0610	CAST	-	034	14	027	053	11/10/72	0400	31.5	00	0208	PTCLOY	
034	17	055	014	11/00/72	1600	31.8	05	067P	OCAST		-030	17	028	023	11/10/72	0400	31.5	00	0502	PICTUA	
624	17	056	014	11/08/72	1600	31.8	05	967P	CCAST		03*	::	024	021	11/10/72	1400	31.5	00	0502	PICLOY	
03#	17	057	015	11/08/72	2000	51.7	02	090P	DCAST -		- 41-	17	030	063	11/10/72	0400	31.3	00	0203	PICLOY	
034	17	070	015	11/08/12	5000	51.7	05	0000	CAST		034	10	031	023	11/10/72	0400	31.3	00	0503	PICLOY	
034	11	024	015	11/08/72	2000	51.7	05	0001	CAST		414	:	031	024	11/10/12	0000	31.3	44	0203	DETEL	
				11/00/12									014	024	11/10/72	0600	11.6	00	0443	DCAST	
				11/08/72							034	i	035	0. 4	11/10/72	0800	11 6	08	0643	DEAST	
414	.,	140	010	11/08/12	2000	31.7	03	0405	DEAST						11/10/72						
414	.,	000	414	11/04/72	2400	31.7	0.5	OOOP	OCAST -		-034-	19	037	024	11/10/72	0800	11.6	04	0693	DEAST .	
414		240	017	11/09/72	0400	11 0	05	1579	DICOL W		03W	19	038	450	11/10/72	0800	11.6	60	0495	OCAST	
-414	17	044	017	11/09/72	0400	11 0	05	1575	DICOLY		034	19	039	024	11/10/72	0000	31.6	06	0695	DEAST	
414	17	7.00	017	11/09/12	0400	11 0	05	1579	PICOLY		-03W-	19	040	024	11/10/72	0000	31.6	00	0495	OCAST -	
				11/09/12							03W	19	041	025	11/10/72	1200	31.2	00	06 15	OCAST	
-034	17		014	11/09/72	0800	11.0	04	1125	DEAST		034	19	042	025	11/10/72	1200	31.2	06	0655	CEAST	
034	17	070	016	11/09/12	0800	11.9	04	1125	DEAST		-034	19	043	075	11/10/72	1200	51.2	00	0455	CAST -	
034	17	071	018	11/09/72	0800	11 9	0.0	1125	DEAST		03W	19	044	025	11/10/72	1200	31.2	06	0655	CAST	
-034	17	972	018	11/09/12	0800	11.9	04	1125	OCAST		034	19	045	052	11/10/72	0051	51.2	00	0455	CCAST	
634	17	073	019	11/09/72	1200	12.0	06	1445	PEAST		-63W	19	046	025	11/10/72	1200	51.2	00	0455	DEAST	-
				11/09/72							034	14	047	025	11/10/72	1200	31.2	06	0655	DCAST	
-034	17	075	019	11/09/72	1200	32.0	06	1443	CAST		03H	19	048	025	11/10/72	1500	31.2	06	0653	CAST	
034	17	076	019	11/09/17	1200	32.0	06	1465	DCAST		-034	10	049	950	11/10/12	1600	30.1	04	1603	CLEAR -	
934	19	001	020	11/09/72	1600	31.9	07	1575	DEAST		034	19	050	050	11/10/72	1600	30.1	04	1003	CLEAR	
4000	25		7.32	The same of the sa	- Compared	TO PROPERTY.	370	marca /	PER SEL		MIA	19	051	026	11/10/72	1600	30 1	04	101.3	CIFAD	

VOY	TP	INT	10x	DATE	TIME	SPD	81	-	A-12		-EATHER	COMMENTS
034	19	052	026	11/10/72	1600	30.1	00	1005	CLEAR			SHIP PITCHING IN SHIP PITCHING IN SHIP PITCHING IN SHIP PITCHING IN SPRAY OVER NO. A SPRAY OVER NO. A SPRAY OVER NO. A SPRAY OVER NO. A
OHE	15	001	001	11/12/72	0400	32.8	04	0	LLOA	HA	14	
04E	51	200	001	11/12/72	0400	32.A	04	0	CLDA	**	14	
naF	15	003	100	11/12/72	0400	35.4	04	0	CLUA	H.A.	IN	
04E	21	004	001	11/15/75	0400	35.4	04	0	CLDY	HA	14	
300	51	005	005	11/15/11	0000	35.0	03	0000	OCAST		1	
04E	51	006	005	11/12/17	0800	35.0	07	090P	nc AST			
94E	51	00:	005	11/15/15	0500	35.0	03	9907	CAST			
)4F	51	008	200	11/12/12	0000	35.0	03	0405	HEAST			
146	51	004	003	11/15//5	1500	32.0	04	1017	CLOA			
380	51	010	003	11/15/15	1500	32.0	04	1016	CLOY			
141	61	011	003	11/12/17	1500	35.0	04	1015	CLDY			The state of the second
38		012	005	11/15/15	1200	35.0	04	101	CLUT			
146	21	013	000	11/12/12	1600	30,0	00	0479	PICTO			
141	11	014	004	11/12/12	1000	30.0	0.0	06/1	PICCO		-	
	21	013	004	11/12/12	1600	15.0	00	0616	PICLO			
345	.:	010	004	11/12/12	1000	37.0	60	0015	PICEO	٠		
	.:	017	005	11/1///2	2000	36.0	07	100	OCAST	0		SHIP PLICATED IN
	? :	010	005	11/12/17	2000	32.0	07	2001	05 487	D	212	Suite ettention to
		014	005	11/12/17	2000	32.0	07	0665	DEAST	0		Sulp placulus IN
-	::	020	003	11/12/12	2000	36.0	0,	000	DEAGT	-		SORAY MUCH MAN A
-		423	000	11/12/12	2400	32.0	00	OBOP	OCAST			SPRAY DUEN ACT
		022	900	11/12/12	3000	36.0	00	060	OCAST			SORAY OVER BUY AT
	21	073	000	11/12/17	2400	13.0	08	0400	OCAST		1	SPRAY DVER HOL AT
	*:	425	000	11/11/73	0000	13.0	41	000	BICLO			SPART LIVER DOWN AL
	31	024	007	11/11/72	0400	13.0	0.7	0820	#1C: 0	·	Contractor of	A Marian
AF	21	027	007	11/13/72	0400	12 0	07	OBZP	PTCLO	v		
4	21	028	007	11/13/72	0400	12.0	07	DROP	PICLO	·		
	31	129	007	11/11/72	0400	12 0	01	LIAP	CLOY	-		PITCH AND SLIGHT
4	21	010	008	11/13/72	2800	12.0	07	1 38P	CLDY			PITCH AND SLIGHT
30	21	031	008	11/13/72	0800	32.0	07	1 189	CLDY			PITCH AND SLIGHT
AE.	21	032	008	11/13/72	0000	12.0	07	ISAP	CLDY			PITCH AND SLIGHT
4E	21	033	009	11/15/72	1200	12.0	06	1450	CLDY			
at	21	034	009	11/15/72	1200	12.0	06	1459	CLOY			
46	21	035	009	11/13/72	1200	12.0	06	1450	CLOY.			PITCH AND SLIGHT PITCH AND ALIGHT PITCH AND ALIGHT PITCH AND ALIGHT
4E	21	036	009	11/13/72	1200	32.0	06	1438	CLUY			
4E	21	037	010	11/13/72	1600	12.0	07	160P	DCAST			
AE.	15	038	010	11/13/72	1600	\$2.0	07	166P	DEAST		-	
SP	15	039	010	11/13/72	1600	32.0	07	INOP	DCAST			
30	21	040	010	11/13/72	1600	32.0	07	166P	OCAST			
aF.	15	041	011	11/13/72	2000	32.0	07	1445	CLDY		-	
4F	21	045	011	11/13/72	2000	12.0	07	1445	CLUA			
AE.	21	045	011	11/13/72	2000	32.0	07	1495	CLDY			
4F	21	044	011	11/13/72	5000	12.0	07	1498	CLOY-		-	
380	21	045	012	11/13/72	2400	32.0	06	1495	CLOY			
30	51	046	012	11/13/72	2400	15.0	90	1495	CLDY			
30	51	047	912	11/13/77	5400	35.4	06	1495	CLDY			
4E	15	048	915	11/13/72	2400	15.0	06	1495	CLDY			

SE ALABITANTE CO

Des	200	1 200
C	7	MES
50	Garcon Mescol	2
į,	.l.	N Part
60	N.	100
E 10	1000 1000 1000	AND THE REAL PROPERTY.
1 11 11 11	100 m	100 M
		100
100	1	Sec.
6	Y	2

404	70	INT	tox	DATE	71 4 E	800	81	RWVD	A-13		EATHER	COMMENTS
				11/14/72								
				11/14/72								
				11/14/72								
946	57		014	11/14/72	0800	35.4	05	1155	PTCLD	4		
				11/14/72								
				11/14/72								
946	53	004	014	11/14/72	0000	35.0	05	1155	PICLO	*		
				11/10/72								
				11/10/72								
				11/14/72								
				11/14/72								
				11/14/72								
				11/14/72								
				11/14/72								
				11/14/72								
				11/14/72								
- 045	23	015	017	11/14/72	2000	32.0	05	1475	DCAST	PA		
				11/14/72								No.
				11/14/72								
				11/14/77								
				11/14/72								
340	53	020		11/14/72	2400	32.0	04	1475	DCAST	RA.	IN	
-146	23	150		11/15/72	0400	35.0	04	1023	CAST	RA	In	
				11/15/72								
				11/15/72								
-946	52	054	010	11/15/72	0400	35.0	04	1052	DCAST	RAI		
				11/15/72								LUM SMELL MIDING
300	5.2	050	050	11/15/72	0000	35.0	05	1052	DEAST	RA	N	LOW SHELL RIDING
-	53	027	050	11/15/72	0000	35.0	05	1052	CCAST	RAI	N	FOR SPETF HIGING
946	5.	050	050	11/15/72	0800	35.0	05	1059	OCAST	RAI	N	LOW SHELL RIDING
				11/15/72								
				11/15/77								
				11/15/72								
***	**	***	021	11/15/72	1200	36.0		1020				
				11/15/72								
				11/15/72								
				11/15/72								
				11/15/72								
946	23	038	021	11/15/72	2000	32.0	05	1285	DCAST	RAI		
				11/15/72								
				11/15/72								
340	23	001	070	11/15/72	2400	32.0		1068	CEAST	RAI	IN .	
				11/15/72								
300	52	043	074	11/15/72	2400	32.0		1005	DCAST	RAI	N	
300	23	044	024	11/15/72	2400	32.0	06	1065	DCAST	RAI		
-	53-	005	025	11/10/72	0400	32.0		0785	CAST	RAI		
				11/10/72								
340	52	047	025	11/10/72	0400	32.0		0783	DCAST	BAI		

Y 0 Y	TP	INT	10x	DATE	TIME	300	-	RWYD	A-14	HEATHER	COMMENTS
) 4F	23	048	075	11/16/72	0400	32.0	06	0785	DCAST	RAIN	
300	53	049	450	11/16/72 11/16/72 11/16/72 11/16/72 11/16/72 11/16/72 11/16/72	0000		06	1205	DEAST	RAIN	
HE.	53	050	076	11/16/72	0000		00	1205	UCAST	RAIN	·
42	53	051	024	11/16/72	0000		06	1502	CAST	RAIN	
340	52	052	920	11/16/12	0000		00	1508	DCAST	RAIN	
4E	52	055	627	11/16/72	1500		05	1205	CCAST	1	
4E	5.2	054	120	11/16/77	1200		05	1205	CCAST		
145	53	055	027	11/16/77	1500		05	1502	CCAST		
	53	070	021	11/10/15	1200	40 .	0.5	1502	HEAST		
	63	001	001	11/19/72	Saun		n/	ande	CHI AND I	MAIN	
		200	001	11/19/72	3000	30.0	47	0500	OCAST	DAIL	
++4	25	003	001	11/19/72	2400	29.0	A7	4549	OCAST	PAIA	
-	55	004	001	11/20/12	0000	20 0	0	OSOP	DEAST	RAIN	
	56	000	002	11/20/72	0400	29 4	07	0500	DCAST	RAIN	
***	35	007	002	11/20/12	0400	29.0	07	OSOP	DEAST	HAIN	
-	36	000	002	11/20/77	0400	20 4	07	CSUP	CICAST	RAIN	
***	34	009	006	11/20/72	0600	29.0	08	0	CLDY		SWELLS ON HUM SP
-	25	010	003	11/20/12	0800	29.0	08		CLDY		SWELLS ON ROW SE
	25	011	005	11/20/72	0800	20.0		0	CLDY		SHELLS ON HUY SP
											QUELLA IN HUM SE
	25	013	004	11/20/72	1200	25.0	09	DONP	PICLO		SPEED REDUCED
	25	014	004	11/20/12	1200	25.0	09	DORP	PICLO		SPEED REDUCED
44	25	015	-004	11/20/72	1500	25.0	14	ORSP	PICLO		SPEED REDUCED_
	25	016	004	11/20/72	1200	25.0	09	9000	PICLD		SPEED REDUCED
44	25	017	005	11/20/12	1400	21.0	10	0205	PTCLO		PITCHING SLAM RE
4#	25	010	105	11/20/17	1400	21.0	10	0708	PICLD		PLICHING SLAY HE
44	25	019	005	11/70/77	1400	21.0	10	0202	PICLE		Lifutue of a. w.
-	52	050	005	11/20/72	1400	51.0	10	6050	PICTO		PITCHING SLAM HE
	25	120	000	11/20/72	1640	51.0	10	0315	PICLO		
-	52	220	000	21/02/11	1600	23.0	10	0212	PICID		
				11/20/72							
41		974	004	11/20/72	1600	23.0	10	0115	bicf or		
•	5.3	655	011	11/20/12	16.00	61.0	10	0428	PICLO		PITCH HEAVY SPRA
••	5.2	050	011/	11/20/72	1800	61.0	10	0052	PICLO		PITCH HEAVY SPRA
				11/20/72							PITCH HEAVY SPHA
•		050	007	11/20/72	1000	21,0	10	6459	PICLO		PITCH HEAVY SPHA
-	**		000	11/20/12	2000		: "	0426	PICLO		PITCH HEAVY SPRA
-	*	710	***	11/20/15	2000	10.0	10	0025	PICLO		PITCH HEAVY SPRA
-	56	***	004	11/20/72	2000	19.0	10	0428	PICLO		PITCH HEAVY SPRA
-	*	411	000	11/20/72	2400	26 0	09	0025	PICLD		EASING OCCAS. S.
	25	030	000	11/20/12	2400	26.0	09	0025	PICLO	A Treatment	EASING OCCAS. SI
-	25	035	000	11/20/12	2400	26.0	04	0425	PICLO	164	EASING UCCAS. S.
	25	034	009	11/20/72	2400	20.0	09	0425	PICLD		EABING OCCAS, SP
	25	037	010	11/21/72	0400	27.0	05	0425	CAST		
	25	030	010	11/21/12	0000	27.0	05	0425	UCAST		
	25	039	010	11/21/72	0400	27.0	05	0475	UCAST		
	25	040	010	11/21/72	0400	27.0	05	0425	DEAST		
	25	041	011	11/21/12	9000	29.0		0675	CLDY		ROLLING 5 DEG IN

404	*	INT	IOX	DATE	TIME	300	ON		A-15	MEATHER	COMMENTS
***	25	500	011	11/21/72	0800	20.0		0675	CLDY		ROLLING 5 DEG 1
				11/21/72							MOLLING S DEG IN
				11/21/72							MOLLING 5 DEG 1
	52	045	015	11/21/72	1500	30.0	15	1555	CAST	LT HAIN	
	55	000	215	11/51/15	1500	30.0	05	1555	OCAST	LT RAIN	
		047	012	11/21/72	1500	30.0	05	1553	OCAST	LI RAIN	
04.	::	048	015	11/21/72	1200	30.0	07	1775	DEAST	LT HAIM	
	**	050	013	11/51/15	1600	29.0	07	1553	DCAST		
***	56	451	413	11/21/72	1400	29 0	07	1550	OCART		
***	34	052	411	11/21/72	1400	20 4	07	1555	DEAST		
-	25	454	010	11/21/12	2000	29 0	07	1555	CIDY		BOLLING IN-BHELL
	25	054	014	11/21/72	2000	29.0	07	1555	CLOY		ROLLING IN SHELL
	25	055	014	11/71/77	2000	29.0	07	1553	CLOY		ROLLING IN SHELL
	25	056	014	11/71/72	2000	29.0	07	1553	CLOY		
	25	057	015	11/21/72	2400	29.0	08	1555	PCAST		
	25	058	015	11/21/72	2400	29.0		1553	OCAST		
	25	059	015	11/21/72	2400	29.0	08	1558	OCAST		
	25	000	015	11/21/72	2400	54.0	08	1555	DCAST		
				11/22/11							
-04-	25	200	016	11/22/12	0400	20.0	07	1553	UCAST		
				11/22/11							
				11/22/72							
-040	::	065	017	11/22/12	0600	50.0	07	1558	PTCDY		
		***	017	11/22/12	0000	24.0	07	1555	PTCDY		
	**	00/	017	11/22/72	0000	24.0	07	1223	PICDY		
44-	**	***	017	11/22/72	0000	24.0	01	1770	FILDY		
***	**	001	010	11/55/15	1200	29.0	07	1770	CLEAR		
	27	441	414	11/22/12	1200	30 4	07	1770	CLEAR		
***	27	004	014	11/22/12	1200	20 0	07	1779	CLEAR		
	27	005	019	11/22/12	1400	20.0	0.7	OTAP	CCAST		
-	27-		050	11/22/11	2000	30.0	07	0253	CLOY		
	27	010	020	11/22/12	2000	30.0	07	0253	CLOY		
	27	011	020	11/22/17	2000	30.0	07	0255	CLOY		
-	27	912	020	11/22/17	2000	30.0	07	0258	CLOY -		
	27	015	150	11/22/12	2400	30.0	05	0705	OCAST		
				11/22/12							
444	51	015	451	11/25/15	5400	30.0	05	0705	OCAST		
				11/55/15							
				11/23/72							
-	•:-	.10	220	11/23/12	0400	30.0	04	0258	OCAST	W-1-1	
944	::	414	220	11/23/72	-400	30.0	04	0255	DEAST		
	27	020	330	11/23/72	0400	30.0	04	0255	DEAST		
	**	423	023	21/52/11	0000	0.75	0,5	0273	DELAST		
	**	150	421	11/57/15	2000	20.0	03	0255	00-31		
-	27	424	021	11/53/15	0800	20 0	41	0255	DEAST		
	27	025	020	11/23/72	1200	29.0	07	1779	DEAST		PORCE 7 WEATHER
	••			11/23/72							FORCE 7 HEATHER

404	10	INT	10x	DATE	TIME	500	84	RW40	A-16	MEATHER	COMMENTS
044	27	027	024	11/23/72	1200	29.0	07	1779	ncast		FORCE 7 WEATHER
044	27	950	024	11/25/72	1200	20.0	07	171P	OCAST		FORCE 7 AFATHER
	27	029	025	11/23/12	1600	30.0	09	177P	DEAST	HAIN	RIDING FASY MEAT
				11/23/12							RIDING FASY HEAT
				11/23/12							PIDING EAST WEAT
				11/23/72							MIDING EASY WEAT
				11/23/72							MOLLING HEAVY 15
				11/23/72							RULLING HEAVY 15
				11/53/15							ROLLING HLAVY 15
				11/23/12							MOLLING HEAVY
				11/53/15							HOLLING HEAVY
				11/25/17							ROLLING HEAVY
				11/25/72							ROLLING HEAVY
				11/53/15							ROLLING HEAVY
				11/23/12							RULLING HEAVY
	"	043	950	11/52/15	2200	20.0	10	0019	DEALT	2414	ROLLING HEAVY
***		***	020	11/23/72	2000	20.0	10	0715	DEAST	2414	MUDERATE HULL
				11/23/72							MODERATE ROLL
				11/25/72							MODERATE HOLL
				11/23/72							MUDERATE RULL
***	37	000	010	11/24/72	0400	20.0	0.8	0715	HEAST	WAIN	RIDING LASY
	37	050	030	11/24/72	0000	29.0	00	0715	CCAST	PAIN	RIDING EASY
-444	21	051	010	11/24/72	0000	29.0	80	0715	DEAST	WAIN	MIDING LASY
				11/24/72							RIDING EASY.
				11/24/72							
				11/24/77							
				11/24/72							
	27	056	031	11/24/72	0600	0.85	05	0488	CLOY		
-044	-27	057	032	11/24/72	1200	28.0	05	2235	CLOY		
	27	058	032	11/24/77	1500	24.0	05	0218	CFDA		
	27	059	032	11/24/72	1200	28.0	05	0233	CLDY		
				11/24/72						the second of	
OSE	24	001	001	11/26/12	0400		03	140	CCAST	RAIN	
05€	24	200	100	11/26/72	0400		03	180	CCAST	HAIN	
- 056	-54	003	100	11/20/72	0400		03	180	CCLST	RAIN	
				11/26/17							
				11/56/15							
				11/50/15							
				11/26/12							
				11/26/72							*
				11/26/15							
				11/26/72							
0.56	54	611	904	11/56/15	1500	30.0	10	0112	CEAST	MALN	
				11/26/72							
				11/20/72							
				11/26/72							
				11/26/72							
456		*::	904	11/20/12	3000	10.0		1003	DEAST	9414	ROLLING HEAVY
A 35			002	11/16/14	5000	30.0		4-03			MARCING MENAL

404	10	**17	101	DATE	TIME	300	81	RHVD	A-17	HEATHER	COMMENTS
055	29	018	005	11/26/12	2000	30.0	09	0903	DCAST	RAIN	RULLING HEAVY
05E	29	019	005	11/26/12	2000	30.0	09	0908	DEAST	RAIN	RULLING HEAVY
OSE	29	050	005	11/20/72	2000	30.0	00	0908	DEAST	RAIN	
OSE	50	150	000	11/26/72	5500	30.0	04	0888	DCAST	RAIN	RULLING HEAVY
05F	54	055	006	11/26/72	5500	30.0	00	0883	UCAST	HAIN	HOLLING HEAVY
				11/26/12							- ROLLING HEAVY-
				11/26/72							ROLLING HEAVY
				11/26/12							EASING
				11/20/12							EASING
05E	29	120	007	11/26/72	5400	30.0	0.6	0755	OCAST	HAIN	EASING
				11/26/72							EASING
026	54	054	000	11/51/15	0400	30.0	01	0/55	HEAST	HAIN	
025	54	0 10	008	11/21/12	0400	30.0	07	0/55	CLA	ALIN	
026		031	000	11/27/12	9400	30.0	07	0/33	OCAS!	9414	
956		032	000	11/27/72	0400	30.0	21	0775	OCASI	****	
				11/27/12							
				11/27/72							
				11/21/72							
OSE	29	035	010	11/27/12	1200	50.0	05	0755	DCAST		
-05F-	29	039	010	11/51/15	1200	30.0	05	0755	DEAST		
05F	29	040	010	11/27/72	1200	10.0	05	0758	DCAST		
OSE	29	041	011	11/27/12	1000	0	04	0753	PTCLDY		HOVE TO
ASE	30	042	411	11/27/73	1-00		04	0755	PICIDI		- HOVE-TO
OSE	29	045	011	11/27/72	1600	0	04	0755	PICLO		HOVE TO
OSE	54	044	011	11/27/12	1600	. 0	04	0755	PTCLO		HOVE TO
OSE	29	045	510	11/27/72	5000		06	0985	DCAST		
OSE	29	046	015	11/27/77	5000	0	06	0985	OCAST		HOVE Tu
OSE	54	047	210	11/27/72	5000	0	06	0965	DCAST		HOVE TO
05E	54	048	210	11/27/72	2000	- 0	00	0985	UCAST		HOVE TO
05E	50	049	013	11/51/15	2400	0	06	0985	DCAST		HOVE TO
05E	54	050	013	11/77/72	2400	0	0.0	0985	OCASI		HOVE TO
-02E	54	051	013	11/27/12	2400	. 0					MUVE TO
026	29	052	013	11/27/72	2400	0			OCAST		START-STOP
350	54	053	014	11/20/72	0400						START-STOP-
				11/25/12					OCAST		START-STOP
				11/24/72					OCAST		START-STOP
				11/28/72							HOYE TO
				11/20/72					DEAST		HOVE TO .
				11/20/72					DCAST		HOVE TO
				11/28/12							
				11/24/72					CLEAR		HOVE TO
				11/28/72					CLEAR		MOVE TO
				11/24/72					CLEAR		MOVE TO
				11/24/72					CLEAR		HOVE TO
ASE	11	001	017	11/28/72	1400	•	04	1414	CIFAR		MOVE TO START 9
				11/29/77							
058	31	003	017	11/28/12	1600	0	04	1433	CLFAR		HOVE TO START & I
05F	31	994	017	11/28/72	1600		04	1455	CLEAR		HOVE TO START 9

404	77	INT	IDX	DATE	TIME	SPD	84	RWVD	A-18	HEATHER	COMMENTS
OSE	31	005	018	11/28/12	2000	09.0	04	1435	CLEAR		WETS STAD ENGTA
OSF	31	006	018	11/28/12	2000	09.0	04	1455	CLEAR		9 ATS STAD ENGIN
-05F	31	-007	018	11/24/12	5000	09.0	04	1453	CLEAR -		- NIS STAD ENGIN
OSE	31	008	018	11/28/72	2000	09.0	04	1453	CLEAR		WIS STHU ENGLA
OSF	31	009	019	11/28/72	2400	15.0	0 5	1655	CIFAR		15 KTS STHO DALY
-ASF	31	010	019	11/24/12	2400	13.0	05	1655	CLIAR		
05E	31	011	010	11/28/72	2000	13.0	03	1455	CLFAR		13 KTS STED TINE T
05E	11	012	010	11/28/72	2400	13.0	0.5	1448	CLEAR		13 KTS STHO PINEY
-056	31	013	050	11/29/17	0400	15.0	03	1700	CLEAR		- STED ENGINE ONLY
USE	31	014	050	11/29/15	0400	15.0	03	1700	CLFAR		
05E	31	015	050	11/29/12	0400	15.0	0.5	1700	CLEAR		STAD ENGINE ONLY
-026-	31	010	050	11/54/15	0400	11.0	0.5	1700	CLFAR		STHO ENGINE DIN Y
055	31	017	120	11/29/12	0000	13.0	04	14/1	CLEAR		STED ENGINE ONLY
956	**	010	021	11/54/15	2600	13.0	04	14/5	CLEAR		STHO ENGINE ONLY
956	?!	014	021	11/29/12	0000	13.0	04	14/1	CILAR		STED FAGINE ONLY
				11/29/12							STHO ENGINE THE
ASE	*	023	422	11/29/72	1200	11.0	04	1479	CLEAR		STED ENGINE MIL
				11/29/72							STAD ENGINE ONL
											STAD ENGINE ONLY
OSE	11	026	021	11/29/72	1600	15.0	0.4	197P	CLEAR		STOD ENGINE ONLY
ASE	31	027	150	11/29/72	1600	13.0	04	1479	CLFAR		STOD ENGINE ONLY
- 340	31	028	023	11/29/12	1600	13.0	04	1974	CLE AR		STED ENGINE DULY
OSE	31	929	024	11/29/72	2000	15.0	04	16/5	PICLDY		STOP ENGINE ONLY
OSE	31	030	024	11/29/72	2000	13.0	04	1675	PICLDY		STAD ENGINE ONLY
-356	11	031	224	11/29/12	2000	15.0	04	1675	PICLOY	-	STED ENGINE DNI. Y
OSE	31	035	024	11/29/12	2000	13.0	04	1675	PTCLOY		STED ENGINE ONLY
SE	31	033	025	11/29/12	2400	13.0	05	1458	PICLDY		STAD ENGINE DIE Y
455	11-	034	025	11/29/72	2400	11.0	05	1445	PICIDY	Section Sections - Sections	STOD ENGIAL ONLY
OSE	31	035	025	11/24/77	2400	13.0	05	1455	PTCLOY		STOU ENGINE ONLY
05E	31	036	025	11/54/15	2400	13.0	05	1455	PTCLDY		STED ENGINE ONLY
-025		037	026	11/30/12	0400	13.0	0.0	1112	DCAST .	CAIN	ENGINE TINE
OSE	31	038	050	11/30/72	0400	13.0	0.0	1115	DEAST &	MIN	- ENGINE ONL
OSE	31	039	050	11/30/72	0400	13.0	00	1115	CCAST A	MIN	STHO ENGINE ONLY
458-	31-	040	950	11/30/72	0400	13.0	76	1113	OCAST A	AIN	STED ENGINE ONLY
02E	31	001	027	11/30/72	0800	15.0	0.6	16/3	OCAST A	MIN	STRO ENGINE ONLY
936	**	045	120	11/30/72	0000	13.0	00	10/5	OCASI A	MIN	STOU ENGINE ONLY
436	::-	***	120	11/30/72	0000	15.0	06	1675	OCAST .		STED ENGINE ONLY
936	21	***	007	11/30/12	4404	15.0	00	1015	OCART .		STHO ENGINE ONLY
***	::	047	020	11/30//2	1200	11.0	0.6	14/5	CCAST		STOD ENGINE CALL
456	**	047	428	11/30/72	1200	::.	00	1675	DEAST		STRO ENGINE ONLY
456	*		026	11/30/72	1200	11.0	06	1675	CCAST		STOO ENGINE ONLY
450	**	001	010	15/01/15	1200	11.0	01	1218	PICLOY		STHO ENGINE UNLY
124	**	002	414	12/01/72	1200	11.0	67	121P	PICLOY		STED ENGINE ONLY
456	11	005	014	12/01/72	1200	13.0	07	1210	PTCLDY		STOO ENGINE UNLY
-025	33	004	0.24	12/01/12	1500	13.0	0.7	1516	LICTO.	No. of Concession, Name and Post Office and Publishers and	STOU ENGINE UNLY
456	33	005	015	12/01/72	1000	13.0	07	1079	DCAST.		STOD ENGINE THEY
	**	006	035	12/01/72	1600	13.0	01	107P	OCAST		STOD ENGINE ONLY

VOV	10	INT	TOX	DATE	TIME	3P0	81	HW40	A-19	MEATHER		COMME	NTS
ase	11	007	035	12/01/72	1600	13.0	07	1079	DEAST	51	80	ENGIFF	ONL
OSF	33	008	055	12/01/72	1600	13.0	07	1072	DEAST	3		ENGTHE	
OSF	33	009	036	12/01/72	2000	15.0	07	095P	DCAST -		180	ENGINE	nat
05E	11	010	016	15/11/15	2000	13.0	07	0954	CCAST	51	80	CHGINE	rest
05E	33	011	036	12/01/72	2000	13.0	0.7	0959	nc 431	51	80	ENGINE	HINL
OSE	33	015	036	12/01/72	2000	13.0	07	0954	DE AST			ENGINE	
OSE	13	013	037	12/01/72	2400	13.0	0.7	OGAL	PICLDY			ENGINE	
OSE	33	014	037	12/01/12	2400	13.0	0.7	OGAP	PTCLDY	51		ENGTHE	
OSE	33	015	037	12/01/72	2400	13.0	07	0446	PTCLDY			FHEINE	
OSE	33	016	037	12/01/72	2400	13.0	07	0445	PTCLOY			ENGINE	
05E	33	017	038	15/05/15	0400	13.0	0.7	0949	PICLOY	31		ENGINE	
OSF	13	018	0.19	15105115	0400	13.0	0.1	0444	BILLFUA	51		ENGINE	
05E	33	019	018	15/05/15	0400	13.0	07	0041,	BICTOA	31		ENGINE	
05E	33	050	038	12/02/12	0400	13.0	07	0495	PTCLOY	31		ENGINE	
				15/05/15								ENGINE	
925	33	055	034	15/05/15	0800	13.0	0/	1046	PICLOY	31		ENGTHE	
350	33	053	039	15/05/15	0400	13.0	07	0949	PICLOY	31		ENGINE	
925	33	024	010	15/05/15	0400	15.0	01	0949	PICCOA	51		ENGINE	
350	;;	053	040	12/02/12 12/02/12 12/02/12 12/02/12 12/02/12	1500	17.0	01	1150	MILLEDA	31		ENGINE	
350	**	026	040	15/05/15	1500	13.0	07	1136	PICLOT	31		ENGINE	
435	**	021	040	12/02/12	1200	13.0	07	1176	PICLO	3		ENGINE	
350	33	020	040	12/02/12	1200	13.0	07	1150	PICEDY			ENGINE	
935	**	024	041	15/05/15	1000	14.0	07	1150	PICLOT			ENGINE	
ASE	**	030	041	15/05/15	1600	14.0	07	1150	PICLOY	41		ENGTHE	
455	**	032	041	12/02/17	1.00	10.0	07	1150	BILLDA			ENGINE	
455	-11	411	041	12/04/72	2000	10.0	05	1200	OCAST.			ENGINE	
455	**	030	042	15/05/15	2000	14 0	05	1308	OCAGT	41		ENGINE	
	22		2022		(E) E) (E) (E)	71:42 (10)		E				ENGINE	
455	· ii	014	042	15/05/15	2000	14.0	05	1200	DCAST-			L.GINE	
OSE	33	037	043	12/02/72	2400	14.0	05	144P	DEAST	51		ENGINE	
												ENGINE	
05E	33	039	543	15/05/15	2400	14.0	05	1849	DEAST -			ENGINE	
OSE	35	040	043	12/02/12	2400	14.0	05	1449	DEAS.	51		ENGINE	
												ENGINE	ON
	-11	443		. 2 / 4 1 / 7 3	0000		45	1040	DICION		40	ENGINE	Cliek
OSE	33	045	044	12/03/72	0400	14.0	05	144P	PTCLOT	51	80	ENGINE	DNL
05E	33	044	044	12/03/72	0400	14.0	05	1440	PTCLDY			ENGINE	
05F.	33	045	045	12/03/72	0000	14.0	04	1670	CLOY				
SE.	33	040	045	12/03/72	0800	14.0	04	16/P	CLOY	51		ENGINE	
OSE	33	047	045	12/03/72	0000	14.0	04	167P	CLOY	51	80	ENGINE	DNL
ORE	47	001	001	01/30/75	2400			-	CLEAR -				-
BBE	47	200	001	01/30/73 01/30/73 01/30/73	2400				CLEAR				
OBE	47	003	001	01/30/73	2400				CLFAR				
380	47	004	001	01/30/73	2400		-	-	CLEAR -				-
				01/31/73									
				01/31/73									
905	47	007	005	01/11/73	1400	24.6	02	ONIP	CLEAR		-		-
				01/31/73									
705	47	004	062	01/11/73	ueud	54.0	90	1340	Cros				

YOY	TP	INT	IOX	DATE	TIME	500	-	-	A-20	HEATHER	VOY	1-	INT	Inx	DATE	TIME	SPD	81	RHVD		MEATHER
											084	51	009	033	02/08/73	1600	24.8	06	025P	PT CL	PY
900	47	010	003	01/31/73	0000	74.6	00	1345	CLDY		084	51	010	033	02/08/13	1000	24.4	06	025P	PT CL	7
000	::	011	003	01/31/73	0800	24.6	00	1740	CLOY		-00=	51	011	033	02/08/73	1600	24.8	06	052b	PT CL) Y
				01/31/73							061	51	015	033	02/08/73	1600	24.8	06	025P	PT CLI	7
				25/11/10							00"	51	013	034	02/08/73	Sugo	24.8	0.0	0158	PT CLI	74
				01/31/73							- 000	21	014	034	02/08/73	5000	54.8	06	0152	PT CL	DY
				01/31/73							08*	51	015	034	02/08/73	5000	24.8	06	0125	PT CL	Y
				** *** ***		20 4		1670			00.	21	016	034	05/08/11	5000	54.4	06	0175	PT CLI	74
OAF	47	018	005	01/11/73	1600	24.6	07	1574	SNOW		00=	21	01/	035	02/00/73	2400	24.8	05	0655	PT CL	7
OSE	47	019	005	01/51/73	1600	24.6	07	157P	SNOW		00-	31	010	035	02/08/73	2400	24.4	05	0655	PT CL	7
OFF	47	020	005	01/31/73	1000	24.6	07	1570	SNI)W		00-	51	020	015	02/08/73	2400	20.0	05	0622	PT CLI	
				01/51/73							004	51	021	014	02/09/73	2400	24.6	42	0022	PT CLI	,
OBE	47	250	006	01/31/73	2000	8.45	08	157P	SNOW			51	455	036	02/09/73	0400	24 6	45	0055	07 61	
985	47	650	006	01/31/73	2000	24.6	08	157P	SHOW			51	021	010	02/09/73	0400	24 8	45	0466	OT CL	
- OBE	47	024	006	01/31/73	2000	24.6	98	157P	SNOW	-	284	51	024	034	02/09/73	0400	24 8	05	0655	PT CL	
				01/31//3						H	084	51	025	037	02/09/73	0800	24.8	05	0655	PT CL	
				01/31/73								-51	026	037	02/09/73	0800	24.4	25	0658	PT CL	· -
				01/31/73						-	084	51	027	037	11/40/50	0.000	24 8	05	0455	PT F1	
985	47	059	007	01/51/73	2000	24.6	08	1315	SNOW		284	51	028	037	02/04/73	0800	8.85	05	2440	PT CL	
OBF	47	050	005	02/01/73	0400	24.6	00	131P	SHOW		-08*	51	029	038	02/09/73	1200	24.9	05	1105	PT CLE	· -
OBE	87	030	000	02/01/73	0400	24.6	08	1315	SHOW -	-	08*	51	030	038	02/09/73	1200	24.9	05	1105	PT CLE	*
				02/01/73							08W	51	031	038	02/09/73	1200	24.9	05	1105	PT CL	*
				02/01/73								51	035	034	02/09/73	1200	24.9	05	1105	PT CLE	Y
				02/01/73							08M	51	033	939	02/09/73	1000	24.9	05	1105	PT CLE	*
				02/01/73							08#	51	034	019	02/04/73	1600	24.9	05	1105	PT CLE	*
				02/01/73								-51	035	039	02/09/73	1600	24.9	05	1105	PT CLE	·
905	47	016	004	02/01/73	0000	50.0	00	1310	SNOK	-	08W	51	036	039	02/09/73	1000	24.9	05	1105	PT CLC	*
985	47	037	010	02/01/73	1500	20.6	08	1310	340#		08#	51	037	040	02/09/73	2000	24.9	04	1325	PT CLO	Y
986	47	038	010	02/01/73	1500	20.0	0.0	1315	MOM			51	038	040	02/09/73	2000	24.9	04	1358	PT CLO	¥
				02/01/75								51	039	040	02/09/73	2000	24.9	04	1329	PT CLO	*
				02/01/73							084	51	040	040	02/09/73	5000	24.9	04	1325	PT CLO	Y
900	41	041	011	02/01/73	1000	24.0	00	127	5404		-00+	51	041	441	27109173	5000	50.0	114	1415	PT CLI	¥
300		042	911	02/01/73	1000	24.6	00	1200	BHOH.		484	51	045	041	45164112	5400	54.4	54	1035	PT CLE	*
900	**	043	011	02/01/73	1000	24.6		1200			081	51	043	041	02/09/73	5400	50.0	04	1438	PT CLO	*
				02/01/73							084	51-	044	041	02/09/73	5400	54.0	04	1435	PT CLO	Y
				02/01/73							000	51	045	045	02/10/73	0400	24.9	05	059P	PT CLO	*
445	**	047	012	02/01/73	2000	25 6	0.0	1290	*****		004	21	040	045	02/10//3	0400	24,9	05	0204	PT CLD	*
446			012	02/01/73	2000	25 6	44	1200	-		- 08*	21	047	042	02/10/71	0000	54,0	05	054P	PT CLD	Y
ARE		049		02/01/73	2400	25 6	**	1100	-		00=	33	0.0	945	02/10/73	9400	54.4	02	059P	PT CLD	Y
AAF		050	***	02/01/73	2400	25.0	08	1199	-		60**	21	044	045	02/10//3	0000	50.4	0.4	104P	PT CLD	*
ARE	47	051	411	02/01/73	2400	25 0		1190	-		-00*	21	070	043	02/10//3	0800	24,9	04	1048	PT CLO	¥
				02/01/73							000	21	463	043	02/10/73	0000	24,4	04	LOGP	PT CLO	1
				02/08/73						*	008	21	461	043	02/10/73	0800	70.4	04	1045	P. CLO	1
										1	000	61	054	044	02/10/73	1700	24.0	00	98.40	PI CLD	
	51	004	031	02/00/73	0800	24.8	00	9050	PT CLO	•	904	51	055	044	02/10//3	1500	24.4	00	0020	PI CLO	
				02/08/73								51	454	000	02/10/73	1200	20.0	0.0	0625	PI CLD	
				02/00/13							00-	51	057	005	02/10/73	1400	25 6	04	4836	er cro	-
				02/08/73							00.	si	058	045	02/10/73	1.00	25.0	-	0830	CLOY	
				02/06/13							00"		.,.	443	art tali?	1040	c2.0	44	ADEL	FFOT	

-	10	141	10x	DATE	TIME	SPD	BH	RWVD	A-	22	WEATHER
	51	059	445	02/10/73	1600	25.0	06	9880	CLOY		
	51	060	045	12/10/73	1600	25.0	06	9580	CLDY		
	51	041	046	02/10/73	2000	25.0	00	037P	CLDY	-	
		540	444	02/10/13	2000	25.0	00	0374	CLOA		
08×	51		04A	02/10/73	2000	25.0	06	037P	CLDY		
	51	044	044	02/10/73	2000	25.0	00	037P	CLDY		
08M	51	045	041	02/10/73	2400	52.0	05	0370	CLDY		
084	51	000	047	02/10/73	2400	25.0	05	037	CLDY		
-08#	51	047	047	12/10/75	2000	25.0	02	0210	CLD	-	
08.	51	068	047	02/10/73	2400	25.0	0.2	017P	CLD	٠.	
	53	001	048	12/11/73	0400	25.0	04	OAZP	CLD		
	53	200	048	02/11/73	0400	25.0	04	0829	CLD	-	
08.	53	005	DAR	02/11/73	0400	25.0	04	ORZP	CLO		
084	53	004	04A	02/11/73	0400	25.0	04	OWSP	CLD		
- 08=	53	0.05	049	02/11/73	0800	55.0		4540			
	53	006	049	02/11/73	0800	55.0	04	0825	CLO		
	53	007	049	02/11/73	0600	25.0	04	0 K 2 P	CLD		
-084	53	008	446	02/11/75	0800	25.0	04	0456	CLD		
084	53	000	050	02/11/73	1500	25.0	06	0 - 2 -	CLD		
084	53	010	050	02/11/75	1500	25.0	0.0	0 7 2 7	CLD		
-08×	53	011	050	02/11/75	1500	55.0	02	0025	200		
084	53	015	050	02/11/73	1200	25.0	0.5	0121	CLO		ues
08*	53	013	051	02/11/73	1000	50.0	64	9050	100	1115	
08=	53	014	051	02/11/73	1600	20.0	0.4	0825	FOC	01	wat
064	51	015	051	02/11/73	1000	20.0	04	0020	100	06	LSF
084	53	016	051	02/11/73	1600	20.0	04	LAGE	FOG	06	
- 08*	-53	017	052	02/11/73	2000	20.0	03	1049	FDE		
084	53	018	052	02/11/73	2000	20.0	0.5	1000	FOG		
08.	53	014	052	02/11/73	2000	20.0	0.5	1000	FOE		
08=	-53	050	056	02/11/73	2000	20.0	03	1279	FOG		
084	33	021	033	02/11/73	2000	20 0	0 5	1279	FOG		
084	23	022	073	02/11/73	2400	20.0	03	1279	FOG		
00*	- 23	023	053	02/11/73	100	20.0	0.3	1279	FOG		
00*	2.7	024	050	02/12/73	0400	20 9	0.3	1278	FOG	1	FTING
100	61	025	050	02/12/73	0400	24.9	03	1279	FUG	L	FTING
004	- 23	027	454	02/12/73	0400	24.9	0.3	1279	FOG	L	IFT146
064	61	024	054	02/12/73	0400	24.9	03	1218	+06	L	IFTING
00-		029	055	02/12/73	0600	24.9	0.4	9580	PT	CLI	DY
	53	030	055	12/12/73	0800	24.9	0.4	0829	PT	CLI	DY
		631	455	02/12/73	0800	24.9	0.4	0825	PT	CL	7
	53	037	055	02112177	0800	24.9	0.4	065		CF	04
	51	017	054	02/12/71	1200	24.9	0.0	150	PI	CL	DY
	54	0.34	056	02/12/73	1200	24.4	0.0	150	PT	CL	DY
	51	015	054	17/5/150	1200	24.9	0.0	150	PI	CL	UT
	51	036	056	02/12/77	1200	24.9	00	1501	PT	CL	04
081	4 51	0.17	051	17/5/1/50	1000	24.5	0.0	150	PT	CL	O.A.
	. 51	0.24	4 057	1 12/12/71	1600	24.9	00	150	PT	CL	04
	. 53	030	051	17/51/50	1600	24.	00	150	PI	CL	DY
100				02/12/73		20 0		1506	PT	CL	DY

VOY	7	INT	IDX	DATE	TIME	300	84	RHYD	A-23	MEATHER	COMMENTS
-000	-53	-041	458	02/12/73	2000	24.9	05	1205	F06 #1	91	
	53	042	058	92/12/73	2000	24.9	05	1203	FOG +1	31	
084	53	043	058	02/12/73	5000	24.9	05	1502	FOG MI	31	
				17151150							
	33	045	059	02/12/13	5400	24,9	05	0975	FOG MI	31	
	33	046	059	02/12/73	5400	24.4	05	0975	FOG MI	31	
***	23	047	054	02/12/73	2400	24.4	05	0975	FOR MI	31	
44-	23	049	074	02/13/73	2400	24.7	05	09/3	07 51 0	31	
				02/13/73							
	*	051	060	02/13/73	0400	24 0	05	0975	PT CLO	*	
	53	052	000	02/13/73	0400	24 9	05	0975	PT CLU		
				02/13/73							
				02/13/73							
	53	055	160	02/13/73	0800	24.4	04	0755	PT CLO	¥	
-	53	050	061	02/13/73	0000	24.4	04	0753	PT CLO	*	
	53	047	200	02/13/73	1500	24.9	04	0465	PT CLU	Y	
				02/13/73							
				02/13/73							
	53	000	005	02/13/73	1500	50.4	04	0403	PT CLD	*	
946	55	001	100	07/15/73	1600	25.0	0.7	1025	OCAST		
				02/15/73							
				02/15/75							
***	22	004	aut	02/15/73	1000	53.0	01	1050	UCTEL		
***	22	003	200	02/15/73	2000	20.0	07	1135	DCAST		
405	**	007	200	02/15/73	2000	20.0	07	1135	DCAST		
	**		200	02/15/73	2000	24 4	87	1133	OCART		
405	35	200	200	02/15/73	3600	20 0	27	1245	DEAST		
				02/15/73							
				02/15/73							
390	55	012	003	02/15/73	2400	24.0	07	1248	DEAST		
OPE	55	013	004	02/16/73	0400	25.0	07	1245	DCAST		
	-99	010	004	02/16/71	0400	25.0	67	1248	DCAST.		
300	55	015	004	02/16/73	0400	25.0	07	1245	OCAST		
				02/16/73							
				02/10/75							
				02/16/73							
946	55	019	005	02/16/73	0800	25.0	07	0795	DCAST		
-046	22	050	005	02/10/73	0000	55.0	07	0795	OCAST -		
				02/16/73							
				02/16/73							
				02/16/73							
				02/16/73							
-495	**	424	007	02/16/73	1600	24.0	07	1025	OCAST		
400	**	027	007	02/16/73	1400	24.0		1025	OCAST		
				02/16/13							
	45	429		02/16/73	2000	24.0	07	10/5	DEART		SPRAY OVER STAD P
				2714/71							SPRAY DVER STED P
1		-	-		-		-57				

YOY	TP	INT	tox	DATE	TIME	SPO	81	RWYD	A-24	HEATHER		COMM	ENTS	
095	55	031	008	02/16/73	2000	24.0	07	1025	DCAST		SPRAY	OVER	STAD	-
				02/16/73							SPHAY	UVER	STHO	A
-A9F	55	035	009	02/16/75	2400	24.0	05	1025	DEAST	FIG		-		_
09E	55	034	009	02/16/73	2400	24.0	05	1025	DEAST	FUG				
OPE	55	035	009	02/16/73	2400	24.0	15	1053	DCAST	FIJG				
				02/16/73						FUG		-		_
				02/17/73										
				02/17/73										
-09E	55	039	010	02/17/73	0400	23.0	05	1052	DCAST	-	-		-	-
09E	55	040	010	02/17/73	0400	23.0	05	1053	DCAST					
				02/11/75							ROLLIN			
				02/17/73							ROLLIA			
				02/17/73							ROLLIN			
				02/17/73							ROLLIN	IG EAS	SILY	
				02/17/75									-	-
				02/17/73										
				02/17/73										
				02/17/73						7		-	-	-
				02/17/73										
				02/17/73										
04E	-55	051	013	02/17/73	1600	24.0	00	1052	DEAST				-	
				02/17/73										
				02/17/73										
				02/17/73								-	-	-
				02/17/73										
				02/17/73										
				02/17/73								-	-	-
				02/17/73										
046	57	002	010	02/18/73	0400	54.0	04	12/5	PI CLD					
-04E	57	000	016	02/18/73	0400	24.0	04	1512	PT CLO	1			-	-
0.05	57	007	016	02/16/73	0400	24.0	04	1215	PI CLO					
				02/18/73						4				
				02/18/73								-		-
OAE	21	010	0.1	02/18/73	0500	24.0	04	0443	CLOY					
				02/18/73										
				02/18/73									-	-
340	5/	013	018	02/18/73	1500	24.0	05	0442	DI CLO					
				02/18/73										
-046	21	015	018	02/18/73	1500	24.0	05	0000	PI CLO				-	-
				02/18/73										
996	67	017	014	02/18/73	1000	23.0	04	0995	CLOY					
946	67	010	914	02/18/73	1000	23.0	04	0995	CLOY					-
				02/18/73										
				02/18/73										-
				02/18/73										
				02/18/73										
				02/18/73										
846	31	950	961	05/10/13	2400	53.0	03	1449						

YOY	10	INT	101	DATE	TIME	SPO	81	RWVD	A-25	MEATHER	404	79	INT	10x	DATE	TIME	500	84	****	A-26	HEATHER
				02/18/73								_				-	-	-			
				02/18/73							044	59	017	034	02/25/73	0800	24.0	06	0512	DCAST	
											04#	54	018	034	02/25/73	0400	24.0	0.0	0512	DEAST	
				02/19/75							-094	59	019	034	02/25/13	0800	24,0	0.6	0512	DEAST	
				02/19/73							044	74	050	0 14	15/52/25	0800	50.0	00	0512	PCAST	
				07/19/71							04=	24	150	0.55	02/25/73	1500	54.0	07	0434	bi cro.	
				02/19/75							-044	54	220	015	02/25/73	1500	24.0	07	0430	PT CLO	
				05/19/73							04#	24	053	0.15	02/25/73	1500	24.0	0.1	0415	AL CTD	
				02/19/73							044	50	074	035	17/55/50	1500	24.0	07	0435	PT CLD	
045	27	035	023	02/19/73	0000	23.0	96	1/50	DEAST		-044	50	024	0.36	02/25/13	1000	25.0	07	0715	PT CLO	
				02/19/73							994	50	027	036	02/25/73	1000	27.0	07	0713	PI CLU	
				02/19/73							074	50	027	010	02/25/73	1600	25.0	0.7	0213	bi cro.	
976	21	034	024	02/19/73	1700	23.0	04	1550	OCAST.		094	59	029	012	02/25/13	3000	25.0	07	0713	CLACE.	
144	57	040	0.24	02/19/13	1600	23.0	0.0	1770	0			50	010	017	02/25/73	3000	25 4	0.7	4215	1.6.21	
				02/19/73							- 49#	50	031	037	05/55/13	3000	25 4	0.7	0215	DEADY	
945	57	044	435	02/19/13	1600	23.0	04	1110	07 61 0			59	032	037	02/25/75	2000	25.0	0.7	0213	DEAGT	
				02/19/73							894	59	033	038	02/25/73	2400	25 0	05	DOIP	PT CIN	
				02/19/73							-09H	59	034	034	02/25/11	2400	25 0	05	0018	PT CLOS	
				02/19/75							MPO	59	035	034	02/25/73	2400	25.0	05	0018	PT CLOS	
				02/19/71							898	59	016	018	02/25/73	2400	25 0	05	0018	PT CLO	
				92/19/73							-09#	59	037	010	02/20/13	0400	25.0	05	0240	PT CLU	
				02/19/73							091	59	038	039	02/26/73	0400	25.0	05	0240	PT CLOY	
405	57	050	027	02/19/13	2000	24.0	04	1204	DEAST	1	894	59	039	039	02/26/73	0400	25.0	05	9999	PT CLD	
496	37	051	027	02/19/73	2400	24.0	04	124P	CCAST		0 9 M	50	040	039	27/05/50	0400	25.0	115	0245	PT CLUY	
BPO	57	052	027	02/19/73	2400	24.0	04	1240	CCAST		0.01	59	041	040	17/05/50	0800	25.0	05	9248	THEAST	
09E-	57	053	020	02/20/73	0400	24.0	04	GAPP	CLDY -		098	59	042	040	27105150	9609	25.0	05	9248	TOCAST	
89E	57	054	078	02/20/73	0400	24.0	04	0489	CLDY		-64H	59	045	040	02/26/73	0600	25.0	05	0248	70C.S1	
09E	57	055	ASO	02/20/73	0400	24.0	04	098P	CLDY		09H	59	044	000	17/45/50	0600	25.0	05	4050	THEAST	
99E	57	050	028	02/20/73	0400	24.0	04	098P	CLOY -		09W	59	045	140	02/26/73	1200	25.0	00	9446	DEAST	
390	57	057	029	02/20/73	0000	24.0			CCAST		-09W	59	046	041	02/26/73	1200	25.0	06	9446	MCAST	
99E	57	058	650	02/20/73	0500	0.05			DEAST		044	59	047	041	02/20/73	1200	25.0	06	0247	UCAST	
OPE-	57	059	650	02/20/73	0800	24.0			OCAST -		044	59	048	041	02/25/73	1200	25.0	00	05ah	PCAST	
09E	57	060	054	02/20/73	08 0	24,0			UCAST		-09H-	59	049	042	02/26/73	1600	52.0	06	0956	CCAST	
944	59	001	0.7	02/24/73	1600	55.0	04	1338	CLOY		094	59	050	042	02/26/73	1600	25.0	0.0	095b	DEAST	
09	59	200	010	02/24/73	1600	55.0	04	1335	CFDA-						02/26/73						
				02/24/73								59	052	042	02/26/73	1600	25.0	00	0954	MCAST	
				02/24/73							044	61	001	043	02/26/73	5000	25.0	00	0053	DEAST	
				02/24/73											02/76/73						
				02/24/73							-09#	-10	003	043	02/26/73	5000	55.0	0.6	0053	TICAST	
				02/24/73							945	•1	004	043	02/26/73	5000	25.0	0.0	0053	CAST.	
				02/24/73											02/26/73						
				02/24/73											02/26/73						
				02/24/73											07/26/73						
				02/24/73											02/26/73						
674	39	210	935	05/54/17	2400	24.0	03	1203	CEAST		-044	21	004	642	21/12/40	0000	65.0	04	0455	DEAST .	
				02/25/73							940	::	010	045	02/27/73	0400	65.0	04	0455	CEAST	
97#	24	014	011	02/25/13	9400	55.0	04	0546	CLOA						11/15/50						
948	34	015	033	02/25/73	0400	20.0	04	0245	CFOA						02/27/75						
948	34	410	622	02/25/73	8400	43,0	04	9546	CEDA		944	2:	413	046	2/27/73	9890	53.0	04	0422	TEAST	
	-	-	-	The same of the same	-	-	-				974	41	014	046	02/27/73	0800	65.0	04	0422	UCAST	

YOY	TP	INT	IOX	DATE	TIME	800	81	RHYD	A-27	MEATHER	VOY	TP	INT	IDX	DATE	TIME	800	81	R=40	A-28	HEATHER
				02/27/73											03/01/75						
				02/27/71											03/01/73						
				05/21/71											03/01/75						
				02/27/73											03/01/73						
				05/51/11											03/01/73						
				02/21/11											03/01/73						
				02/27/75											03/01/73						
	61	023	008	11/15/50	1600	23.0	05	045P	PT-CLO	Y					03/03/73						-
	61	024	048	02/27/73	1600	23.0	05	045P	PT CLO	*					03/03/73						
49	61	025	049	02/27/73	2000	25.0	07	061P	CLDY		100	63	003	001	03/03/73	2400	24.6	04	0465	DCAST	
				45/27/73											03/03/73						-
				02/21/13											03/04/73						
				02/27/73											03/04/71						
				02/27/73											03/04/73						
				02/27/73											03/04/73						
	01	031	050	05/27/73	2400	25.0	07	0455	CLOY						03/04/73						
				02/28/73											03/04/73						-
				02/28/73											03/04/73						
				12/20/73											03/04/73						
				02/28/73											03/04/73						
																					-
94	61	039	952	02/28/73	0000	25.0	04	06/3	RAIN		10F	63	017	005	03/04/73	1600	29.7	05	0783	CLDY	
				02/28/73							10E	63	018	005	03/04/73	1600	29.7	05	0785	PT CLDY	
				92/28/73											03/04/73						
				02/25/73							105	63	051	006	03/04/73	5000	29.7	04	0798	PT CLDY	. '
											101	63	072	006	03/04//3	2000	20.1	04	0745	SPT CLO	-
				02/28/73							100	4.7	024	006	03/04//3	2000	29.7	04	0795	SPI CLU	
				02/28/73							-105	14	025	007	03/04/73	2400	20 1	04	0795	LOT CLO	
	61	048	054	02/28/73	1600	25.0	06	1455	DCAST		105	44	026	007	03/04/73	2400	29 1	04	0795	PT CLOS	
				02/28/75											03/04/73						
				02/25/73											03/05/73						
				02/28/75							10E	63	030	008	03/05/73	0400	8.85	03	0793	FOG	
94	61	053	050	02/28/73	2400	25.0	08	1455	CLDY-		- 10E	63	031	008	03/05/73	0400	8.85	03	0795	FOG	-
911	61	054	056	02/24/73	2400	25.0	0.6	1455	CLDY		105	63	035	008	03/05/73	0400	28.8	03	0795	FUG	
**	61	055	056	02/28/73	2400	25.0	08	1453	CLDY		105	63	033	000	03/05/73	0600	1.02	04	0793	PT CLDY	
	61	056	056	02/28/13	2400	25.0	0.6	1455	CLDY-		10E	65	034	000	03/05/73	0000	20.1	04	0795	PT CLOY	
-	61	057	057	03/01//1	0400	25.0	00	1455	PT CLO		105	63	036	009	03/05/75	0800	29 1	04	0795	PT CLDY	
-	41	450	057	01/01/73	0400	25.0	06	1455	PT CLD	,	105	41	030	010	03/05/73	1300	28 0	0.0	1025	PT CLOY	
	61	060	057	03/01/75	0400	25 0	0.0	1459	PT CLO	,					03/05/73						
	61	061	058	03/01/75	0000	25.0	05	1005	CLEAR		105				03/05/73						
91	61	500	058	03/01/75	0800	25.0	05	1005	CLEAR		- 10F										
94	61	063	054	03/01/73	0800	25.0	05	1003	CLEAR	A1 35-	101	63	041	011	03/05/75	1600	28.9	04	1025	PT CLDY	
			12.00	03/01/73											03/05/73				1111		

404	TP	INT	IOX	DATE	TIME	390	81	RHVD	A-29	MEATHER	COMMENTS
108	63	043	011	03/05/73	1600	28.9	04	1029	PT CLD		
				03/05/73							
105	63	045	012	03/05/73	2000	29.0	00	1052	PT CLO		
105	65	046	012	03/05//3	2000	29.0	06	1025	PT CLO		
105	65	047	012	03/05/73	2000	29.0	00	1052	PT CID		
TOE	63	048	012	03/05/73	2000	29.0	06	1052	PT CLU		
107	63	049	013	03/05/73	2400	28.9	05	1053	PT CLO		
105	63	050	013	03/05/73	2400	28.9	22	1025	PT CLO		
10F	63	051	013	03/05/13	2400	28.9	05	. 452	PT CLO		
10E	63	052	015	03/05/73	2400	20.9	05	1000	PT CLO		
10E	63	055	014	03/06/73	0400	6.82	05	1543	PT CLU		
105	65	054	014	03/00/73	0400	28.9	0.5	1245	PT CLO		
1 OF	63	055	014	03/06/71	0400	28.9	05	1245	PT CLU	•	
				03/06/73							
				03/06//3							
				03/06/73							
				03/06/73							
				03/06/73							
				03/06/73							
				03/06/73							
				03/06/73							
				03/05/73							
105	63	065	017	03/06/73	1600	28.7	05	0575	CLAST		
10E	63	066	017	03/06/13	1600	28.7	05	0578	DCAST -		
				03/00/73							
				03/06/73							
				03/06/73							
				03/06/73							
				03/06/73							
				03/00/73							
				03/06/73							
				03/06/13							
105	65	003	019	03/06/73	2400	28.6	07	0795	OCAST -		
				03/06/73							
				03/07/73							
				03/07/73							
				03/07/73							
				03/07/73							
				03/07/73							
				03/07/73							
				03/07/73							
				03/07/73		20.1	00	1003			
				03/07/73					UCAST		
				03/07/73					MCAST		
				03/07/73			-		OCAST -		
				03/07/73		20 .			OCAST		
				03/07/73							PORT LIST
				05/01/75							PORT LIST
				03/07/73							PORT LIST
107		050	052	03/07/73	1500	20.0	0.0	1003	CICAST		PURI 6131

VOY	TP	INT	IOX	DATE	TIME	SPO	81	# * ¥0	A-30	HEATHER	COM	HENTS	VOY	TP	INT	IDX	DATE	TIME	800	-	RHYD	A-31	MEATHER
105	45	021	626	03/07/73	1000				DEAST		PORT	1121					03/12/73						
				03/01/15					CCAST			LIST					03/12/73						
				03/07/75			-		DEAST			LIST					13/12/73						
				01/07/73					CCAST		PORT	LIST					03/12/73						
10E	65	025	025	03/07/75	1600	28.5	06	07/5	DCAST.								03/12/73						
				03/07/73													03/12/73						
				03/07/73													03/12/73						
301	92	058	052	03/07/75	1000	28.5	00	0112	UCTEL								03/12/73						
-10E	65	054	054	01/07/73	5000	54.4	00	0775	FUA -		-						03/12/73						
				03/07/73									10#	67	037	010	03/13/73	0400	28.5	05	9999	RAIN	
				03/07/73									-10H	67	038	010	03/13/73	0400	28.5	05	4620	RAIN -	
-101	63	036	020	03/07/73	5000	20 0	00	OFFS	BT CLO		1		104	67	034	010	03/13/73	0400	28.5	05	9999	RAIN	
101	67	0 53	027	03/07/73	2400	28 4	05	0555	PT CLC								03/13/73						
				03/07/73													03/13/73						
				03/07/73									104	67	005	011	03/13/13	0800	24.5	04	056b	DCAST	
INF	45	037	028	03/08/13	0400	28.8	04	0335	CLEAR								03/13/73						
				03/08/75						-	_						03/13/73						
106	45	039	024	03/08/75	0400	8.85	04	0335	CLEAR								03/13/73						
105	65	040	850	03/08/73	0400	24.A	04	0335	CLEAH								03/13/73						
-106	65	041	029	03/08/75	0600	28.9	45	0305	CLEAR	-	-						03/13/73						
10E	65	042	929	03/00/13	0800	28.9	50	0305	CLEAR								03/13/73						
IOF	65	043	029	03/08/73	0800	28.9	0.5	0303	CLEAR								03/13/73						
-10E	65	044	029	03/08/71	0000	28.9	20	0305	CILLAR _				- 10-	47	050	013	03/13/73	1600	26 4	04	0000	PI CLE	
104	67	201	100	03/11/73	1600		03	1526	BCAST								03/13/73						
104	67	200	001	03/11/73	1600		03	152	OCAST				-100	67	053	014	03/13/73	2000	28 8	0.7	MAIP	DEART	
-10	67	007	001	03/11/73	1000		03	1250	DEAST	-	-5170		104	67	054	014	03/13/73	2000	8.85	07	0419	DCAST	
	67	004	001	03/11/73	1600		03	1250	UCT :								03/13/73						
10=	67	005	005	03/11/73	5000	20,1	0.5	164	DEAST								03/15/73						
-10=	67	006	200	03/11/73	5000	20.3	0.3	1645	OCASI -			- Comment					13/15/73						
				03/11/73									104	67	058	015	03/15/73	2400	24.5	08	DASP	OCAST	
104	67	008	300	03/11/73	5000	28 0	0.4	1045	CLEAD				-10H	67-	054	015	03/13/73	2 00	28.5	08	GAIP	OCAST-	
-10#	67	004	003	03/11/73	2400	26 0	0.4	1417	CLEAR		750		104	67	060	1.15	03/13/73	2400	28.5	06	0412	OCAST	
10*	01	010	001	03/11/73	2400	28 0	0.0	1019	CLEAR								03/14/73						
10-	47	011	003	03/11/73	2400	28.9	04	141P	CLEAR								03/14/73						
100	47	011	004	03/12/73	0400	28 A	05	0748	PT TLD	Y							03/14/73						
104	67	014	004	03/12/73	0400	8.45	05	074P	PT CLO	*							03/14/73					-	
	67	015	004	03/12/13	0400	8.85	05	0748	PT CLU	Y		-					03/14/73						
104	67	016	004	03/12/73	0400	28.8	05	074P	PT CLO	Y							03/14/73						
104	67	017	005	03/12/73	0400	28.6	06	1199	PT CLD	*							03/14/73						
-104	67	018	005	03/12/73	0000	24.6	00	1198	PT CLD	Y			- 104	40	000	017	03/14/73	1300	27 4	0.0	0140	KA14-	
104	67	019	005	03/12/73	0600	28.6	06	1198	PT CLO	*							03/14/73						
10#	67	050	005	03/12/73	0800	28.6	06	1199	PT CLD	*							03/14/73						
-104	67	150	000	93/12/73	1200	28.7	06	096P	PT CLO	Y		-					03/14/73						
104	67	055	000	05/12/73	1500	Sh.7	00	0044	BI CTD	1							03/14/73						
104	67	053	000	03/12/73	1500	28.7	00	0969	PT CID								01/14/73						
-104	47	024	006	03/12/73	1500	28.7	00	096P	PT CLO								03/14/73						
104	67	052	007	03/12/73	1600	20,6	0.5	1197	PI CLD								03/14/73						
104	67	920	007	03/12/75	1600	20.6	0.0	1146	PI CLU	1													

VOY	TP	INT	10x	DATE	TIME	3PD	81	RWVD	A-32	PEATHER	COMMENTS
10#	69	009	020	03/14/73	1600	29.4	10	001P	DEAST		
				03/14/75							
				03/14/73							
				03/14/73							
104	69	013	150	03/14/73	1600	29.4	10	001P	OCAST		
				03/14/73							
104	69	015	150	03/14/73	1800	29.4	10	001P	DEAST		
104	69	016	151	03/14/73	1800	29.4	10	001P	OCAST		
-10%	69	017	055	03/14/73	2000	29.4	14	9014	CLOY		
104	69	018	055	03/14/73	5000	29.0	09	0014	CLDY		
104	69	019	250	03/14/73	2000	29.4	94	GOLP	CFOA		
				03/14/73							
10#	69	150	023	03/14/73	2200	29.4	09	001P	CLOY		
100	69	250	053	03/14/73	5500	29.4	04	0019	CLDY		
10#	60	057	550	03/14/73	5500	29.4	04	ONIP	CLDY		
				03/14/73							
				03/14/73							PITCHING
				03/14/73							PITCHING
100	69	150	024	03/14/73	2400	25.2	09	0445	CLOA		PITCHING
10	69	950	054	03/14/73	2400	55.5	00	0045	CLOY		PITCHING
				03/14/73							PITCHING
104	69	030	024	03/14/73	2400	22.7	0.4	0003	CLOA		PITCHING
104	69	031	024	03/14/73	2400	25.2	00	0043	CLOY		PITCHING
				03/14/73							PITCHING
				03/15/73							
				03/15/73							
				03/15/73							
IOM	69	036	025	43/15/75	4400	10.8	0.4	0443	bl Cin	4	
124	94	037	052	03/15/73	0400	19.8	0.8	0645	PL CFD	1	
104	44	038	052	03/15/73	0400	10.4	0.8	0443	PT CLO	Υ	
10	69	039	052	03/15/73	0400	19.8	0.5	0443	PT CLU	Y	
				03/15/73							
				03/15/73							
				03/15//3							
				03/15//3							
				03/15/73							
				03/15/73							
				03/15/73							
				03/15/73							
				03/15/73							4-E DEC MORT
				63/15/73							4-5 DEG. PORT LI
				03/15/73							A-S OLG. PORT LI
				03/15/73							4-5 DEG. PORT LI
				03/15/75							DEG, PORT LI
				03/15/73							
				03/15/71							
				03/15/73							
				03/15/13							
				03/15/73							
10.		430	95.4	43113113	5000			1301	06.01		

404	79	INT	10x	DATE	TIME	300	BN	RWVO	A-33	-tather	vov	10	INT	10x	DATE	TIME	300		RHYD	A-34 MEAT
10*	64	059	029	05/15/75	2000	79.6	02	136#	00451			71	000	411	03/21/75		20 1			
10*	64	000	059	03/15/73	5000	29.4	05	1500	DEAST		116	71	050	013	03/21/75	0400	29 1	0.0	1245	PT CLOY
				03/19/75							-11E	71	051	013	05/21/75	0400	20 1	0.0	1265	PI CLOY
				03/19/75						-	116	71	052	015	03/21/75	6466	19 7	64	1245	PT CLOY
				03/19/75							116	71	055	014	03/21/73	0800	28 5	05	1285	CIDA
				03/19/73							- 11E	71	054	014	03/21/73	0000	28 5	05	1285	CLDY
				03/19/73					OCAST.		116	71	055	014	03/21/73	0800	28 5	05	1285	CLDY
				03/19/73					DCAST		115	71	056	014	03/21/75	0400	28 5	05	1285	CLDY
116	71	001	200	03/19/73	1400				CCAST		-116	71	057	015	03/21/73	1200	28 7	06	1245	CLEAR
											116	71	058	015	03/21/73	1200	28 7	06	1285	CLEAR
				03/19/73							115	71	059	015	03/21/73	1200	28 7	00	1285	CLEAR
				03/19/73							-11F	71	060	015	03/21/73	1200	28 7	06	1285	CLEAR
				03/19/73							115	71	061	016	03/21/73	1600	28 9	05	1515	PICINY
				03/19/73		24,3	04				115	71	062	016	03/21/73	1600	24 0	05	1515	PTCLOY
				03/19/71					OCAST		-115	71	063	016	03/21/75	1600	28 9	05	1515	PICLOY
				03/14/75					OCAST		115	71	064	016	03/21/73	1600	28.9	05	1515	PICLOY
				01/19/73							116	71	065	017	03/21/13	2000	29.0	00	1515	CLOX
				03/19/73					CAST		-115	71	000	017	03/21/73	2000	29 0	00	1515	CLOV
				03/19/75							116	71	067	017	03/21/73	2000	29 0	06	1515	CLOX
116	11	010	005	03/19/73	5000	64.0	0.0	Inch	UCAST		115	71	068	017	03/21/73	2000	29 0	06	1515	CLOY
				03/19/73							-116	71	069	018	03/21/73	2400	28 A	0.4	1515	DCAST
				03/19/73							115	71	070	018	03/21/73	2000	28 A	0.0	1515	DCART
				03/19/73							116	71	071	014	03/21/73	2400	26 .	04	1516	DCART
				03/19/75							-11E-	71	072	018	03/21/73	2400	28 A	04	1515	OCAST
				03/19/73							116	71	075	019	03/22/73	0400	28 0	0.4	1515	DEAST
				03/19/73							115	71	074	019	03/22/73	6460	28 0	01	1515	OCAST
				03/20/73							-11F	71	075	019	03/22/73	0400	28 0	43	1518	DCAST
				03/20/73							115	71	076	019	03/22/73	0400	24 0	03	1515	OCAST
				03/20/73							115	73	500	020	03/22/73	0800	28 9	0.4	1515	DEAST
116	71	0.0	007	03/20/73	0400	Cn	0.5	1122	DEAST			73	001	020	03/22/73	0800	28 9	04	1515	DEART
116	71	054	008	03/20/73	0000	20,0	04	15/1	Cros		11E	73	004	020	03/22/13	0800	28 0	04	1515	DCAST
112	71	030	008	03/20/73	0,000	20.8	04	1578	Cros		11€	73	005	150	03/22/75	1200	28.9	04	1518	204
				03/20/73							-11E	73	006	150	03/22/73	1200	28 0	04	1515	FOE
				03/20/73							116	73	007	150	13/25/20	1201	28 9	64	1515	606
				03/20/73							11F	73	008	.50	03/22/13	1200	28 9	04	1515	FOR
				03/20/73							-11t	73	009	022	03/22/73	1600	28 A	04	1065	FOG
				03/20/73							115	73	010	550	03/22/73	1600	28 8	04	1065	FOG
				03/20/73							116	73	011	022	03/22/73	1600	28 8	04	1045	FOE
				03/20/73							11F	73	012	022	03/22/73	1600	28 A	04	1065	FOR
				03/20/13							11E	73	013	150	03/22/73	2000	28 8	04	1045	DCAST
				03/20/73							11E	73	014	023	03/22/73	2000	28 A	04	1065	DEAST
				03/20/73							-11E	73	015	023	03/22/73	2000	28.8	04	1063	DEAST
				03/20/73							11F	73	016	023	03/22/73	2000	2A A	04	1065	DEAST
116	11	300	911	03/20/73	2000	20,1	05	1355	PI CLD		116	73	017	024	03/22/73	2400	28 A	04	1045	DEAST
				03/20/13							-115	73	DIA	024	13/22/73	2400	28 8	00	1048	OCAST.
116	11	944	011	03/20/73	5000	20.7	05	1 458	PI CLO	-	116	73	019	024	3/22/73	2400	28 8	04	1065	DEAST
116	11	444	210	01/20/73	Saug	20,0	04	1375	PI CLD		115	73	050	024	03/22/73	2400	28 A	04	1005	DCAST
				03/20/73							116	73	150	025	03/23/73	0400	28 8	01	1005	PT CINY
116	11	047	015	03/20/73	2400	28,6	04	1355	PI CLO		- 11E	73	550	025	03/23/73	0400	28 8	0.6	1000	PT CLOY
116	"	040	015	03/20/73	2400	20.6	04	13.3	PI CLO		115	75	025	025	3/23/73	0400	28 8	03	1045	PT CLOV
																	50.0	0.3	1000	- LLUT

*01	TP	INT	IDX	DATE	TIME	SPD	84	RWYD	^		HEATHER
116	73	024	025	03/23/73	0400	28.8	03	1065	PT	CLDY	
116	73	650	026	03/23/73	0400	28.R	04	0615	PT	CLDY	
-11E	73	076	050	03/23/73	0800	8.85	04	0618	PT	CLOY	-
116	73	027	026	13/23/73	0000	8,85	04	0615	PT	CLDY	
				03/23/73							
				03/23//3							
11F	75	030	027	03/23/73	1200	8.85	05	1005	PT	CLDY	
116	73	031	027	03/23/73	1200	8.85	05	1005	PT	CLDY	
				03/25/73							
				03/25/73							
11E	73	034	028	01/25/73	1600	8.85	05	1005	PT	CLDY	
111	75	035	ASO	03/23/73	1600	28.A	05	1065	PT	CLDY	
11F	73	036	028	05/23/75	1600	8.85	05	1003	PT	CLOY	
				03/23/73							
11E	75	038	950	03/25/73	2000	8,85	05	1065	PT	CLOY	-
11E	73	039	029	03/23/73	2000	8,85	05	1005	PT	CLDY	
118	73	040	029	03/23/73	2000	8,85	05	1005	PT	CLDY	
11E	73	041	030	05/25/73	2400	28.5	03		PT	CLOY	
				03/25/75					PT	CLOY	
11E	73	045	030	03/25/73	2400	28.5	03		PT	CLDY	
11E	73	044	010	01/23/73	2400	28.5	05	-	PT	CLDY	-
116	73	045	931	03/24/73	0400	26.0	50		CLE	AR	
11E	73	046	031	03/24/73	0400	26.0	50		CLE	AR	
				03/24/73					CLE		
TIE	73	048	0 11	03/24/75	0400	20.0	02		CLE	AR	
				03/24/73					PT	CLOY	
				03/26/75					PT	CLOY	-
11#	75	003	001	03/76/13	1200	8.65	03			CLDY	
11"	75	004	001	03/26/73	1200	26.8	03			CLDY	
-11*	75	005	005	03/26/73	1600	24.7	0.3	025P	PT	CLDY	
11*	75	006	500	03/26/73	1600	26.7	03	075P	PT	CLOY	
11*	75	007	002	03/26/13	1600	26.7	05	9250	PT	CLOY	
11*	75	008	500	03/26/73	1.00	24.7	05	0250	PT	CLDY	
114	75	004	0 .5	03/76/75	2000	28.5	05	044P	ac.	ST	
1.0	75	010	003	03/26/13	2000	28.5	05	0449	nc 4	ST	
-11*	-75	011	005	03/20/73	2000	28.5	05	044P	OCA	81-	
114	75	012	001	03/26/73	2000	28.5	05	0444	004	181	
11*	75	015	004	03/20/73	2400	28.5	05	0449	OC.	ST	
-11*	75	014	004	03/26/73	2400	28.5	05	044P	OC.	ST	-
11.	75	015	004	03/26/73	2400	28.5	05	044P	DC	ST	
114	75	016	004	03/20/73	2400	28.5	05	9990	nc	ST	
-11"	-75	017	005	03/21/73	0400	8.85	03	4550	CLI	Y -	-
11.	75	018	005	03/27/73	0400	28.8	03	055b	CLE	7	
11.	75	019	005	03/27/73	0400	8.85	0.5	4550	CLE	Y	
	75	020	005	01/27/13	0400	28.8	03	9575	CLI) ¥	-
114	75	150	400	03/27/73	0600	8.85	05	0228	nc	181	
118	75	550	000	03/27/73	0800	A. 85	05	0225	00	ST	
-110	75	023	000	03/27/73	0400	4.45	05	0 73	nc	ST -	-
	75	024	006	03/27/73	0000	8.85	05	0552	OCI	ST	
				03/27/73							

L. ED. A-37 HEATHER TIME SPD BN RWYO A-36

***RATHER**

1700 2A, A 05 0225 (ICAS) DRIZZLE

1200 2A, A 06 025 (ICAS)

1200 2A, A 06 025 (ICAS)

1200 2A, A 07 025 (ICAS)

1200 2A, A 08 0849 (IC A-36 VOY TP INT IOX DATE TIME SPO BN RHYD VOY TP INT IDX DATE TIME SPD BN RNVD 1358 1358 1358 1358 1418 1418 1418 1418 Y TP INT IDX DATE TIME BPD BN RHUD A-38 #

E 79 007 002 04/01/73 2000 24,8 06 0235 0CAST
E 79 000 002 04/01/73 2000 24,8 06 0235 0CAST
E 79 000 002 04/01/73 2000 24,8 06 0235 0CAST
E 79 010 003 04/01/73 2400 25,6 05 0455 CLDY
E 79 010 003 04/01/73 2400 25,6 05 0455 CLDY
E 79 010 003 04/01/73 2400 25,6 05 0455 CLDY
E 79 011 003 04/01/73 2400 25,6 05 0455 CLDY
E 79 012 003 04/01/73 2400 25,6 05 0455 CLDY
E 79 013 004 04/02/73 0400 25,6 05 0455 CLDY
E 79 013 004 04/02/73 0400 25,6 05 0455 CLDY
E 79 013 004 04/02/73 0400 25,6 05 0455 CLDY
E 79 013 004 04/02/73 0400 25,6 05 0455 CLST
E 79 014 005 04/02/73 0400 25,6 05 0455 CLST
E 79 015 004 04/02/73 0400 25,6 05 0455 CLST
E 79 016 004 04/02/73 0400 25,6 05 0455 CLST
E 79 017 005 04/02/73 0400 25,6 03 023P CLDY
E 79 018 004 04/02/73 0400 25,6 03 023P CLDY
E 79 020 055 04/02/73 0400 25,6 03 023P CLDY
E 79 020 055 04/02/73 0400 25,6 03 023P CLDY
E 79 020 055 04/02/73 0400 25,6 03 023P CLDY
E 79 020 065 04/02/73 0400 25,6 03 023P CLDY
E 79 020 065 04/02/73 0400 25,6 03 023P CLDY
E 79 020 065 04/02/73 0400 25,6 03 023P CLDY
E 79 020 066 04/02/73 0400 25,6 03 023P CLDY
E 79 020 066 04/02/73 0400 25,6 03 023P CLDY
E 79 020 066 04/02/73 0400 25,7 03 024P CLDY
E 79 020 067 04/02/73 0400 25,7 03 024P CLDY
E 79 020 067 04/02/73 0400 24,7 03 054P CCAST
E 79 020 067 04/02/73 0400 24,7 03 054P CCAST
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E 79 020 067 04/02/73 0400 24,7 03 054P CCAST
E 79 034 004 04/02/73 0400 24,7 03 054P CCAST
E 79 035 004 04/02/73 0400 24,7 03 054P CCAST
E 79 035 004 04/02/73 0400 24,7 03 054P CCAST
E 79 035 004 04/02/73 0400 24,7 03 054P CCAST
E 79 035 004 04/02/73 0400 24,7 03 054P CCAST
E 79 035 004 04/02/73 0400 24,7 03 054P CCAST
E 79 035 010 04/02/73 0400 24,7 03 054P CCAST
E 79 035 010 04/02/73 0400 24,7 03 054P CCAST
E 79 035 010 04/02/73 0400 24,7 03 054P CCAST
E 79 035 010 04/02/73 0400 24,7 03 054P CCAST
E 79 035 010 04/02/73 0400 24,7 03 054P CCAST
E 7 A-38 HEATHER VOY TP INT 10X DATE TIME SPO BN RHYD VOY TP INT TOX DATE TIME SPO AN RHYD A-39 HEATHER 7 015 04/01/13 2000 20.0 03 1049 OCAST
8 015 04/01/13 2000 20.0 03 1049 OCAST
9 015 04/01/13 2000 24.0 03 1049 OCAST
015 04/03/13 2000 24.0 03 1049 OCAST
0 015 04/03/13 2000 24.0 03 1048 OCAST
0 015 04/03/13 2000 24.0 03 1048 OCAST
0 015 04/04/13 0400 24.0 03 1048 OCAST
0 016 04/04/13 0400 24.0 03 1048 OCAST
0 017 04/04/13 1200 24.0 03 1048 OCAST
0 018 04/04/13 1200 24.0 03 1048 OCAST
0 018 04/04/13 1200 24.0 03 1048 OCAST
0 018 04/04/13 1200 24.0 03 1048 OCAST 12E 79 12F 79 12E 79 12E 79 12E 79 12F 79 12F 79 12E 79 057 059 060 061 062 063 064 065 066 067 070

APPENDIX B

PARAMETRIC STUDIES

This appendix contains the plots and tabulated summaries resulting from the parametric studies program, designated "SPLOT". Each plot presents either a five-curve family of various ship speeds or a five-curve family of relative wave direction groups for a transducer output against Beaufort Number. Within each Beaufort Number, the magnitude of a particular point is determined by calculating the mean of the appropriate data. A superscribed note on each plot designates which value is applicable. The measured data set is composed of the maximum waveinduced peak-to-trough value within each 30-minute data interval, or the RMS value determined for that interval. The graph title notes which characterization is applicable. Eight measurements, all from Recorder No. 1, were selected for study:

- Longitudinal Vertical Bending Stress
 Longitudinal Horizontal Bending Stress
 Torsional Shear Midship Stress
- 4. Forward Shearing Stress-Port
- 5. Forward Shearing Stress-Starboard
- 6. Roll Angle
- 7. Pitch Angle
- Forward Hull Vertical Acceleration

Each tabulated summary (Tables III-XXXIV) presents a listing of all plotted points along with the number of data points comprising each plotted mean point and its standard deviation.

Table B-I provides an index for all parametric plots and summaries.

Table B-II gives the code for the ship speed or relative sea direction curve families as used in the plots.

TABLE B-I Figure and Table Index for Parametric Studies

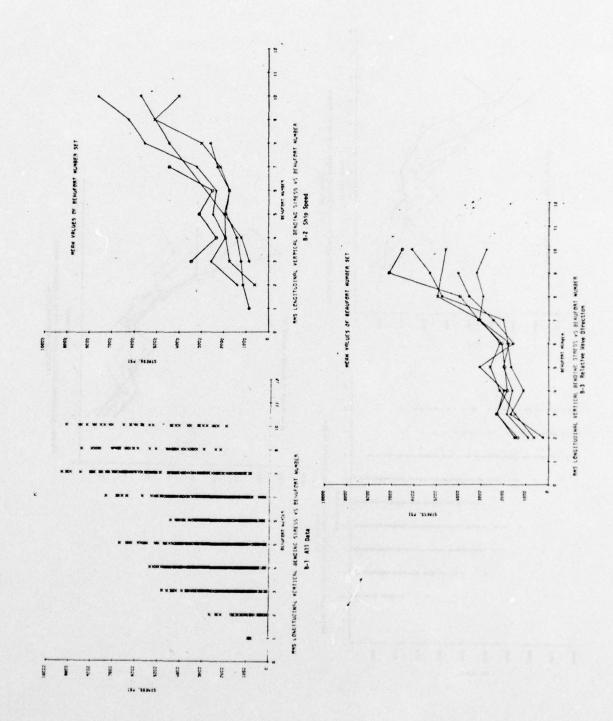
For value each 30-	e within minute						Fo	rse	nso	r*							
interval of:		LVB		LHB		TSM		SFP		SFS		ROLL		PITCH		FAV	
For values each Beaufo	rt No. Set	RMS	Мах	RMS	Max	RMS	Max	RMS	Max	RMS	Max	RMS	Max	RMS	Max	RMS	Max
All Data	Points	1	4	7	10	13	16	19	22	25	28	31	34	37	40	43	46
Mean of	by Ship Speed	2	5	8	11	14	17	20	23	26	29	32	35	38	41	44	47
All Data Points	by Relativ	3	6	9	12	15	18	21	24	27	30	33	36	39	42	45	48
Summary Listing	by Ship Speed	111	٧	IIV	IX	IX	XIII	ΧV	IIVX	XIX	XXI	XXIII	XXV	XXVII	XXIX	IXXX	XXXI
	by Relative Wave Direction	1٧	VI	V111	х	XII	XIV	XVI	XVIII	xx	IIXX	XXIV	XXVI	XXVII	xxx	IIXXX	xxxI

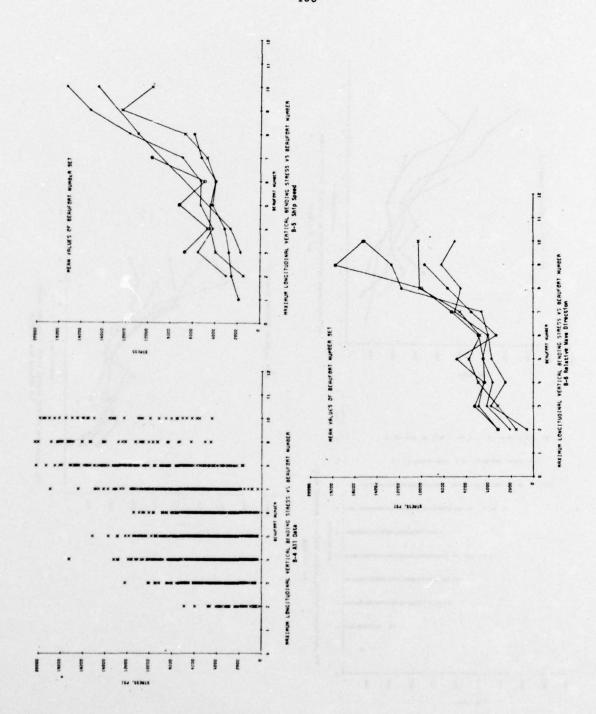
Note: Arabic numbers are Figure Numbers B-1, etc.
Roman numberals are Table Numbers B-III, etc.
*See Table III for definition of Sensor Abbreviations

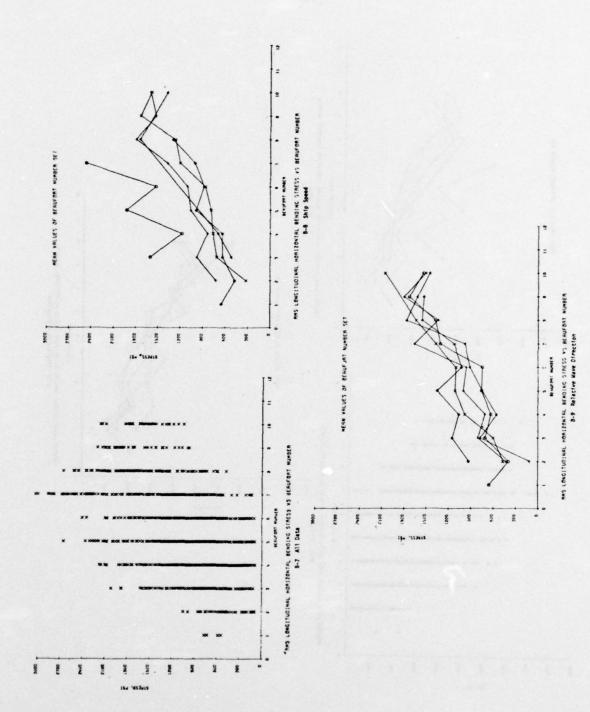
TABLE B-II

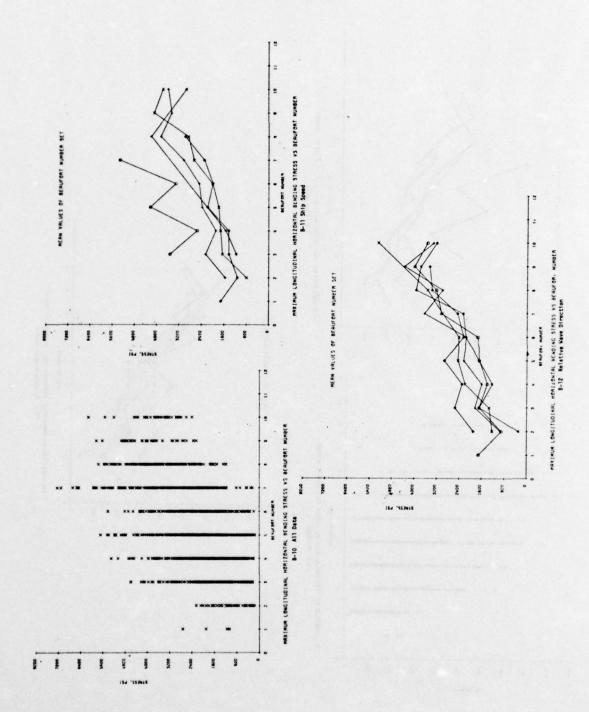
LEGEND FOR PARAMETRIC STUDIES

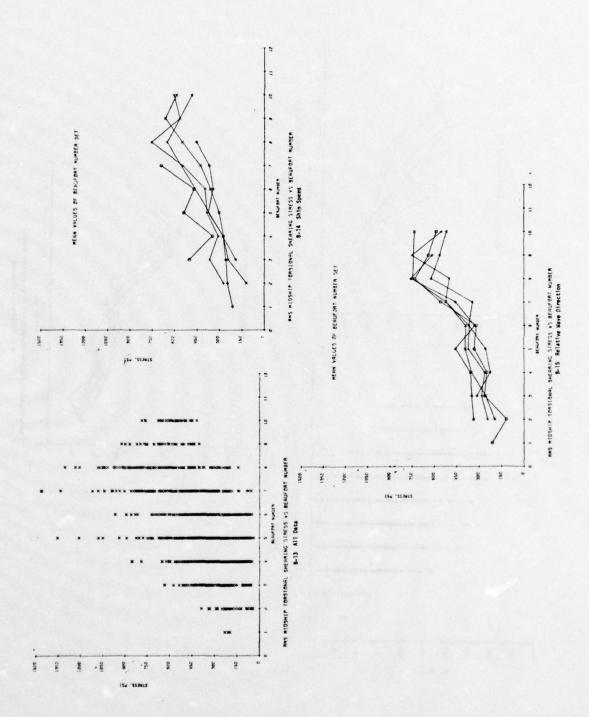
SYMBOL	Ship's Speed, Knots	Relative Sea Direction, Deg. P or S
0	1-15	0-30
Δ	15-20	31-60
+	20-25	61-120
×	25-30	121-150
♦	30-35	151-180

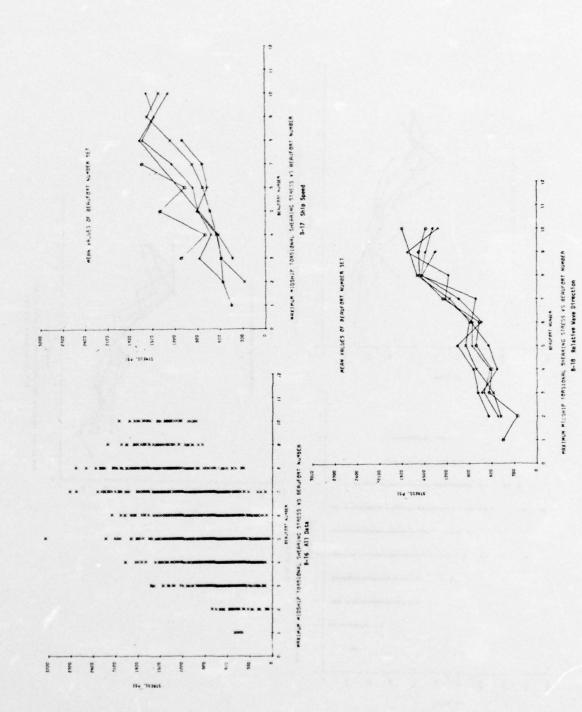


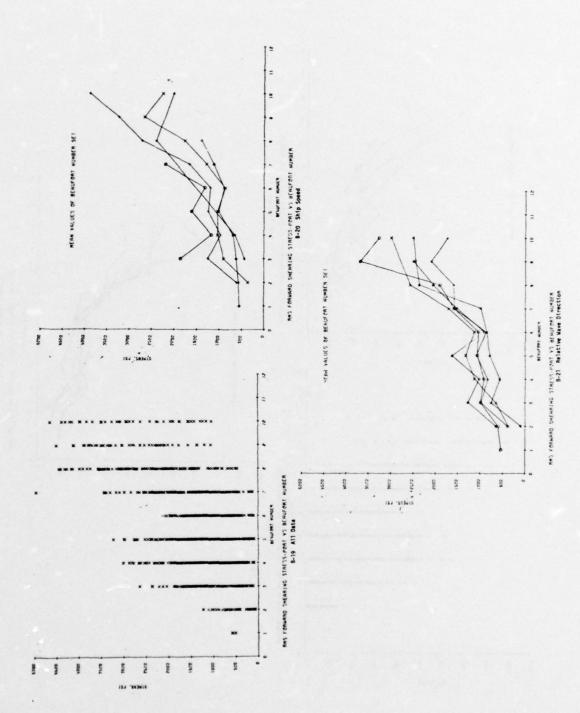


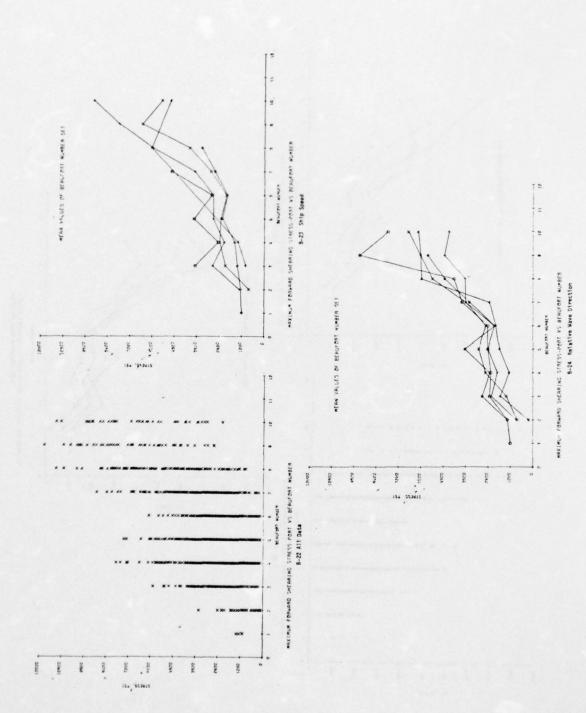


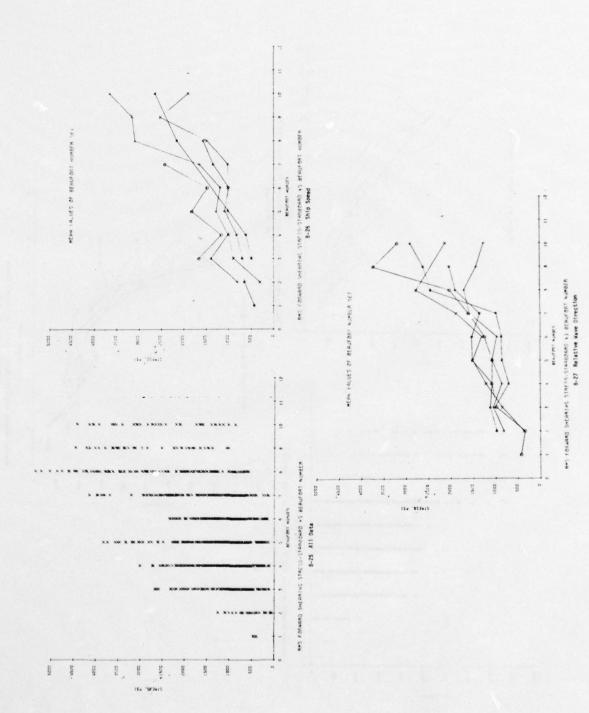


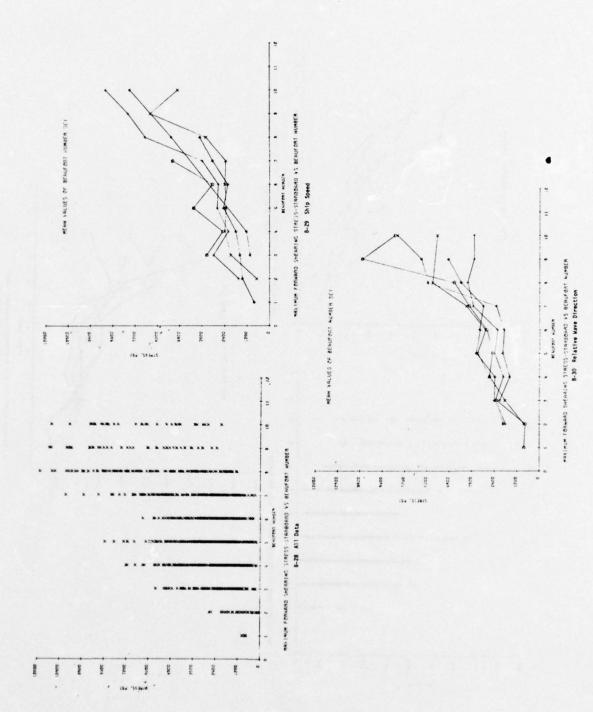


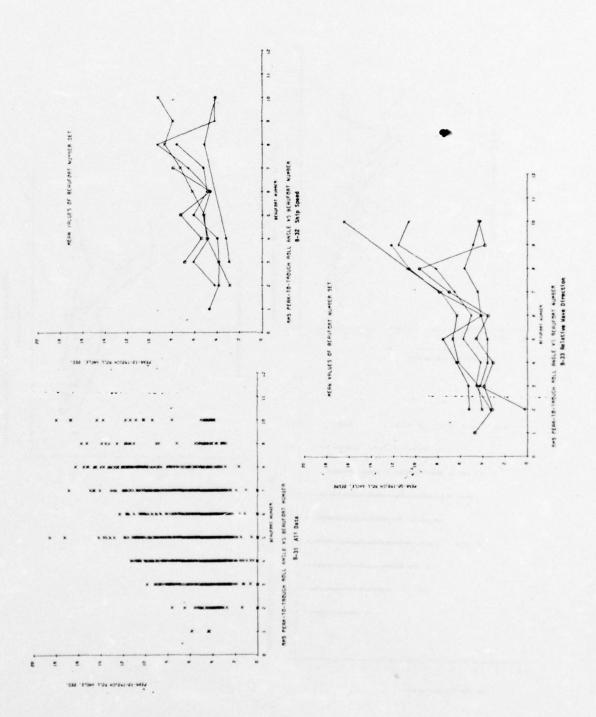


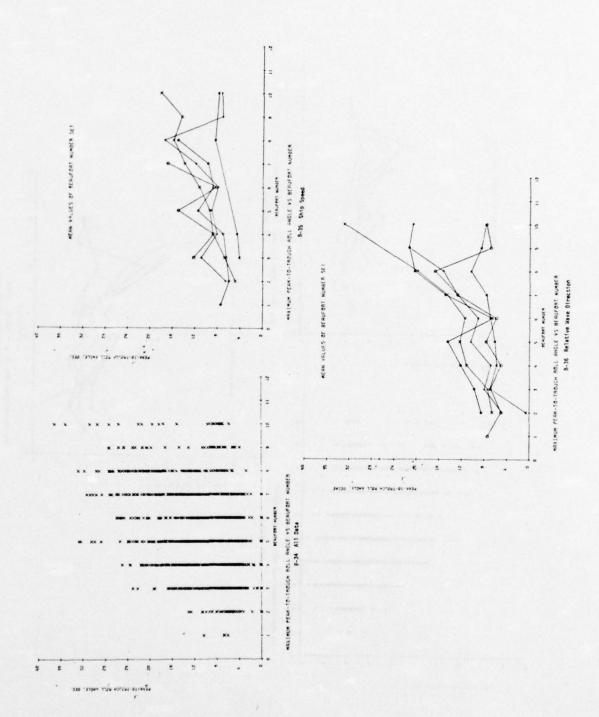


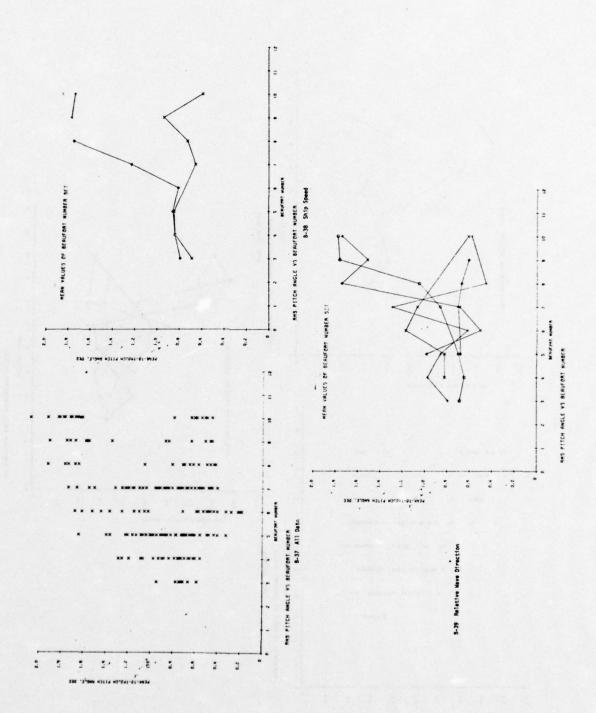


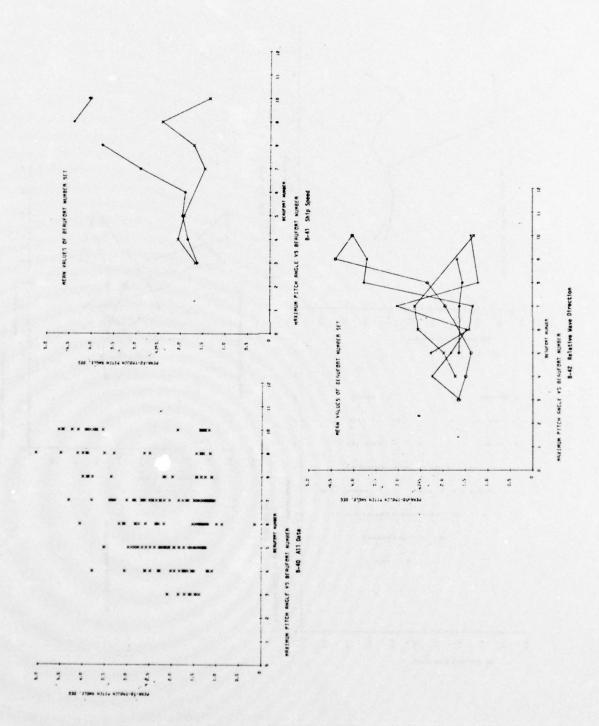


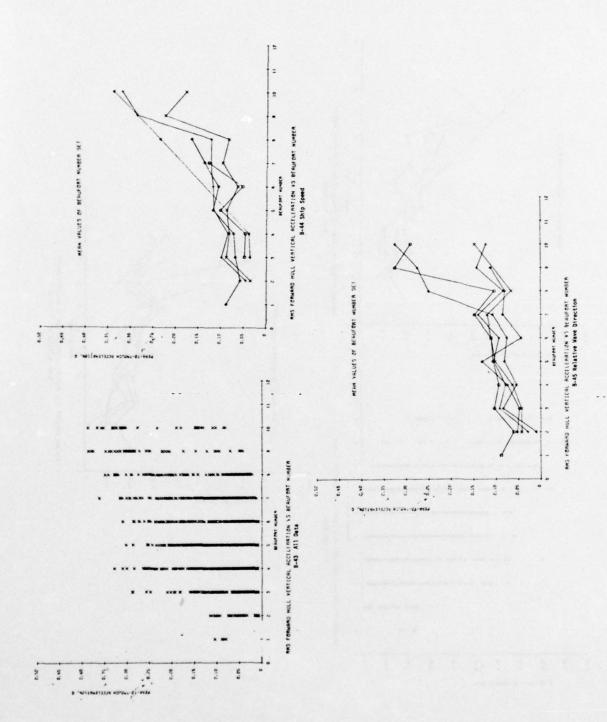


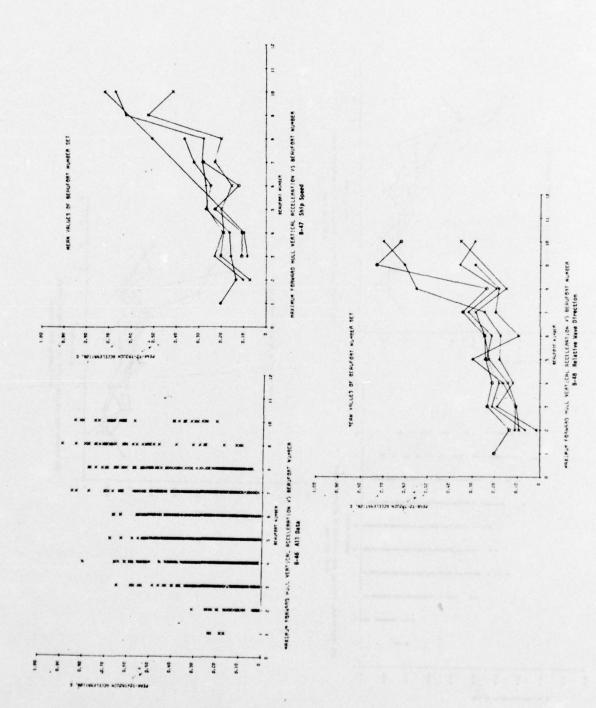












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1	'n	1121.	1310.		
	**	1713.	1314.	594.	A
:	126	1087.	1518.	572.	The second second second
	11	1750. 2265. 2572.	1997. 2504. 2872.	1068.	
•					

IV

in a garage					2	
		CTION BETWEEN	0.0 AND 31.0		SYMBOL OCTAGONAL	
	EAUF OPT	NO. UF DATA	MEAN	-	81, CEVIATION	
	AUTOL II					
	;	,:	1372.	1551.	723.	
	3	40	5315.	2370.	519,	
	;	47	1839.	2204.	1215.	
		57	2069.	2406.	1227.	
	1	20	3131.	3165.	541	
	:	,:	3958. 7115.	4306. 7141.	1674.	
	10	1	4522,	4805.	1941.	
	11			-	Array 10 mm	CONTRACTOR SERVICE SERVICES
	15					Committee of the second second
ELATIVE	HAVE DINE	CTION BETHEEN	31.0 AND 61.0	PLOT	SYMBOL TRIANGLE	
	EAUFORT	NO. OF DATA	HEAN	RHS	ST. DEVIATION	
	NUMBER					A-4-4
	1	0	253,	251.	43,	
	3	54	1673.	257.	916. 715.	
	•	110	1111.	1351.	715.	
	:	75	1657.	1935.	786.	
	;	50	2027.	2231.	932.	
	:	35	4755.	4686.	1124.	- 1 mm - 1 mm - 1 mm - 1
	10	12	5301.	5377. 6130.	902.	
	11					
FLATIVE	MAVE DIRE	CTION BETHEEN	0.151 GHA 0.10	PLOT	SYMBOL PLUS	
,	NUMBER	ND, OF DATA	MEAN		ST, DEVIATION	
	MUMBER					
	2	10	912.	1001.	543,	5- Party (44.4) 11.11
	3	12		1001.	1112	and the same to the same to
	•	179	1612.	1933.	1067.	
	:	158	2010.	1939.	992.	
	1	108	3090.	3370.	1346.	
		35	2915.	3651	2470.	
	10	:	3215.	3263.	563.	
	11				310.	
	15 "	0.				
		CTION BETWEEN 1			SYMBOL X	
	SEAUFORT		21.0 AND 151.0	RMS	ST. DEVIATION	
	NUMBER	NO. UF DATA	nt An		SI, DEVIATION	
	1	12	653,		215,	
	1	45	1476.	1716.	876.	
	•	96	2176.	2406.	1025.	
	•	92	2598.	2980.	1460,	
	;	41	3068.	3726.	2114.	
	•	67	4955.	5386.	2109,	
	10	:	4597.	4623.	493.	
	11	0	4341,	4023,	****	
	15	•				
ELATIVE		CTION BETHEEN 1	51.0 AND 180.0	PLOT	SYMBOL DIAMOND	AND A STATE OF THE PARTY OF THE
	BEAUFURT	NO, OF DATA	HEAN		ST. DEVIATION	
	NUMBER	POINTS				
	!					
	1	20	1499.	1502.	102,	
		42	1985.	2551.	1139.	
	•	24	3064.	3315.	1264.	
	,	52	1555.	2585.	883. 177.	
		15	3554.	3674.	932.	
			4052.	****	484,	
	10					

MUMBER 1 2 3 4 5 4 7 6 7 6 10 11 12 12 13 14 15 16 17 10 11 12	D. OF DATA POINTS 10 12 34 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PLOT BYN. HEAN 1757. 2640. 10950.	### ##################################	8T, DEVIATION 722, 1899, 2004, 602, 1543,	
SEAUFORT NO TO	23 16 12 36 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PLOT BYMMEAN 1757. 2640.	5061. 7592. 5039. 9844. 80L TRIAN RMS	1809. 2204. 602. 1543, 166. 116. 525.	
SPAUFORT NO 1 2 3 4 5 5 7 6 6 1 1 1 1 2	23 16 12 36 8 8 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9	PLOT BYMMEAN 1757. 2640.	5061. 7592. 5039. 9844. 80L TRIAN RMS	1809. 2204. 602. 1543, 166. 116. 525.	
SPAUFORT NO 12 2 3 4 5 5 6 7 7 6 9 10 11 12 12 12 12 12 12 12 12 12 12 12 12	23 16 12 36 8 8 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9	PLOT BYMMEAN 1757. 2640.	5061. 7592. 5039. 9844. 80L TRIAN RMS	1809. 2204. 602. 1543, 166. 116. 525.	
SEAUFORT NO NUMBER	10 12 34 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PLOT BYM. MEAN 1757. 2640. 10950.	7552. 5039. 9844. BOL TRIAM RHS	2204, 602, 1543, 1543, 1543, 1144, 525,	
SEAUFORT NO	36 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PLOT BYMMEAN 1757. 2640. 10950.	5030. 9844. 80L TRIAN RMS	602, 1543, (GLE 87, DEVIATION 114, 525,	
SEAUFORT NO NUMBER	0.0 AND 20.0 0. OF DATA POINTS	PLOT SYMMEAN 1757. 2640. 10950. 14550.	FOL TRIAM RHS 1760. 2691.	114. 525.	
SPAUFORT NO NUMBER	0.0 AND 20.0 0. OF DATA POINTS	1757. 2640. 10950. 14550.	1760. 2691.	116. 525.	
SEAUFORT NO NUMBER 15 3 4 5 5 6 7 7 6 9 10 11 12	0.0 AND 20.0 D. OF DATA POINTS	1757. 2640. 10950. 14550.	1760. 2691.	116. 525.	
BEAUFORT NO NUMBER	POINTS O O O O O O O O O O O O O O O O O O O	1757. 2640. 10950. 14550.	1760. 2691.	116. 525.	
BEAUFORT NO NUMBER	POINTS O O O O O O O O O O O O O O O O O O O	1757. 2640. 10950. 14550.	1760. 2691.	116. 525.	
NUMBER 1 2 3 4 5 6 7 6 9 10 11	POINTS 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1757. 2640. 10950. 14559.	1760. 2091.	116. 525, 1507,	
1 2 3 4 7 6 7 6 9 10 11	0 0 0 0 0 0 0 0 0 0 0 0	10950. 14550.	11065,	1507,	
3 6 7 6 10 11	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10950. 14550.	11065,	1507,	
5 6 7 6 10 11 12	0,0 AND 25,0	10950. 14550.	11065,	1507,	
10	0,0 AND 25,0	10950. 1455 0 ,	11045,	1507,	
10	0,0 AND 25,0	14550,			
11	0,0 AND 25,0	14550,			
11	0.0 AND 25.0		14617.	1303.	
12	0.0 AND 25.0				
27 BPELO BET-EEN 20					- N. Mary 1
27 2720 021-02- 00		PLOT SYM	80L PLUS		
BEAUFORT NO	O. OF DATA				1. 40.00
NUMBER	POINTS	MEAN	RHS	ST. DEVIATION	
1					
3	56	3034.	3074.	2346.	***
•	155	4236.	4871.	2405.	
	130	5386.	5782.	2623.	
	76	11730	12405.	3396.	
1	12	17374.	15507.	3160.	
11	0	.,,,,	1/30/.	£130.	
15	•				
IP SPEED BETHEEN 25	5.0 AND 30.0	PLOT 874	BOL X		
REAUFORT NO	D. OF DATA	HEAN	RHS	ST. DEVIATION	
NUMBER	POINTS				
1	.0		****		
;	80	3979	2016.	1364.	
	162	4473.	5500.	3136.	-
	43	4034.	4426.	1823.	
	74	4790.	5045. 7754.	3768.	
•	31	12404.	13105	4400.	
10	20	9697.	10357	3540.	man of many and
13	•				
1P SPEED BETHEEN 30	0.0 AND 35.0		BOL DIAMO	OND	
DEAUFORT NO	D. OF DATA	HEAN	RHE	ST. DEVIATION	and the second second
PUMBER	POINTS				11. M. S C
1	.;	1003. 2553. 2606. 3160. 4267. 3003.	3060. 2060. 3071.	1486 955 1417 1372 2256 2020	
	#	2606;	2966	*55	
	90	3160,	3471	1417	
•	126	1993,	4587.	2254,	
	126 67 16	\$300. 5946.	6720.	3132,	
,;	:				

LATIVE MAVE OFF	CTION BETHEEN -	0.0 440 11		HOOL OCTABONAL	
		0.0 x40 31			
REAUPONT	POINTS	HEAN	RH8 3	T. DEVIATION	************

	10	5101,	3850.	1025	
i	10	5231.	5428.	1451.	
	07	4351.	5332.	3080.	
	44 57	4477.	5140.	2525.	
i	20	7271.	7555.	1976.	
• • • • • • • • • • • • • • • • • • • •		9900.	10811.	4522	
10	:	17677	17730	1377.	
11	0		,,,,,,		
18	•		-	The same of the sa	
LATIVE WAVE DIRE	CTION APTHERN 3	1.0 AND 61.	.0 PLOT SY	HBOL TRIANGLE	
BEAUFORT	NO. OF DATA	MEAN	RMS S	T. DEVIATION	
				A PROPERTY OF	
1	3	585,	587,	56,	
j	24	3770.	4200	1997.	
- ;	110	3747	2761.	1612.	
1	32	4020-	4306	1545.	
1	50	4609.	9092.	2186.	
:	75	11755.	12210.	3305	
10	12	15081.	15556	2116.	
11	0	A			
15	•				
471VE 41VE 01H	CTION BETWEEN 6			4001 Pt 118	
BEAUFORT	NO. OF DATA	MEAN	*H3 3	T. DEVIATION	
- tynaca		14,000,000			
1	0				
	10	2110.	2469.	1261.	
	179	3630	4861	2526.	
i	190	4543.	5094	2303.	
•	120	4053.	4620.	2218.	
;	108	6440.	7699.	3236.	
•	*	8172,	8599.	2678	
10	•	6487.	7211.	1784,	
15	0				
LATIVE MAVE DIRE	ECTION BETWEEN 12	21.0 AND 151	.0 PLOT SY	-80L X	
BEAUFORT	POI TE	MFAN	P . 5	T. DEVIATION	
			To Carrie and		
1	12	1545.	1601.	420.	
,	45	3173.	1594.	1088.	No. 111 - \$1800 - 1110 - 1 1 1 1 1 1 1 1 1
•	96	4914.	5510.	2504.	
:	52	5764.	5109	1094	
1	47	6524.	7699.	4081.	
	67	10109.	10098.	4071.	
10	:	10246,	10272,	736.	
11	:	102.0	102/2,	1301	
15					
	****** ******				
	COTION BETWEEN 15		O PLOT BY		
BEAUFORT	NO. OF DATA	HEAN	****	T, DEVIATION	
1	•				
	**	3207.	5354		
	20	4001.		2204	
,	**	3203	7410.		
	50	3503	7410	1010	Treatment of the second of the
	12	1990.	7700.	1666,	
•	1;	9667;	9805	1745.	
10			**************************************	CARLON CONTRACTOR CONT	-
11	0				

ONS LONGITUDINAL	HORIZONTAL	BENDING	STRESS	V 9	REAUFORT	NUMBER

	1.0 AND 15.0		OCTA	ONAL	VII
BE AUFORT NUMBER	NO. OF DATA	MEAN	RHS	ST. DEVIATION	
1					
:	23	1006	1620.	215. 507. 542. 174.	
5	. 10		2000.	542.	and a second contract of the second contract
•	15	1520,	1530.	174.	
1	36	2469.	2463.	263.	
9	•				
10	•				
11	:				
SHIP SPEED BETHEEN	15.0 AND 20.0	PLOT SYMBOL	TRIA	AGLE	
BEAUFORT	NO. OF DATA	MEAN		ST. DEVIATION	
NUMBER	PUINTS	ne an	mm3	er. perialion	
1					
;	•	520.	521.	29,	
		695.	696	22,	
•	•				
;	0		10 ages 40 mass		
		1740.	1754.	224,	
10	•	1374.			
11	•	13/4.	1375.	63.	
15	-	****			COLUMN TO STATE OF THE STATE OF
SHIP SPEED BETHEEN	20.0 AND 25.0	PLOT SYMBOL			A CONTRACTOR OF THE PARTY OF TH
BE AUFORT NUMBER	NO, OF DATA	MEAN	RMS	ST, DEVIATION	The common and the second of the common and the com
1	0		220		N
3	54	729.	759.	309,	
	157	A 20			to the company of the state of
5	138	1062.	1127.		
;	75	1103.	1200.	473. 546.	
	78	1796.	1833.	364.	
10	15	1531.	1575.	366.	and the second second
	0	1000.	1603.	101.	
15	•				
SHIP SPEED RETHEEN	25.0 AND 30.0		×		
REAUFORT	NO. OF DATA	MEAN	RHS	ST. DEVIATION	
1	0	325,	401.	235,	
,	16	714.	808.	377.	
:	161	765.	861.	395.	
:	171	793.	932.	344.	
7	74		1286.	450.	No harpes Makindara (1.16
:	52	1200.	1316.	360.	
10	20	1736.	1766.	321.	
11	0		14111		CONTRACTOR AND ADDRESS OF THE PARTY OF THE P
SHIP APELD BETHLEN	10.0.110.11			(E) HINTHE	
BEAUFORT	30,0 AND 35,0	PLOT SYMBUL			and the transfer of the state o
BEAUFORT	NO, OF DATA	MEAN	RHS	ST. DEVIATION	
!		653,	660,	95.	
;	22	475, 637, 640,	504.	190	
4	100	640.			er ode state trad dan in the spectal dealer of the trade of the state
1	90	991.	1019.	200.	
;	125	1008,	1030,	367.	
	10	1297	1186.	469,	
10	0				NOT THE RESIDENCE WHILE SHEET AND A SECOND STATE OF THE SECOND STA
11	0				
12	0				

RMS LONGITUDINAL	MURTZONTAL	MENDING	STRESS VS	BEAUFORT	NUMBER

MECALIAG MAAG CIN	ECTION BETAFEN	0.0 AN	0 31	. PLOT	STHBOL	CCTAGO
REAUFORT	NO. OF DATA	HE		RHS	ST. 0	EVIATION
			53.	660.		95.
2	50	3	95.			
	4.6	1	00.	787		
;	88 71	;	50.	846.		314.
•	58	7	46,	859.		426.
	23			1360.		425
:	50	13	30.	1450.		
10	16	17	37,	1775		200.
11	0	.,	• • •	1334.		200.
RELATIVE WAVE DIR	FCTION METALEN	31.0 AN	0 61	.0 PLOT	SYMBOL	TRIANGL
BEAUFORT	NO. OF DATA	ME		RMS		VIATION
NUMBER						
;	:	,	11,	114.		15,
,	25			A15.		
•	100	5	54.	484		
	15	7	50.	748.		271.
;	48			1067.		
•	32	17	65.	1801.		362.
•	15	10	10,	1639.		259.
10		14	50.	1453,		94,
iż	i					
RELATIVE WAVE DIN	ECTION BETHEEN	61.0 AN	0 121	.0 PLOT	SYMBOL	PLUS
BEAUFORT	NO. OF DATA	HE	AN	RHS	sT, 00	MOITALLA
,						
2	10	:	27.	904.		219.
	179	7	08.	786.		
	189	10	03.	1110.		
÷	128	9	56,	1045.		420.
,	108	16	35.	1808.		709.
•	,,	17	99.	1818.		262.
10		15	02,	1520.		229,
11	•					
MELATIVE PAVE DIR	ECTION BETHEEN	121.0 AN	0 151	.0 PLOT	STABOL	×
BEAUFORT	NO. OF DATA	HE		RHS	87, 01	VIATION
1						
3	12		67.	495.		162.
		6	77.	1065.		223.
5	96			1214.		422.
	52	10	72,	1212.		516.
,	49	13	72,	1469.		526.
:	•7	10	37.	1678.		371.
10		20	54,	2058,		131,
11	0					,
RELATIVE MAVE DIR	ECTION BETWEEN	151.0 AM	0 180	.0 PLOT	37#80L	DIAMOND
BEAUFORT	NO. OF DATA	HE		RMS		MOITALLA
1	0					
1		•	27.	1265. 1150.		91.
1	50	11	47.	1265.		
;	45	10	50,	1371.		451.
	50			1132.		485.
,	52	11	53,			293.
:	12,	15	53.	1565.		301:
		13		13/4		3011
10						
10	:					

VIII

MAXIMUM LONGITUDINAL MORIZONTAL BENDING STRESS VS BEAUFORT NUMBER

BHIP APEEN HETAFEN	1.0 AND 15.0	FLOT SYMBOL	OCTAGO	MAL
REAUFORT	POINTS	MEAN	RHS :	ST. DEVIATION
3	0	3520.	3552.	478.
•	73	2548.	2718	1001.
:	16	4221. 3316.	4403. 3354.	1253.
7	36	5324.	5393.	858.
•	0			
10	0			
11	0			
		PLOT 34480L	TRIANGL	
SHIP SPEED BETWEEN	15.0 AND 20.0	MEAN .		ST. DEVIATION
NUMBER	NO. OF DATA	nea.		
1	0			
1	0	1154.	1155.	62.
•	4	1530,	1533.	93.
	0			
7	0	4193.	4297.	943.
8 9	0			
10	•	2932.	5933.	43.
15	ò			
SHIP SPEED BETHEEN	0.05 DHA 0.05	PLOT SYMBOL	PLUS	
BEAUFORT	NO. OF DATA	MEAN	RMS	ST. DEVIATION
NUMBER				
1 .	0	1554,	1598.	370.
i	54	2248.	2378.	771.
5	157	2371.	2536.	900.
	75	2479.	2586.	1033.
7	79	3033.	3252.	1173.
•	15	3461.	3579.	913.
10	12	3584.	3599.	326.
15	ò			
SHIP APELO BETAFEN	25.0 AND 30.0	PLOT SYMBOL	x	
BEAUFOMT NUMBER	NO. OF DATA	HE AP	RHS	ST. DEVIATION
1	0			
	16	792.	921.	471. 895.
	161	1715.	1477.	801
5	171	1781.	1999.	908.
7	74	2661.	2849.	1016.
	52	2866.	2977.	805.
10	20	3771,	3892.	964.
11	0			
SHIP RPFED BETHEEN	30.0 AND 35.0	PLOT SYMBOL	DIAMON	0
REAUFORT		MEAN		ST. DEVIATION
NUMBER	NO. OF DATA			or, berranda
!	22	1704.	1835.	475.
3	47	1116.	1450-	424.
;	100	1424.	1569,	646.
	125	2175.	2159.	040.
,	67 16	2976.	3239,	612.
•	0	21/0,	3234,	1270.
15	0			
11	0			

IX

MAXIMUM LONGITUDINAL HORIZONTAL RENDING STRESS VS BEAUFORT NUMBER

		0.0 AND 31:0			
BEAUFORT	NO. OF DATA	HEAN	RHS	ST, DEVIATION	
1		1709.	1835	670.	
	70	903.		670	
	46	1687.	1579	847.	
	71	1402.	1894.	776.	
	58	1737.	TORG.	969,	
1	23	3043.	1224	1070.	
:	50	3218.	3302.	1030	
- 10	16	3997.	3575	496.	
11					
BEAUFORT		0.16 GMA 0.1	RMS	ST. DEVIATION	with the contract of the section of
NUMBER	POINTS	AE A.		31, 001121104	
;		293.	312,	107;	and the second s
· · · · · · · · · · · · · · · · · · ·	25	1661.	1/68.	546.	
•	108	1229.	1524.	902.	
	72	1697.	1820.	634.	
•	32	2166.	2315	817.	
	35	3937.	4016.	800.	
•	12	3769.	3824.	650.	the second second second
10		3515*	3233.	376,	and the second section for the first of the second
12	•		*		
FLATIVE WAVE DIR	ECTION BETWEEN 6	0.151 ONA 0:1	PLOT	SYMBOL PLUS	
REAUFORT	NO. OF DATA	HEAN	RHS	ST. DEVIATION	
	0				
	10	932,	1046.	474,	
3	70	1831,	20A0.	731	
;	179	1599,	2467	1077.	
	128	2155,	2359.	960,	
,	108	3640.	3950.	1532.	
:	35	2947,	3235.	1210.	
10	:	4355, 3328,	3370.	725.	and the second second
11	0				
	FCTION BETHEFN 12	1.0 AND 151.0	PLOT	SYMBOL X	
REAUFORT NUMBER	NO. OF DATA	MEAN	RHS	ST. DEVIATION	
1	0				expectation and account of
3	12	1725,	1315.	475. 528.	
	96	2195,	2011	997.	
	91	2449,	2693.	1171.	
:	55	2412.	2675.	1156.	
7	69	3001,	3229.	1193.	
		22241	3020.	•11.	
10		5300,	5336.	*555	
11					
REAUFORT	NO. OF DAYA	1.0 AND 180.0	PLOT	SYMBOL DIAHOND	
NUMBER	POINTS			31, 00111104	
. 1	:	1895,	1902.		
;	20	2547.	2806.	1177	
	45	2302.	2480.		AND AND AND AND AND ASSESSED AS A SECOND OF THE RESIDENCE AS A SECOND OF T
•	24	2936.	2204	608-	
,	20	2464.	2300	1101.	
	12	3372.	3423	589.	
10	7	3460,	3584.	935.	

In settu	RET-PEN	1.0 440	15.0		00 740	ONAL	
AFAU	FORT	NO. OF DA	**	MEAN		ST. DEVIATION	
	1						
	-			501.			
		55		344.	372	133,	
	•			534.	372	137,	
	;	12		609.	474.	60.	
		0					
	10	0					
	11						
IP SPEED	AFTHEEN	15,0 440	20.0	PLOT SYMBOL	TRIAN	1GL 6	
4740	FRET	40, OF 04		HEAM		ST. DEVIATION	
M	1	POINTS					
	3	:		192.	193	17.	e deposition of an agreement and a second of
	•			211.	277.		
	•						
	,	0		444.	455	- 43;	
	9						
	10			463.	484.	30.	**************************************
	15	•					
1P 3PFF0	RETHEEN	20.0 AND	25.0		PLUS	Object Committee of the	
	PORT	40. OF 04	7.4	MEAN		ST. DEVIATION	
	- 46.4						
	,			275.	282.	70,	e de la la companya de la companya d
	3	55		366.	376.	86.	
	5	156		344,	334.	172.	
	6	75		398.		151.	
		77		753.	588. 773.	221	NOT THE OWNER OF THE PARTY OF T
	•	15		565,	574.	97.	
	10	15		603,	.05.	51.	
	12	o					
	9ET#F#	25,0 440	30,0	PLOT SYMBOL			
***	POPT	40. 05 PA	**	HEAN		ST. DEVENTION	
	1					47.	
	3	73		120.	138	108.	
	•	159		774	317.	159.	
		43		302.	363.	747.	
	:	75		427. 549.	977.	213.	
	•	11		661.	675.	238.	
	10	20		964.	943.	•••	the second secon
	12	ő			- period and		**************************************
-	RETHEEN	10.0 AND	35.0		DTANC)ND	
964	FORT MAFR	NO. OF DA	**	MEAN	***	ST. DEVIATION	rent secular (second
	1	.:		211.	.212.	111	*****
	3	10		746.	247	40.	
	4			246. 254. 275. 374.	207.	112.	
	:	118		379.	176	156.	
	1	78		140	177	101:	Committee of the Commit
	*	16		454.	442.	141.	
	10	0					

ME MIDSHIP TORSTONAL SHEARTHG STHESS VS BEAUFORT NUMBER

RELATIVE WAVE DINE		0.0 AND 1	11.0 PLOT	SYMBOL OCTAGONAL
BEAUFIDET	NO. OF DATA	MEAN	***	ST, DEVIATION
		211.	212.	13.
	12	117.	139.	76.
i	45	117.	281.	71:
•	79	250.	270. 375.	104.
•	70	331.	375.	176.
;	61	557.	645.	162,
	20	729.	707.	321.
•	10	639.	651.	125.
10	16	504.	544.	64.
11	0			
RELATIVE HAVE DIREC		31.0 AND 6		SYMBOL TRIANGLE
REAUPORT	POINTS	MEAN	RHS	ST. DEVIATION
1	•			
;	24	315.	321.	60.
	97	776.	250.	
5	71	257.	275.	99,
•	24	170.	405	165.
7	31	344.	TYA.	177.
:	35	563.	629. 571.	101.
10		517.	519.	12;
11	0			
12	0			
RELATIVE WAVE DIREC	TION BETHEEN	61.0 AND 12	1.0 - PLOT	SYMBOL PLUS
REAUFURT	NO. OF DATA		945	ST. DEVIATION
MAHER	POINTS			
1	0			
2	63	243.	313.	133.
•	177		297.	
5	178	372.	422.	200.
•	127	369.	412.	103.
!	110	522.	500.	202.
:	35	500.	763.	148.
10	*	552.	556.	74,
ii	0			
15	0			
RELATIVE -AVE DIREC	TION RETHERN	121.0 440 15	51.0 PLOT	34480L X
HEAUFORT	HO. 05 0454	YEAV	0-9	ST. DEVIATION
*11-46	POINTS			81, 021141104
1			7	
,	12	197.	204.	53.
	45	353.	307.	156.
,	91	102	419.	
•	52	392.	431.	182.
!	4.6	253.	501.	276.
:	67	745.	769.	188,
12		732.	735.	45.
11	:			
RELATIVE HAVE DIREC				SAMONT DIVIDUA
REAUFORT	POINTS	MEAN	RHS	ST. DEVIATION
1				
ż		337.	330,	35,
,	20		366.	140
•	. 24	350.	366. 375. 470.	111.
	. 24	331.	362.	106.
· ·	, 51	459	475.	120.
	12	756.	774.	145.
•	,	614.	955'	97.
10	0			
11	0			
16				

IIX

	EEN RETHEEN	1.0 AND 15.0	PLOT SYMA	OL OCTAG		X
		NO. OF DATA	MEAN	PH8	ST. DEVIATIO	·

	,	;				
	1	22	798.	1130.	101,	
	,	16	1399.	1464,	450.	
	•	.15	1005.	1081.	107.	
		33	1639.	1665.	3134	
	•	•		-		
	10	:				
	15	ě				
SHIP 5		15.0 440 20.0		OL TRIAM	10LE	we consider the control of the contr
	REAUFORT	NO. OF DATA	HEAN	- AM5	ST. DEVIATION	•
	1	•				***************************************
	;	:	436,	449,	107.	
		•	623,		41,	**************************************
		:	-			
	;	i				
			1666,	16454	246,	
	10	:	1287.	1295.		
	11	•				
						the state of the same and the same and appropriate for modern and account of
3+1P 3	PEED METAFEN	20.0 AND 25.0	PLOT SYMB	or seed and this events		
	MEAUFORT NUMBER	POINTS	MEAN	RMS	ST. DEVIATION	
	-0	7.114.9				
	1	0	- 10 1		**********	the company of the state of the company of the state of t
	1	53	562. A74.	572.	105.	
		154	714.	762.	309.	
	- 5	133	A91.	452.		
	;	75	1237.	1041.	402.	
	:	78	1631.	1672.	369.	
		15	1466,	1487.	538,	
	10	12	1581.	1596.	531.	
	15	•				
		25,6 AND -30,6		IOL X		
	-	NO. OF DATA	PFAN	***	ST. DEVIATION	
					The second	The state of the second st
	ż	16	262.	- 139.	100.	the later transfer decreased transcription and the second
	1	73	584.	651.	288	
	;	150	735.	744.	377.	
		45	M31.	*86.	410-	Contraction of the Contraction o
	1	73	970.	1073.	456.	
	•	31	1565,	1351.	321.	
	10	20	1013.	1439.	2917	
	11	;				the wint control relations assessed in one of the control of the
8HIP 5		30,0 AND 35.0		OL 014") H D	THE RESIDENCE OF CONTRACT OF C
	REAUFORT	NO. OF DATA	HEAN	***	ST. DEVIATION	· · · · · · · · · · · · · · · · · · ·
		*******	450.	451.	34 ,	
	;	10	566.	582.	134.	
		::	565.	807.	150	
	;	::	404.	- 707.	200;	The second secon
	;	118		452.	356.	
	,	74	1101	452. 467.	121:	The second of th
	:	10		1100.		CONTRACTOR AND

MAXIMUM MINSHIP TORSTONAL SHEARING STRESS VS BEAUFORT NUMBER

				SYMBOL OCTAGONAL	
HEAUFIRE	POINTS	MEAN	#45	ST. DEVIATION	
		450,	491.	34.	
,	15	264.	330.	100;	
,	45	599	677,	246.	-
;	70	809.	921.	201.	
	61	703.	ASQ.		
1	21	1554.		6651	
:	50	1572,	1672.	262	
10	16	1476.	1498.	256,	
11	0				
15	•				
TIVE -AVE DIR	FETTON HETHERY 3	1.0 AND 61.	.0 PLOT	SYMBOL TRIANGLE	
HEAUFORT	NO. OF DATA	MEAN	HM3	ST, DEVIATION	
MINNER	POINTS				
;	0				
	24	725.	741.	152,	
•	• * *		597.	284.	
:	71	642.	711.	305,	
,	31	AOA.	891.	115,	
	35	1539.	1571.	318.	
	15	1476.	1501.	260.	
10	8	1362,	1396.		
15	•				
TIVE MAVE DEP	ECTION HETHEEN 6	1.0 AND 121.	0 PLOT	SYMBOL PLUS	
REALIFORT	NO. OF DATA	MEAN	845	ST. DEVIATION	
NIJMBER	POINTS			-	
!	0	***			
;	63	520.	526.	45. 367.	
4	177	621.	711	345.	
5	178	*65.	971.	445.	
;	127	1213.	935.	432.	
	110	1172.	1311.	565.	-
•		1725.	1/51.	299.	
10		1313.	1326.	183,	-
15		THE PERSON NAMED IN			-
	ECTION RETWEEN 12				
REAUFORT	NO. OF DATA	MEAN	PHS	ST. DEVIATION	
MIJUMER	POINTS				
1	12	484.			
1	45	574.	515.	256.	When the car
	94	003.	A79.	358.	
5	•1	044	I A S A	400.	
;	52	1156.	1347.	450.	
	67	1592.	1644.	410.	
•	0			The second secon	
10	;	1797.	1799,		
12	•			Carrier and the contract of the second second of the second secon	
TIVE -AVE 010	FETION HETHERN 15	1.0 AND 180.	0 PLOT	SYPHOL DIAMOND	
RELIFORT	POINTS	META	Br2	ST. DEVIATION	
MINHER			N 43 14 14 14 14 14 14 14 14 14 14 14 14 14	The state of the s	
1		646.	449.	.614	
. !	20	780.	847	370.	***
;	48	1058	1091	264,	
;	20	1058.	814.	344,	
,	51	1036.	1070.	527:	
		1374	1660	127.	
	15	1344	1177	744	
.:	1	1144,	1378.	286,	

### SPECIAL PROPERTY OF THE PR	FOR AND AMERICAN	TH 35-01 HT VS HEA	UFORT NUMBER			
### ST, DEVIATION ### POT ST ### POT ST ### POT ST ### POT STPBUL TRIANGLE #### PLOT STPBUL TRIANGLE #### PLOT STPBUL TRIANGLE #### PLOT STPBUL TRIANGLE ###################################			PLOT AVEAU	05146	0441	
### 1975 1864 205 205 215						
1572 1684 225 22		POTNES	4614	***	ST. DEVIATION	
19	,					
1176, 1246, 227, 227, 228, 227, 128, 227, 228,		0			100	
### SPEED RETURN 10,0 AND 20,0 PLOT SYMBOL TRIANGLE ***READFORM POTATA** ***NORTH POTATA** ***PAINTING** **			1170.	1249.	437	
### SPEED RETURNS IN, A AND 35, A PADE SYRBOL TREAMGLE Reading		16	1609.	1663.	422.	
SMIP SPEED METATERS IN.O AND 20.0 PLOT SYMBOL TREAMGLE Readford M.O. 19 PATA MEAN 95 ST, DEVIATION NUMBER 90 10 10 10 10 10 10 10 10 10 10 10 10 10			1317.	1324,	113,	
SMIP SPEED METHERN IS, A AND 20.0 PLOT SYMBOL TRIANGLE READFIGURE NO. OF PATE PEAN GRS ST. DEVIATION MUMMERY PAINTS 2190. 415. 436. 24. 23. 24. 25. 20. 2190. 2405. 140. 20. 2190. 2405. 140. 20. 2190. 2405. 140. 20. 2190. 2405. 140. 20. 2190. 2405. 140. 20. 2190. 2405. 140. 20. 2190. 2405. 140. 2190. 2405. 140. 20. 2015. 2158. 775. 2015. 2158. 775. 2016. 2158. 250. 2017. 2158. 250. 2018. 2408. 240. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2019. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408. 2408. 2019. 2408.			erne.	2213.		
### SMEED METATERS (N.) AND 20.0 PLOT SYMBOL TRIANGLE REARITION ***REARITION ***R	,					
SMIP SPEED METHERN IN, OF DATA PLAN SYMBOL TRIANGLE READFRIGHT NO, OF DATA PEAN GAS, 3T, DEVIATION NUMBER PRINTER 1						
PRESENTED NO. OF DATA PEAN GRS 3T, DEVIATION NUMBER OF STREET STATE STATE OF STATE	11					
READERS NO. OF DAYA PEAN ORS ST. DEVIATION	SHIP SPEED HETSELS	15.0 440 20.0	PLOT SYMBOL	TRIAN	GLE	
	REAUFIRE	NO. OF DATA			ST. DEVIATION	
### A	MUMH) Q					
### ### ##############################	1					
### ### ##############################	•		415.	436.	50.	
### ##################################			641.	643.	23,	
### A			*			
### SHIP SPEED RETUREN 20,0 AND 25.0 PLOT SYMBOL PLUS ### PAINTINET NO. OF OXIS HEAN RMS ST. DEVIATION ### PAINTINET NO. OF OXIS HEAN RMS ST. DEVIATION ### PAINTINET NO. OF OXIS HEAN RMS ST. DEVIATION ### PAINTINET NO. OF OXIS HEAN RMS ST. DEVIATION ### PAINTINET NO. OF OXIS HEAN RMS ST. DEVIATION ### PAINTINET NO. OF OXIS HEAN RMS ST. DEVIATION ### PAINTINET NO. OF OXIS HEAD SO. O. PLOT SYMBOL Y ### PAINTINET NO. OF OXIS WISH SO. O. PLOT SYMBOL Y ### PAINTINET NO. OF OXIS WISH SO. O. PLOT SYMBOL Y ### PAINTINET NO. OF OXIS WISH SO. O. PLOT SYMBOL Y ### PAINTINET NO. OXIS WISH SO. O. PLOT SYMBOL Y ### PAINTINET NO. OXIS WISH SO. O. PLOT SYMBOL Y ### PAINTINET NO. OXIS WISH SO. OXI	,	0				
SHIP SPEED RETURN 20.0 AND 25.0 PLOT SYMBOL PLUS PRANTICUT 10.0 F OATA NUMBER PRINTS 1 0 0 10.0 AND 120.5 1302. 500. 1 10.0 120.5 1302. 500. 2 10.0 120.5 1302. 500. 3 10.0 120.5 1302. 500. 3 10.0 120.5 1302. 500. 4 10.1 90.0 1002. 500. 5 140 120.5 1370. 576. 6 7 77 1191. 1207. 450. 7 7 77 166. 1665. 764. 8 7 7 27 126. 1655. 764. 8 7 7 27 126. 1655. 764. 9 12 300. 3017. 474. 11 0 12 3000. 3017. 474. 11 0 12 3000. 3017. 474. SHIP SPEED RETURN 20.0 PLOT SYMBOL X 4 10.7 10.5 120. 605. 10 10 10. 10. 1205. 605. 11 10 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1205. 605. 11 17 10. 1955. 615. 12 10 20 2052. 2360. 704. SMIP SPEED RETURN SO.0 AND 35.0 PLOT SYMBOL DIAMOND REQUERIES NO. AND 35.0 PLOT SYMBOL DIAMOND RESURES NO. AND 35.0 PLOT SYMBOL DIAMOND RESURES NO. AND 35.0 PLOT SYMBOL DIAMOND RESURES NO. AND 35.0 PLOT SYMBOL DIAMON			534W.	2403.	144.	
12 0			2015.	2150.	775,	
SHIP SPEED RELIEFS 20.0 AND 25.0 PLOT SYMBOL PLUS PRINCIPLY 40. OF OXIA HEAM RMS ST. DEVIATION NUMBER 40. OF OXIA HEAM RMS ST. DEVIATION 1	11					
### ##################################			D. C			
			77 7.50			
1		POTETS		RMS	ST, DEVIATION	
1	1					
181 966, 1092, 506, 576, 140 1707 1711, 1207, 430, 576, 177 1191, 1207, 430, 77 1191, 1207, 430, 77 171, 1666, 1845, 784, 784, 784, 784, 784, 784, 784, 784			619.	624.	85.	
140			966.	1092.	506.	
7 77 1666. 1845. 784. A 7A 2719. 2850. 856. 9 12 3248. 3272. 395. 10 12 3866. 3917. 474. 11 0 12 3666. 3917. 474. 11 0 12 3666. 3917. 474. 11 0 12 3666. 3917. 474. SHIP SPEED RELIEF 25.0 AM 50.0 PLOT SYMBOL X		140	1243.	1370.	576.	
A 7A 2719, 2850, 856, 9	•		1191.	1267.	430.	
12 3248, 3272, 3495, 101 10 12 3868, 3017, 474, 111 12 16 12 16 17 17 17 17 17 17 17			2719.	2850.	856.	
SHIP SPEED RETURNS 25.0 AND 50.0 PLOT SYMBOL X REALBORY TO, IF DATA TARE TO A ST. DEVIATION 1 0 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 322. 1 10 303. 485. 356. 2 10 10 10 10 10 10 10 10 10 10 10 10 10		12	324A.	3272.	395.	
SHIP APPEN DETIFIED 25.0 AND 50.0 PLOT SYMBOL X HAS ALBORY 100. F DATA 1673 AND 50.0 PLOT SYMBOL X 1 0 305. 405. 322. 1 10 305. 405. 322. 2 16 305. 205. 405. 3 107 1030. 1244. 606. 3 107 1030. 1244. 606. 3 107 1037. 1224. 652. 3 10 107 107. 1224. 652. 4 51 1768. 1055. 815. 4 51 1768. 1055. 815. 10 20 2252. 2360. 704. 11 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			3888.	3917.	474.	
1		÷				
1		25.0 440 50.0	PLOT 54800	. *		
1	KF 4 - 4 - 10 T		EAL	B45	ST. DEVIATION	
2 16 305. 465, 322. 4 107 1030, 1244, 606, 5 162 1037, 1224, 606, 6 4 5 661, 931, 1266, 1566, 7 165 1266, 1566, 1566, 9 35 2672, 2622, 910, 10 20 2252, 2360, 704, 11 0 0 SHIP SPEED RETHERN SO, A AND 35,0 PLOT SYMBOL DIAMOND REAUFIRET NO. 11F 0474 HEAN RMS ST, DEVIATION HIMBER PRINTS 1 2 574, 652, 310, 4 102 667, 761, 327, 5 86, 14, 6 117 652, 960, 466, 7 77 1124, 1245, 537, 6 15 1393, 1506, 576,						
NO		16	363.	485.	355.	
102 1037, 1220, 652, 652, 652, 652, 652, 652, 652, 652	•	*0	A95.	994.	432,	
## 45			1037	1224.	652.	
### 1269 1576		45	ANI.	933.	154.	
35 2672, 2822, 910, 10 20 2252, 2360, 704, 11 0 11 0 12 0 SHIP REFERENT SOLARD 35,0 PLOT SYMBOL DIAMOND REAUFIRET NO. OF DAYA HEAN RHS ST. DEVIATION HUMBER POINTS 1 5 545, 546, 14, 2 22 574, 652, 310, 3 44 617, 652, 210, 4 107 667, 761, 327, 5 66 111, 1664, 314, 6 117 652, 984, 446, 7 77 1124, 1245, 557, 4 15 1393, 1508, 578,	,	**	1269.	15.6.	509.	
10 20 2252, 2360, 704, 11 5 11 5 12 0 SHIP APPEO RETHERN SO,0 AND 35,0 PLOT SYMBOL DIAMOND REAUFORT MOUNTER POINTS 1 2 545, 546, 310, 2 10, 652, 310, 3 40, 617, 652, 310, 4 102 667, 761, 327, 5 66, 117 662, 989, 446, 7 77 1124, 1245, 557, 4 15 1393, 1506, 578,	:	15	2672	2022	910.	
SHIP APPER RETHERN SO, A AND SS, A PLOT SYMBOL DIAMOND REAUFORT NO. OF DATA HEAN RHS ST. DEVIATION NUMBER POINTS 1 9 565, 566, 34, 10, 10, 10, 10, 10, 10, 10, 10, 10, 10		50	2252.	2360.	704.	
REAUFIRT MO. DF DATA HEAN RHS ST. DEVIATION HUMBER POINTS 1	11					
REAUFIRT NO. IF DATA HEAN RHS ST. DEVIATION 1 2 545. 586. 14. 2 22 574. 652. 310. 3 86 617. 652. 210. 4 102 667. 761. 327. 5 86 1011. 1064. 334. 6 117 652. 989. 446. 7 77 1124. 1245. 537. 4 15 1393. 1508. 578.	S-IP APFFO MET-FF	50.0 AND 35.0	PLOT 84480	L DIAM	OND.	
\$ 22 570, 566, 34, \$ 22 570, 652, 310, \$ 40 617, 652, 210, \$ 107 667, 761, 327, \$ 86 1011, 1064, 330, \$ 117 652, 469, 446, \$ 7 77 1120, 1205, 537, \$ 15 1303, 1500, 570,	MEAUFORT	NO. OF DATA	HEAN		ST. DEVIATION	
117 652, 968, 446, 77 1124, 1245, 537, 15 1393, 1508, 578,	MINER	Philais				
117 652, 989, 446, 7 77 1124, 1245, 537, 15 1393, 1508, 578,	1	22	574	652.	310,	
117 652, 989, 446, 7 77 1124, 1245, 537, 6 15 1393, 1508, 578,	i	• • •	617.	632.	510.	
117 652, 989, 446, 7 77 1124, 1245, 537, 15 1393, 1508, 578,		103	1011	741.	327.	
17 1373, 1300, 370,		117	652	989.	446.	
17 1373, 1308, 376.	,	79	1124.	1245.	557.	
10	:		1393,	1508,	578.	
	10					
11	11					
18 0	15	•				

		4.			
DAS FINALAND	QUE AUT . C.	STHESS-PORT	V 9	TRO SUA 38	NUMBER

	CTION NETHER	0.0 AND 31.0	PLOT	SYMBOL OCTAGONAL	
READFORT	NO. OF DATA	MFAN		ST. DEVIATION	
;	20	545.	720.		
•				370:	
•	8.8	466.	1139.	660.	
•	71		1216.	585.	
	61	105A.	1214.	598,	
,	21		1627.	354.	
:	50	1911.	2001.	592.	
10	16	3688.	3702.	183.	
ii	0		3431.	1430.	
15	•				
RELATIVE PAVE DIR	FCTION HETNEEN	11.0 AND 61.0	PLOT	SYMBOL TRIANGLE	
REAUFORT	NO. OF DATA	MEAN	RMS	ST. DEVIATION	
MOMMEN	Prints				
;		102,	104.	16.	
,	20	753.	413.	357.	
4	111	517.	A70.	360.	
•	80	78A.	861.	347.	
,	15	A65.	894.	234,	
	32	2177	1105.	465.	
;	16	2452.	2438.	811.	
10	11	2504.	2667.	917.	
!!	0				
RELATIVE -AVE MIN				SYMANL PLUS	
REAMFORT	POINTS	MFAN	RM3	ST. DEVIATION	
1					
1	10	401.	461.	550.	
4	183	961.	1136.	570,	
	190	1002.	1199,	544.	
	127	MAS.	984.	516.	
,	110		1703	112	
	31	1605.	1997.	1191.	
•	•	2044.	2140.	421.	
11	•	1741.	1768.	309.	
13	0				
	ceson wetaer	121.0 AMD 151.0	PLAT	SYMBOL X	
	PATA			ST. DEVIATION	
1	12	145.	401.	122.	
	97	1114.	1277.	362.	
;	AT	1124.	1525.	756.	
;	44		1211.	468.	
1	41	1710.	2013.	1061.	
•	47	2581.	2724,	882.	
10	:	2996.	****		
11	,	2440,	3018.	365,	
13	•				
PFLATTUF - AVE ATRE		151.0 400 160.0	PLOT	SYMAGE DIAMONG	
8EA-15-19-1	NO. OF DATA	MFAN		ST. DEVIATION	
,					
1		.652.	453.	.17.	
	70		1420.		
;	**	1014.	1500.	626.	
	20	977.		380.	
;	42			425.	
	17			206.	
	,	2405,	2575.	392,	
10					
" "	•				

IIVX

754. W. 4 174v	AMP COLVE	STHE SSOP INT	VA BEAUFORT	NUMBER

BHIR SPECU HETSES	1.0 AND 15.0				
SE SUFURT NUMBER	POINTS	"FAV	***	37.	OF VIATION
1					
3	:				
4	23	3701.	3721		918.
•	16	3769.	3913,		1050
;	15	2616.	3913.		154.
	36	4964.	5028.		100.
	•				
10	:				
13	,				
SHIP SPEFO RETHEN	15.0 440 20.0		TREAM	GLE	
BEAUFORT	NO. OF DATA	MEAN	-	ST.	DEVIATION
NUMBER	NO. OF MATA			• • •	
1	0				
5	:	994.	1001		110.
		1415.	1001.		116.
:	°				
;	0				
•		6037.	6105.		910.
10	?	5023.	5403.		1991.
ii	0				
12	•				
	20.0 440 25.0	PLOT SYMBOL	PLUS		
HF AVE 10 T	POINTS		RMS	87.	DEVIATION
1	0				
. :	30	1353.	1372.		230.
4	161	2158.	2980.		1113.
•	140	2745.	3002.		1217.
;	11		2948.		1411
•	7.0	EGTT	6261.		1705.
12	12	7785.	1877.		1150.
11	:	,,,,,			
8-12 APERD BE1-15-	25.0 AHT 30.0	PLOT SYMBOL			-
NA AMEGINE					
No action	POTNTS		Rus		DEVIATION
1					
;	14	2081.	2345,		1041.
	167	2104	2024		1676.
•	145	5333.			1900.
;	43	2042.	3007		922.
	51	2065. 3064. 6536.	4514.		2515.
10	39	653A.	7003.		2515.
11	•	5405.	4723.		1500,
12	•				
	30.0 440 35.0		01440	40	
4 AUFORT	POINTS	HEAV	-	57.	DEVIATION
- INFR	POINTS				
1	,,	1204.	1513.		133:
1		1271.	1540		
	102		1794.		752.
:	, 117	1000			1000.
i	11	2654.	2276		1365.
	15	3340.	3670.		1510.
10					
!!	•				
1,0					

IIIVX

HANTMON PRINCIPLE SHIP STUPSS-PORT VS BEAUFORT NUMBER

		TION HE IMEEN	0.0 AND 11.0	PLOT	SYMBOL OCTAGONAL	
		POINTS	MEAN	***	ST. DEVIATION	
			1205.			
	;	20		1213.	949.	
	1	4.6		3404		
		88	2251.	2790.	1647.	
	:	71			1306.	
	,	61	3421.	2797.	1401.	
		20		4514	881.	
	•	16	9281.	9350.	1137.	
	10	10	7762.	A158.	2379,	
	11	•				
RELATIVE W	AVE DIRECT	ION HETWEEN 3	1.0 AND 61.0	PLOT	SYMBOL TRIANGLE	
		NO. OF DATA	MEAN	RHS	ST. DEVIATION	
		PEINTS				
	1		213.			
	í	24	1792	1924.	617.	
	4	111	1742.	1504.	806.	
	5	*0	1800	1984	A3A.	
	,	35	1997.	2066	526.	
	*	51	2330.		1126.	
	q	16	4021:	6318.	1710.	
	10	11	6161.	6571.	2285.	
	11	0				
	W. 01055					
		ION HETHERN A			SYMMOL PLUS	
NI NI	IFORT IMMER	POINTS	MEAN	***	ST. DEVIATION	
	!	0				
	?	10	841.	1026.	509.	
	3 4	177	2225.	2592.	1331.	
	5	190		2306.	1304.	
		127	2046	2147.	1114.	
	7	110	3001.	1911	1927.	
	•	11		4570-	2148.	
	10	:	4741.	4000.	1140.	
	11	?	4444.	4592.	935,	
	1)	0				
FLATIVE	VF STREET	104 HETHERN 121	1.0 400 151.0	PLOT	SYMHOL X	
NE 417		POINTS	MFAN	RMS	ST. DEVIATION	
	2	12	A45.	***	251.	
	1		1911.	1615.		
	4	97	2579.	2847.	1107	
	:	67	2922.	1101	1021.	
	;	44	2514.	2708.	1001.	
		67	5387.	2995	2210.	
	•			10.61		
	10	•	6680,	6686.	200.	
	!;	÷				
	VF D185C11	ION HETHERN 151	. 0 AND 180 0	P1 07	SYMBOL DIAMOND	
ME AVE						
NU	unfa	POINTS	MEAN	RM3	ST. DEVIATION	
	;	•				
		20	1576.	3000.	180.	
	1		6,16.	3000	1283.	
	;	49	2572.	2681.	1175.	
	;	49	2712.	2681.	1375.	
	:	20	3660.	3614.	1072.	
	;	20 20 20	2041.	2681. 3814. 2192.	795.	
	:	20 20 20 52	3005.	2681. 3614. 2192. 1537. 4807.	1072. 795. 958. 971.	
	•	20 20 20	2041.	2681. 3814. 2192.	795.	

ANS FORMER SHE LOTING STRESS-STARBOARD VS BEAUFORT NUMBER

SHIP SPEED RETWEEN	1.0 440 19.0	PLAT SYMBOL	OCTAGO	HAL
BEAUFORT NUMBER	NO. OF DATA	MEAN		ST. DEVIATION
1	•			
ŝ	:	1001.	1674;	200;
	23	1161.	1245.	
5	10	1473.	1885	137
;	36	2021.	2453.	235.
	•			
io	:			
ii	0			
18	•			
	15.0 440 20.0	PLOT SYMBOL	TRIANG	
BEAUFORT	NO. OF DATA	MEAN	R48	ST. DEVIATION
1	•			
1	:	490.	491	30.
		612.	491	30.
5	2			
,	0			
	:	2149.	2155.	154.
10		2634.	2634.	145.
11				
12	0			
	21:0 AND 25.0		PLUS	
REALIFORT	POINTS	MEAN	***	ST. DEVIATION
1	0			
1	54	1391.	AP7. 1533. 1173.	1934
4	155	1016.	1173,	245.
:	138	1276.	1244	437
;	77			
;	78	3095.	1314	1178
in	12	3653,	3684.	417.
11	0			
SHIP APEED BETAFEN	25.0 440 50.0	PLOT SYMBOL	×	
AFAUFORT		MFAN		ST. DEVIATION
NUVAFA	POTHTS	,	***	Br. Deviation
2	.0	***		240.
i	16	887.	366.	396.
4	155	303. 667.		577.
:	166	1020	1176	506
!	73			
:	52	1485.	1643. 2727. 2037.	702. 1039. 730.
in	50	1899.	2037.	738.
1;	•			
SHEP SPERO RETREEY	30.0 440 35.0		01440	40
STAUPORT	NO. OF DATA	MEAN		AT. DEVIATION
NUMBER	NO. OF DATA			
1	:	427.	478	311.
	19	494		
	**	1004.	1125	300
	**			
!	• • • • • • • • • • • • • • • • • • • •	1345.	1700.	971.
	0		1,00.	
12	0			
11	0			

XIX

XX

RMS FORWARD AMFARING STRESS-STADROARD VS BEAUFORT NUMBER

RELATIVE MANE DIRECTION RETWEEN 0.0 AND \$1.0 PLOT SYMAPL DETAGRINAL ST. DEVIATION PLOT SYMBOL TRIANGLE RELATIVE WAVE DIRECTION APTHEFN \$1.0 AND 61.0 1010. 701. 850. 867. 987. 2036. 2600. RELATIVE WAVE DERECTION RETWEEN AL. O AND 121.0 PLOT SYMBOL PLUS POINTS 269. 615. 57a. 536. 490. 782. 1519. 231. 230. 364. 847. 1206. 1498. 1299. 1867. 2760. 2110. 337. 2116. RELATIVE MAVE MIRECTION BETHEEN ISL'S AND 180.0

MANTH IN SITULAND	 STOP SE-STABBILLED	VA	4 MP	HAFO

	1.0 440 15.0		DETAG	ONAL
REAMEMET	un, ne hata	MFAN		ST. DEVIATIO
WITH RE M	POINTS			31,
>	,			
•		1152.	7371.	355,
;	21	7494.	4241.	1216.
;	16	1052.	3074.	1216. 367.
:	16	5184.	5238.	713.
	:			
10	0			
11	:			
SHIP SPEED RETHERN	15.0 AND 20.0	PLOT SYMBOL	TRIAN	
RF AUFORT	ED. OF DATA	HEAN	845	ST. DEVIATION
1				
;	0	1042.	1044.	40.
4	4	1257.	1239.	60.
•				
;	ć			
		5251.	5311.	795.
•	•			
10	4	7504,	7571.	1047.
	•			
	24,0 440 25.0	PLOT SYMBOL	PLUS	
AF AUFORT	MO. OF DATA	MEAN		ST. DEVIATIO
404414				
;	:	1452.	1690.	357.
,	54	294A	1204.	1263.
4	15A			1285
	134	2001.	7174.	1492.
;	76	2734. 3595. 6654.	4158.	20A9.
	7.4	6654.	7099.	2444.
, ,	12	7597.	7714	1495.
11	,	0704.	****	1667.
15	•			
SATE SELED HELPER	24.0 AND 50.0	PLOT SYMBOL	×	
4F LIFTIBT	POINTS	PEAN	8+5	ST. OFVIATIO
,	16	445.	848.	568.
. 4	70 155	2070.	5549.	1484.
4	166			1104
;	45		PAGA.	1259.
,	71	2152	7967.	1865.
•	11	6194.	1846.	ZRAA.
11	20	4920.	4241.	1805.
!!				
311 - 45FFD #FT=FF4	30.0 AND 35.0		01440	INO
AF LUFTIPT	NO. OF DATA	MEAN	**5	ST. DEVIATIO
1	4	421.	824.	
	10	1091	1415.	709.
1			1684.	548.
4 5	6.4	1804.	2015.	891. 709.
	**			1149.
,	65	3054.	3005.	1906.
1	17	3721.	4045.	1586.
111				
11	0			
17	•			

XXI

IIXX

HARTMIN FIRELES SHEARING STHESS-STARROARD VA REAUFORT MUNREL

### ### ### ### ### ### ### ### ### ##	-		AND 11.0	PLOT	SYMBOL OCTAGONA
	R	NO. OF 04TA	MFAN		AT. DEVIATION
### ### #### ### ### ### ### ### ### #	NUMATO	POINTS			
### A	!		821.	824,	81.
### ### ### ### ### ### ### ### ### ##		12	2287		634.
### ATT PROTECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMMOL TRIANGLE NEATHER NO. OF DATA NEAN PASS. 1231. ### ATT PROTECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMMOL TRIANGLE NEATHER NO. OF DATA NEAN PASS. 1265. ### ATT PROTECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMMOL TRIANGLE NEATHER NO. OF DATA NEAN PASS. 1 DEVIATION POINTS. 10 PLOT SYMMOL TRIANGLE NEATHER NO. OF DATA NEAN PASS. 1 DEVIATION POINTS. 10 PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAN PASS. 1 DEVIATION POINTS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAN PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAN PASS. 1 D. PLOT SYMMOL PLUS POINTS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAN PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAN PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAN PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL D. PLOT SYMMOL PLUS PRINTED NO. OF DATA NEAR PASS. 1 D. PLOT SYMMOL D. PLOT SYMOL D. PLOT SYMMOL D. P			2441	1049	1489.
### A		6.5			1338.
## 20	;	31	1727	30654	1213.
## 10		50	4531.	4778.	1515.
## A 1		16	9483.	43 a 7 .	1102.
### ATTIVE WAVE DIRECTION RETWEEN 31.0 AND 81.0 PLOT SYMBOL TRIANGLE REALFLOAT WILL ARE AND 81.0 PLOT SYMBOL TRIANGLE REALFLOAT WILL ARE AND 81.0 PLOT SYMBOL TRIANGLE REALFLOAT WILL ARE AND 81.0 PLOT SYMBOL TRIANGLE REALFLOAT RETWEEN 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 PLOT SYMBOL PLUS APAIRED WILL ARE AND 81.0 AND 121.0 AND 122.0 AND 122	10		7734.	P050.	5531.
REALESST NO. OF DATA POINTS 1 0 2 0 1 1164. 2 0 0 2110. 2820. 1184. 4 10 1285. 2006. 1285. 4 10 1280. 2006. 1285. 488. 4 10 1280. 2006. 1285. 488. 4 10 1280. 2006. 1285. 488. 4 10 1280. 2006. 1880. 488. 4 10 1280. 2006. 1880. 1					
1	RPLATIVE WAVE DIRE	CTION AFTHEEN 31	.0 440 61.0	PLOT	SYMANL TRIANGLE
1		POINTS	MEAN	RMS	ST. DEVIATION
1					
10 2110, 2020, 1184, 1285, 408, 408, 1580, 2020, 1285, 408, 408, 109, 109, 109, 109, 109, 109, 109, 109					
## SA 15A2, 202A, 1286, 968, 1971 1996, 1987, 604, 968, 1991, 1997, 604, 1997			2110.	2020.	1184.
### 100 10	4	5A	1542.	2024	1265.
## 120			1946.	2165.	948.
## 12 5050, 6250, 1091. ## 12 6050, 6270, 1466. 10 # 7581, 7651. 1032. ## 12 606. ## 1	;	12		2645.	1360.
## 12	•	15	5954.	4254	1921.
RPLATIVE VAVE DIRECTION RETWEEN 61.0 AND 121.0 PLOT SYMBOL PLUS APALIFORY NO. OF DATA MEAN BAS ST. DEVIATION NUMBER POINTS 1 0 180A. 1921. 00A. 1 10 101A. 212B. 1510. 00A. 1 12 2530. 265. 1539. 1 10 127. 2530. 2662. 1210. 2 1 10 3523. 30A. 17A2. 3 1 10 3523. 30A. 17A2. 4 1 10 3523. 30A. 17A2. 5 1 10 3523. 30A. 17A2. 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				4074	1466.
RELATIVE MANY DIRECTION RETWEEN 61.0 AND 121.0 PLOT SYMBOL PLUS RELATIVE MANY DIRECTION RETWEEN 61.0 AND 121.0 PLOT SYMBOL PLUS RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE MANY DIRECTION RETWEEN 121.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIRECTION RETWEEN 151.0 AND 150.0 PLOT SYMBOL DIAMOND RELATIVE MANY DIAMOND RELATIVE MANY DIAMOND			7501,	7651.	1032.
### ### ### ### ### ### ### ### ### ##					
1	RFLATTVF WAVE DIRE	CTION RETULEN 61	.0 400 121.0	PLOT	SYMADL PLUS
1	AF LUFTRY	NO. OF DATA	HEAN	-	ST. DEVIATION
2	27-47-4				
1	!				
## 160 101A, 217a, 1312, ## 182 219a, 258a, 1210, ## 182 219a, 258a, 1210, ## 127 223A, 258a, 125a, ## 110 3523, 358a, 178a, ## 31 3823, 558a, 3511, ## 4 31 3823, 558a, 3511, ## 8 3823, 558a, 3511, ## 8 3823, 558a, 3511, ## 8 12 4167, 4030, 151,0 PLOT SYMBOL X ## 8 12 40 1850, 2113, 1058, ## 12 40 1850, 2113, 1058, ## 12 40 1850, 2113, 1058, ## 12 40 1850, 2113, 1058, ## 12 40 1850, 2113, 1058, ## 12 40 1850, 2113, 1058, ## 12 40 1850, 2137, 288a, 1075, ## 13 3877, 2830, 2857, ## 14 20 2857, 848b, 601, ## 11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	i	55			
## 187 2894, 2882, 1210, ## 127 2234, 2864, 1254, ## 110 3523, 3984, 1782, ## 31 3823, 3884, 1782, ## 4 3483, 3584, 641, ## 11		149	1914	2124	1412.
### 110		142		2682.	1210.
A 31 SA71, NOSA, 3511, A 3401, 3586, 601, 10 A 3401, 3586, 620, 11 A 3401, 3586, 620, 11 A 3401, 3586, 620, 11 A 3401, 3586, 620, RELITIVE VAVE DISPCTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELITION NUMBER POINTS 1 0 R21, 677, 308, 1 0 R21, 677, 2 0 R21, 677,			1531	256A.	1254.
## A 3483, \$588, 641, 10 11 10 11 10 11 10 11 10 11 10 11 10 10			. 7583	SOSA.	3511.
RELATIVE VAVE DISPECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE VAVE DISPECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X RELATIVE VAVE DISPECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL DIAHOND 1 0 8 1257 2500 2501 2500 2500 2500 2500 2500 2500		A	IGAL.	TSAR.	841.
RELETIVE VAVE DISPECTION RETWEEN 121.0 AND 151.0 PLOT SYMBOL X REALFORT NO. OF DATA MEAN PMS ST. DEVIATION NUMBER POINTS 1 0 R21. A77. 305. 1 0 A6 1550. 2113. 1056. 2 10 R21. A77. 260A. 1075. 5 AA 128A. 1021. 1522. 5 AA 128A. 3000. 006. 7 3A 3A77. 260A. 1075. A A7 5000. A220. 2521. 0 0 0 SA55. BAR6. 601. 11 0 0 A 5455. BAR6. 601. 11 0 0 B SA55. BAR6. 601. REALFORT NO. OF DATA MEAN PMB ST. DEVIATION NUMBER POINTS 1 0 1071. 1027. 157. 2 0 2107. 2010. 1033. 3 07 2777. 2550. 936. 5 24 3164. 1773. 1750. 5 74 3164. 1773. 1750. 6 6 6 3177. 1104. 365. 7 12 24167. 0015.		1	1401.	3548.	450'
### POINTS 1	13				
1	RELATIVE WAVE DIRE	CTION RETHEEN 121	.0 440 151.0	PLOT	зуннов х
1		MR. OF DATA	MEAN	PM3	ST. DEVIATION
10	40-474	bullet 3			
### ### #### ### #### #### #### #### ####	;		421	477	100
1 0 10			1850.	2117	1056.
1 0 10		91	2637.	284A.	1075.
## 10 ## 151.0 AND 180.0 PLOT SYMBOL DIAMOND ### 10 ## 151.0 AND 180.0 PLOT SYMBOL DIAMOND #### 151.0 AND 180.0 PLOT SYMBOL DIAMOND ###################################					1525.
## 67 5000, A220, 2521, 10 4 5453, SAR6. 601, 11 0 0 12 0 0 ### 151.0 AND 180.0 PLOT SYMBOL DIAMOND **REALFORT VO. OF DATA HEAV BHS ST. DEVIATION **REALFORT VO. OF DATA HEAV BHS ST. DEVIATION **POINTS** 1 0 1021, 1027, 157, 2 4 1021, 1027, 2510, 1033, 3 07 2777, 2550, V36, 4 20 2307, 2610, 1033, 5 74 3364, 1773, 1750, 5 74 3164, 1773, 1750, 6 8 3177, 1104, 365, 7 7 52 2777, 3114, 915, 8 12 4167, 4030, 1503, 9 7 462, 4042, 901, 11 0	;	14	3479	3000	2197.
10		67	5690.	A224.	2521.
### 11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0					
### ##################################	11	. 0	3455.	5486.	601.
### ### ### ### ### ### ### ### ### ##	15	0			
1 0 1071, 1027, 157, 157, 1 0 2 0 2 107, 2 10, 1033, 2 0 2 107, 2 10, 2		CTION METHERN 151	.0 AND 180.0	PLOT	SYMBOL DIAMOND
2 4 1071, 1027, 157, 4 20 2107, 2010, 1053, 5 20 3102, 2510, 910, 5 24 3104, 1773, 1750, 6 8 3177, 1104, 365, 7 52 2077, 1114, 915, 6 12 4167, 0010, 1505, 9 7 4862, 0001, 11 0	RELIFORT	MO. OF DATA	MFAN	BH8	ST. DEVIATION
2 4 1071, 1027, 157, 4 20 2107, 2010, 1055, 5 24 3104, 1773, 1750, 6 8 3177, 1104, 365, 7 42 2077, 3114, 915, 8 12 4167, 4010, 1505, 9 7 462, 4072, 4000, 1505, 11 6					
3		4	1971.	1927.	157.
3 74 3164, 1773, 1750, 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		20	2377	2610.	1053.
7 12 2777, 1104, 155, 7 12 12 14 15, 15 15, 15 15, 15 15, 15 15 15 15 15 15 15 15 15 15 15 15 15	,	74			1750.
7 72 2477, 3114, 915, 4167, 935, 4167, 935, 935, 935, 935, 935, 935, 935, 935	•			1108	365.
11 0			2477.		914.
11 6			4862	4940	1503.
	117	*			*****
12 0					
	15	0			

IIIXX

WAS DEAK-TO-THOUGH BOLL ANGLE VS REALFORT MIMBER

	MID WELNE MELMEN	1.0 AND 15.0	PLOT SYMBI	OL OCTAG		
	REALIENRY		METH	945	ST. DEVIATION	
	NIMAFE	POINTS		****	ar. or training	
	,					
	1		6898.	40454	610.	
	•	23	5423.	5723.	1828	
	*	16	7271.	7603,	385	
	;	14	7910.	8006.	1237.	
	•	0				
	•	0				
	10	÷				
	15	0				
8	MID SPEED BETAFFY	15.0 AND 20.0	PLOT SYMA	OL TRIAN	GL F	
	SPAUFORT	NO. OF DATA	HEAN	RHS	ST. DEVIATION	
	NIMAFO	PHINTS				
	1 2					
	í		2030.	2961	429,	
	a	4	3215.	1220.	181.	
	5	^				
	7	0				
	8		5144.	4230:	950.	
	9	•				
	10	4	4141.	4144.	168,	
	11	0				
	'	,				
		20.0 AND 25.0		INL PIUS		
	REALIENRY	POTHTS	MFAH	RMS	ST. DEVIATION	
	HUMBER	h1 w 1.2				
	1	6				
	,	A	4210.	A351.	1016.	
	5 4	55 15A	6111.	4175.	1815.	
		140	. 52A1.	8778	23454	
	4	77	45AA.	4240.		
	,	78	6567.		3091,	
	A .	7A 12	9510.	9749.	2013.	
	10	15	4254.	4302.	928.	
	11	0				
	15					
	SHIP SPEED RETWEEN	24.0 AND 10.0	PLOT SYNB			
	9 AUF OFT	HOL HE DATA	MEAN	9+5	ST. DEVIATION	
	HIMAFR	POINTS				
	1	h				
	,	16	SAGU.	1380	1769,	
	3	5A1	3888.	5636	2125. 2715.	
		176		6130	1596.	
	A	41	4109	A830,	2882.	
	7	76		7087	1244.	
	A .	71	7691.	9405. 8917.	3596.	
	12	50	7928.	10395.	4675,	
	11	0				
	17					
-	SHID SPEEN METHERN		PLOT SYNA	OL DIAM	OND	
	READFORT	HO, OF DATA	MEAN	RHS	ST. DEVIATION	
	NIJHRFR	PUTHES				
	,		4722.	4767	652,	
	2	17	3845.	4196.	1640.	
	,	4.6	SASA.		1686.	
	;	105	1941. 6094.	4579.	2484.	
	,	126	4879.	5298	2067.	
	7	AO	5721.	5570.	1791.	
	:	16	7597.	8477.	3761.	
	12	0				
	11					
		1				

VXIV

THE PEAK-TO-TROIGH TOLL ANGLE VS BEAUFORT MURBER

RFLATIVE WAVE DIR	ECTION APTHERN	0.0 AND 31.0	PLOT	SYMBOL OCTAGONAL	
NUMBER	POINTS	MEAN	-	ST. DEVIATION	
MONNEN	POINTS				
1		4722.	4767	652.	
2	50	1110.	3523,	1454	
3	47		4439,		
	87	3069.		2003	
5	72	4236	4370,	2951.	
;	55	3519.	45024	4235.	
	20	9404	A161,	4960.	
•	16	3785.	3845	677.	
10	16	4336.	4344.	344.	
11	0				
17	0				
RELATIVE WAVE DIR	FCTTON RETHEFN	\$1.0 AND 61.0	PLOT	SYMBOL TRIANGLE	
REAUFORT		HEAN .		ST. DEVIATION	
METONIAL	POINTS	PEAN	W#8	31. DEALWILLOW	
1	0				
2	4	720.	456	397.	
1	24	4251,		1624,	
4	111			2142.	
	74	3535.	1979.	1826.	
7	31	4432.	4777	1782	
A	12			1974	
9	12	ansa.	4004	390.	
10	*	4195.	4100.	154,	
11	0				
17	•				
RELATIVE WAVE DIR	ECTION BETWEEN	41.0 AND 121.0	PLOT	SYMANL PLUS	
88 10 10 1		MEAN		ST. DEVIATION	
NUMBER	POINTS	MEAN	RHS	ST. DEVIATION	
Williams M	-01-18				
	٨				
5	10	3286.	4006	2361.	
1	72	4419.	4206.	2405.	
4	177	cier.		2204.	
5	190	5711. 5034.	6361	2810.	
7	100	A50A	220.54	2188	
4	30	650A. 8173.	AUTA.	3608.	
4		11590.	11797.	2050.	
1.0	A	10500.	10753.	1695.	
11	0				
15	0				
BALTIAL MARE DIM	SCALUM MEANERN	121.0 AND 151.0	PINT	SYMBOL X	
854:15007	40 OF 0444	MEAN		ST. DEVIATION	
NUMBER	POINTS	TEAM	***	ST, DEVIATION	
1	0				
?	12	4144.	4086.	550.	
3	48	4195.	4728	1743.	
5	98	6150.	7134	2530.	
,	52	6317.		5945	
1	89	7713.	A550.	3689.	
	67	10741.	10910.	1914.	
9	0				
10	9	16397.	16449.	1100.	
11	0				
1,					
*** *****					
RELATIVE WAVE DIG	PCTTON METHER	151.0 AND 180.0	PLDT	SAMBUT DIVHOND	
9FA IFORT	YO. OF DATA	MEAN	-	ST. DEVIATION	
MILINAKE	POINTS		*****	3.4 001141104	
;	20	5309.	92144	217.	
•	40	6127	58244	1080	
,	24		77584	1856.	
	20		41214	643.	
7	52				
A	12	10565.	10810.	2393.	
	1	12180.	17334,	1972.	
10	0				
11	0				
	0				

TAXISHE PLANTISTICH HOLL ANGLE VS BEAUFORT NUMBER

SHIP SPEED RETLEEN	1.0 AND 15.0	PLOT SYPBOL	DETAG	ONAL		VVV
HI ADFORT	NO. OF DATA	HEAN	RMS	ST. DEVIATION		XXV
PAPPLIA	PUINTS			A CONTRACTOR		
1	0					
3	0	12275.	12456.	2132.		
,	53	8718	9617.	4016. 5870.		
•	16	15012.	8340.	1271.		
;	36	16925.	17463.	4315.		
	0					
10	0					
11	0					
15	0					
SHIP SPEED RETAREN	15.0 AND 20.0	PLUT SYMBU	L TRIAN	GL F	•	
					17 . T. S. C.	
HE ALLE OF T	POINTS	MEAN	RMS	ST. DEVIATION		
NUMBER						
1	0					
5	8	4163.	4212.	646.		
4	4	4552.	4639.	694,		
5	0					
,	0			2045.	And the second second second second second	
8		8521.	8762.			
10	4	7947.	8001.	923,		
11	0					
16					A THE RESERVE OF PRINCIPLE OF A	
SHIP SPEED RETAILS	20.0 450 25.0	PLOT SYMA	L PLUS		to a constant	
		MEAN	RHS	ST. DEVIATION		
BEAUFORT	NO. OF DATA	TEAN	RHO	37. 007	A 14 (14 (14 (14 (14 (14 (14 (14	
2	A	6564.	6888.	2086.		
5	55 156	10944. 6148.	11681.	4081.		
1 5	100	9100.	10399.	5034.		
	77	7981.	9614.	5360.		
1	7 A 7 A	11945. 1747A.	13/23.	5985,	**	
9	15	1225.	7525.	2110.		
12	17	7381.	7422.	754.		
12	0					
SHIP SILLE HETAFEN	25.0 AND 30.0	PLIIT SYNS	OL X			
BEAUF-IRT	POINTS	MEAN	RMS	ST. DEVIATION		tarris armed Month Source
	PRINTS					
1	0					
,	16	48/2.	6010.	3520. 4731.		
4	102	6790. 8873.	8276.	5705.		
,	176	9461.	11516.	0566.	The same of the sa	
7	76	11507. 1393A,	15535.	6896.		
1	51	15080.	17359.	6448.		
9	11	14507.	20588.	7373.		
11	0				19	
12	0					
	** * * **	9: 05 5000	UL DIAM	OND		
SHIP SPECO RETHERN		PLOT SYMB				
BEAUFORT	NO. OF DATA	WEAN	BMS	ST. DEVIATION		
`				1100		
;	12	7458.	7627	3053.	115 - 128 - 12 - 12 - 12 - 12 - 12 - 12 - 1	
,	48	6512.	7141.	3393.	The state of the s	
	172	7027.	17148	5237. 3848.		
5	126	11523.	10600.	4747.	• •	
,	ма	9771.	10681	4514,		
	15	15133,	17309.	04011		
10	0					
11	3					
1						

MAXIMIM PEAK-TO-TROUGH BOLL ANGLE VS BEAUFORT NUMBER

RPLATTUP WAVE OTR				SYMBOL OCTAGONAL	X
REALIFORT	POINTS	MFAN	P1-8	ST. DEVIATION	
1		7458.	7627	1689,	
,	20	5011.	9904.	3122.	
•	47	6870.			
:	87	9026. 7701.		4026	
	72	5893.	9516,	5593. 5931.	
1	"	12827.	15000	7793.	
	20	16801.	I OOGA.	9077.	
•	16	6916.	7114	1000.	
10	16	7670.	7722.	902.	
11					
RELATIVE WAVE DIR	ECTION METHEEN	31.0 AND 61.	0 PLOT	SYMBOL TRIANGLE	
REAUFORT	HO. OF DATA	MEAN	RHS	ST. DEVIATION	
,	0				
,	4	568,	1137.	984.	
1	50		8025.	305A.	
9	111	5771. 6124.	7311.	4489. 3839.	
;	35	4070	7678.	3201.	
7	51	7694.	8642.	3935.	
	32	10413.	11147	4034	
.:	15	8626.	8702.	1145.	
10		7764.	7810.	855.	
15	•				
RPLATTYF WAVE DIR	ECTION RETWEEN	61.0 AND 121	.0 PLOT	SYPHOL PLUS	
REALIFORT	NO. OF DATA	MEAN	RHS	ST. DEVIATION	
1	0				
,	10	4824.	4504.	3947.	
3 4	72	8001.	.502.	5123.	
•	177	10440.	12037	5990.	
6	128	9114			
7	109	IDAKA	10014	5635.	
•	34	15318.	17751.	7934.	
10	*	21514.	21054.	4377.	
11	6	roine.	Sinay.	3827.	
is	•				
RPLATTYP MAVE DIP	ECTION METHERN	171.0 AND 151.	.0 PLOT	SYMBOL X	
REAUFIRT	NO. OF DATA	HEAN	RHS	ST, DEVIATION	
	0				
2	17	660a.		1068.	
1	44	7408.	*508*	3516.	
•	**	11110	12207.	5131.	
:	92	12300.	13400.	\$153.	
;	37	14702.	12810. 14507.	56114 7507	
	67	19934	20350,	4133.	
	0				
10		38401"	33141.	3165.	
13					
RFLATIVE MAVE DIR	FCTION SETWERN	191.0 AND 180.	0 -101	SYMBOL OTANONO	
BEAUFORT	NO. OF DATA	HEAN		ST. DEVIATION	
NUMBER					
1	:	8527. 9788.	8574.	***	
,	50	9786.		4053,	
:	44	12141		4507.	
:	20	14504		3001.	
;	52	6554.	14090	1920	
4	12	15007.	20816.	4049	
•	7	21445.	21760.	3486.	
10	0				
	0				

SHE PITCH ANGLE VS REAUFORT NUMBER SHIP AFEED METHEEN 1.0 AND 15.0 PLOT SYMBUL OCTAGONAL IIVXX MEAN RMS ST. DEVIATION NO DATA POINTS SMIP SPEED BETHEEN 15.0 AND 20.0 PLOT SYMBOL TRIANGLE NO. OF DATA HEAN RHS ST. DEVIATION 1851. 142. SHIP SPEED BETHEEN 20.0 AND 25.0 1765. 1767. 108. SHIP SPEED BETHEEN 25.0 AND 30.0 PLOT SYPHUL X RMS ST. DEVIATION 65. 149. 310. SHIP SPEED RETREEN 30.0 AND 35.0 PLOT SYMBUL DIAMOND MEA". PHS ST. DEVIATION

RMS PITCH ANGLE VS BEAUFIRE NUMBER

and the second second	DEVIATION	R#8 AT	HEAR	MO. OF DATA	HEAUFORT
	V			POINTS	NO. NEW
					1
1	65,		687.	4	1
	56;	701.	698,	: -	:
		,		ò	
	73.	864.	861.		1
	448. 87.	1142.	1765.	•	:
	103,	1783.	1780.		10
				•	11
					12
	OL TRIANGLE	PLOT SYMB	.0 AND 61.0		LATIVE WAVE DIRE
	DEVIATION	RHS 57,	HEAN	NO. OF DATA	TREAL SHE
				0	1
					1
	439,	1076.	983,		•
-	674	507.	503.	4	
	106.	1749.	1746	•	:
	95.	1515.	1512.		
	145,	1747.	1741.	•	10
				0	- 12
	IOL PLUS	PLOT AYMS	.0 AND 121.0	ECTION BETREEN 6	LATIVE WAVE DIRE
	DEVIATION	RHS ST.	MEAN	AD. OF DATA	REAUFORT
				0	1
and the same of the same of	92.	797.	191.	0	•
	203.	994.	973.	15	4
	185.	817.		20	
	370.	1345.	1293.	20	;
the second second second second	10.	454.	450.		
				0	•
	**.	588.	560.	0	11
				•	12
		PLOT 3448		ECTION HETHERN 12	
,	06VI47104	ans 57.	PEAC	POINTS	RESIFIET
				•	1
				0	1
	92.	825.	820.	0	1
	263,	842.	621.	16	,
			1172.		*
	182.	1186.	1045		
	101.	1186.	1067.		
	101.	1072.	1067.	8	:
	182.	1186.	1067.		10
. ,	101.	1072.	1067.	8	:
	101,	1072.	610.	- 8 0 0 3	10
	101,	610. PLOT 8YP8	610.	6 CATION PELMEEN T2	LATIVE WAVE DIRE
	101.	610. PLOT 8YP8	610.	ECTION SETNERN 15	LATIVE WAVE DIRE
	101.	610. PLOT 8YP8	610.	ECTION SETHERN 15	SOUPORT NUMBER 1 2 3
	162, 101, 20, 10L DIAMONO DEVIATION	1072. 610. PLOT 8YP8 RHS 8T.	610. 610. 1.0 APR 180.0 HEAN	ECTION SETHEEN 15	SEAUPORT NUMBER
	162, 101, 20, 10L DIAMONO DEVIATION	1072. 610. PLOT SYPS RHS ST.	610. 610. 610. 610. 610. 610.	ECTION SETHERN 15	LATIVE WAVE DIRIC BEAUFORT NUMBER
	101. 20. 20. 10L DIAMOND DEVIATION 20.	1072. 610. PLOT SYMB RMS ST.	610. 610. HEAN	ECTION BETWEEN 15 NO. OF DATA POINTS	LATIVE WAVE DIRIC BEAUFIRET NUMBER
	102, 101, 20, 10U DIAMOND DEVIATION	1072, 610, PLOT 8YM8 RM8 8T, 679, 744, 672,	610. 610. 610. 610. 610. 610. 610. 610.	ECTION SETNEEN 15 NO. OF DATA POINTS	SEAUPORT NUMBER 12 3 5 5 7 6
	101. 20. 20. 10L DIAMOND DEVIATION 20.	1072. 610. PLOT SYMB RMS ST.	610. 610. HEAN	ECTION BETWEEN 15 NO. OF DATA POINTS	EATIVE WAVE DIRIC BEAUFIRET MUMBER 1 2 3 4 5

MAXIMUM PITCH ANGLE VS BEAUFORT NUMBER SHIP SPEED RETHEEN 1.0 AND 15.0 PLOT SYMBUL OCTAGONAL XIX MEAN RHS ST. DEVIATION NO DATA POINTS SHIP SPEED RETHEEN 15.0 AND 20.0 PLOT SYMBOL TRIANGLE NO. OF DATA REAUFORT MEAN RMS ST. DEVIATION SHIP SPEED BETHEEN 20.0 AND 25.0 PLCT SYMBUL PLUS REAUPORT NO. OF DATA NUMBER POINTS MEAN RMS ST. DEVIATION SHIP SPEED BETWEEN 25.0 AND 30.0 PLOT SYMBUL X NO. OF DATA PHS ST. DEVIATION HEAN 1657. 2050. 1917. 201. 377. 631. SHIP SPEED BETWEEN 30.0 AND 35.0 PLOT SYMBOL DIAMOND RMS ST. DEVIATION MEAN

MAXIMUM PITCH ANGLE VS REALIFORT NUMBER

######################################	RESUFORT	NO. OF DATA	HEAN	-	ST. DEVIATION	
1457, 1480, 261, 376, 1470, 1771, 326, 1770, 1771, 326, 1771, 3271, 3		POINTS				
### ### ### ### ### ### ### ### ### ##	1					
1976			1657,	1680.	281	
RELATIVE PAVE DIRECTION BETWEEN \$1.0 AND \$1.0 PLOT SYMBOL TRIANGLE PREMISED NO. P. DATA NUMBER POINTS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL TRIANGLE PREMISED NO. P. DATA NUMBER POINTS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL PLUS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL PLUS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL PLUS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL PLUS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL PLUS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL PLUS RELATIVE PAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL X PRESENCE NO. P. DATA NUMBER POINTS RELATIVE WAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL X PRESENCE NO. P. DATA NUMBER POINTS RELATIVE WAVE DIRECTION RETWEEN \$1.0 AND \$1.0 PLOT SYMBOL X PRESENCE NO. P. DATA NUMBER POINTS RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL X PRESENCE NO. P. DATA NUMBER POINTS RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION RETWEEN \$1.10 AND \$1.0 PLOT SYMBOL DIRECTION RELATIVE WAVE DIRECTION \$1.10 PLOT SYMBOL DIRECTION RELATIVE \$1.0 PLOT SYMBOL DIRECTION RELATIVE \$1.0 PLOT SYMBOL DIRECTION RELATIVE \$1.0 PLOT SYM			1496.	1536,	376.	
RELATIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL TRIANGLE PRESENTATION NO. OF DATA NEAR PHS 81. DEVIATION ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLAG ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLAG ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLUS ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLUS ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLUS ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLUS ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLUS ***PARTIVE - AND DIDECTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL FLUS ***PARTIVE - AND DIDECTION RETWEEN 121:0 AND 131:0 PLOT SYMBOL X ***PARTIVE MANY DIDECTION RETWEEN 121:0 AND 131:0 PLOT SYMBOL X ***PARTIVE MANY DIDECTION RETWEEN 121:0 AND 131:0 PLOT SYMBOL X ***PARTIVE MANY DIDECTION RETWEEN 121:0 AND 131:0 PLOT SYMBOL X ***PARTIVE MANY DIDECTION RETWEEN 121:0 AND 131:0 PLOT SYMBOL X ***PARTIVE MANY DIDECTION RETWEEN 131:0 AND 131:0 PLOT SYMBOL DIAMOND ***PARTIVE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTINE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTIVE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTIVE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL DIAMOND ***PARTITE MANY DISPCTION RETWEEN 131:0 AND 180:0 PLOT SYMBOL D						
RELATIVE MANY DISECTION RETWEEN \$1.0 AND \$12.0 PLOT SYMBOL TRIANGLE PERIFORM NO. OF DATA NEAN SHS ST. DEVIATION PERIFORM NO. OF DATA NEAN SHS ST. DEVIATION 1	,	4	1944.	1971.	326.	
RELATIVE WAVE DISPECTION BETWEEN \$1.0 AND \$1.0 PLOT SYMBOL TRIANGLE PREMISSORT NO. OF DATA	•		9149	2548,	1002.	
RELATIVE WAVE DISPECTION SETUREN SILO AND 61:0 PLOT SYMBOL TRIANGLE PRINTED NAT. OF DATA NUMBER POINTS 1 0 2 2267. 2394. T68. 1 120. 1375. 1375. 1377. 2 0 1220. 1375. 1375. 1377. 2 0 1376. 2387. 1375. 1377. 2 0 1376. 2387. 1375. 1377. 2 0 1376. 2387. 1375. 1377. 2 0 1376. 2387. 2387. 2387. 2 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			4395.	0016	120	
### AVE DISPECTION BETWEEN \$1.0 AND \$1.0 PLOT SYMBOL TRIANGLE #### POINTS	11					
PRINTED NO. OF DATA NUMBER POINTS	13	•				
	SELATIVE HAVE DIS	FCTTON BETWEEN	31:0 AND 61:0	PLOT	SYMBOL TRIANGLE	
### POINTS ### POINTS ### POINTS ### POINTS ### POINTS ### POINTS #### POINTS #### POINTS #### POINTS ##### POINTS ###################################	PEATIFORT	NO. OF DATA	MEAN		ST. DEVIATION	
### 1267. 2304, 768, 1676. 167	HUMAFR	POINTS				
## 1 2267, 2394, 768, 1 1626,	;					
## 1 2267, 2304, 788, 1226, 1624, 81, 1326, 1325, 1375, 1376, 2375, 1376, 2375, 1376, 2375, 1376, 2375, 10	i					
## 1872. 1375. 137. ## 1372. 1375. 137. ## 1372. 1375. 137. ## 10	4					
### AND DESCRIPTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL PLUS ###################################				2304	768.	
### AND DESCRIPTION RETWEEN 61:0 AND 121:0 PLOT SYMBOL PLUS ###################################	;		1128	1335	137.	
## 10		4	3760.	3/00.	250,	
## ATTIVE PARK DISECTION RETWEEN 121,0 AND 121.0 PLOT SYMBOL PLUS ### ATTIVE PARK DISECTION RETWEEN 121,0 AND 121.0 PLOT SYMBOL PLUS ### ATTIVE PARK DISECTION RETWEEN 121,0 AND 181.0 PLOT SYMBOL X ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL X ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL X ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL X ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL X ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL X ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISECTION RETWEEN 151,0 AND 180.0 PLOT SYMBOL DISHOND ### ATTIVE PARK DISHOND ### AT			3680.	1700	287.	
### PRINTIPLE OF PRINTS 10 AND 121.0 PLOT SYMBOL PLUS			4006.	4018.	303.	
### ST. DEVIATION #### POINTS	12	·				
### ST. DEVIATION #### POINTS	PARTE -AVE DID	FCTION RETHERN	61 0 AND 121 0	PLOT	SYMBOL PLUS	
1 0 0 1672, 1627, 138, 2702, 2504, 679, 127, 270, 1819, 1670, 451, 1770, 977, 70, 1210, 90, 1210, 1210, 90, 1210, 1210, 90, 1210, 1210, 90, 1210, 1210, 90, 1210, 1210, 1210, 90, 1210, 1210, 90, 1210	-					
### ### ### ### ### ### ### ### ### ##	NUMBER	POINTS				
### 1672, 1672, 1673, 1794, 17	!					
### 172	i	4	1622.	1627:	136:	
10 1210, 1771,	4	12	2747.	2303.	470	
### A				1870.		
### 1210, 12	;		1021	3127	600	
10 8 1370, 1303, 195, 111 0 0 112 0 0 SPIATIVE MANY DISPRETION RETWEEN 121,0 AND 151.0 PLOT SYMBOL X REALFORDT NO, OF DATA PAN NIMBER POINTS 1 0 1 0 1726, 1727, 70, 2 1 0 1802, PASO, 310, 3 180 1802, PASO, 310, 5 10 3 1803, 1806, 310, 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		4	1810.	1214.	99.	
### PPLATIVE MAVE DISPECTION RETWEEN 121,0 AND 151.0 PLOT SYMBOL X ###################################		0				
### PLATIVE MAVE DISPECTION RETWEEN 121,0 AND 151.0 PLOT SYMBOL X #### POINTS			1377.	1303.	193.	
### POINTS						
### POINTS	RPI ATTVF WAVE DTS		121 O AND 151	PLOT	SYMBOL X	
#FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND #FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND ##FAUTUR NAVE DIRECTION HETWEFN 151,0 AND 180,0 PLOT SYMBOL DIAHOND ###################################	PEA IFORT	VA. OF DATA				
### ##################################	NIVAFA	POINTS				
######################################	;					
### 1776, 1777, 70, 1872, 1873						
#FAUTOUR NOT DATA #FAUTOUR NOT	4	4 .	1776.	1727:	70;	
PFLATIVE WAVE DISECTION HETWERN 151,0 AND 180,0 PLOT SYMBOL DIAMOND #FAJFORY NO. OF DATA MEAN RMS ST, DEVIATION 1 0 2 0 3 0 4 0 0 5 0 1000. 1080. 303. 6 0 0 7 27 1626. 1724. 571. 7 27 1676. 1570. 280.		16	1982.	2584	139.	
### 1805. 1306. 89: 11			2621	2640.	310.	
10 3 1305. 1306. 89: 11 0 11 0 0 1305. 1306. 89: 11 0 0 11 0 0 1305. 1306. 89: 11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			total in the same			
### 150 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0		110		
#FA:)FORT NO. OF DATA HEAN RMS ST, DEVIATION #FA:)FORT NO. OF DATA HEAN RMS ST, DEVIATION 1 0 2 0 3 0 4 0 5 0 6 0 7 27 1626, 1724, 571, A 1556, 1570, 280, B 7 177, 1771, 1864	11		1303.	1308.	***	
#FAJFORT NO. OF DATA HEAM RMS ST. DEVIATION 1	"	,				
1	PPLATIVE WAVE DIR		151.0 AND 180.0	PLOT	SYMAN PIANONO	
1	HELDFORT	NO. OF DATA	HEAH	R45	ST, DEVIATION	
3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	,	4				
0 1800. 1800. 383. 0 1870. 1724. 571. 0 1550. 1570. 280. 0 1771. 886.	1	0				
7 27 1626, 1724, 571, 4 1559, 1570, 250,	4	:	1640.	1680.	365.	
4 1550, 1570, 250, 7 1476, 1771, 344		•				
7 1678. 1771. 566.			1474.	1724.	571.	
	?	61	1500	1570	384	

IXXX

SHIP SPEED BETAFEN	1.0 440 15.0	PLOT SYMBUL	DCTAG	UNAL	
8F&UF-)4T	NO, OF DATA	MEAN	RMS		DEVIATIO
NUMMER					
1	9				
3	22	494.	506.		186.
5	15	1023	1071.		314.
;	12	533.	534.		267.
•	0				
10	0				
11	•				
18	٠				
HIP SPEED RETAREN	15.0 AND 20.0	PLOT SYMBOL	TRIAN		
REAUFORT	POINTS	MEAN	RMS	57.	DEVIATIO
1 2	0				
1	A	368,	371.		50.
5	0				
;	0				
	8	2365.	2371.		169.
10	4	3404.	3407.		152,
15	0				
HIP *PEER BET.EFH	20.0 AND 25.0	PLOT SYMBOL	PL US		
BEAUFORT	NO. OF DATA	NEAN		37,	DEVIATIO
NUMBER					
1	0	457.	464.		77.
:	136	999.	1051.		676
5	119	1169.	1548		565.
;	72	1184.	1351.		564.
d	67		1506.		858.
10	12	2885.	1525		171.
11		3217.	3221.		1/1.
15	0				
HIP SPEED HETAEFN	25.0 AND 50.0	PLOT SYMBOL	×		
BE AUFORT NUMBER	POINTS	MFAN	ннз	st.	DEVIATIO
;	16	355,	547.		417.
3	78		1032.		450.
,	157	. S88	1076.		672.
,	45 73		700		294
	51	847.	1091.		686.
10	31	2244.	2488.		1065.
11	0	1790.	1974.		831.
12	0				
HIP SPEED RETREEN	30.0 440 35.0	PLOT SYMBUL	DIAMO	ND	
RF &UF (IP +	NO. OF DATA	MEAN	P#8	57.	DEVIATIO
;	4	889.	894.		
i	47	493	603.		280.
:	100	724.	865.		474.
,	121	1069.	1335.		610.
1	67	1300.	1632.		769.
	15	1670,	1000.		1042.
10	0				

MAS PHRAMAD HOLE VENTICAL ACCELERATION VS HEADFORT NUMBER

HELATIVE MAVE OF	RECTION BETWEEN	0.0	AND 31.0	PLOT	344906	UCTAGONAL
HE AUFORT NUMBER	POTATS		MEAN		87. OE	VIATION
1			844.	840,		
2	50		400.	735.		425.
,	46		1037.	1133.		758.
•	83		1062.	1202.		424.
	57		1101.	1376.		424
7	55		1461.	1559.		487.
•	50		1039.	1429,		981,
10	16		3257.	3266,		717.
ii						
11	•					
RELATIVE MAVE OF	SECTION METHERN	11.0	AND 61.0	PLOT	SYMBOL	TRIANGLE
PERMIN	NO. OF DATA		MEAN	RMS	ST. DE	VIATION
	. 0					
	4		98.	101.		24.
	20		539,	931.		410.
•	109		BOR.	1000.		590.
	35		744	787.		249.
!	48		1079.	1278.		684.
:	32		2496.	2559.		562.
10			3247.	3255.		190.
11	0					
15	٠					
RELATIVE NAVE OF	HECTION SFINEEN	61.0	AND 121.0	PLOT	SYMBOL	PLUS
REAUPIDE	"O OF 0. **		PEAN		47 DE	VIATION
# 3P#(#	POINTS				0., 00	
1	0					
1	10		920.	304.		122.
	164		7AL.	1015.		646.
5	183		1050.	1231.		642.
;	125		1400.	1049		590.
	108		836.	928.		402.
9			1466.	1517.		510.
10			1215,	1254.		308.
11						
		2				
RELATIVE MAVE DI	RECTION HETHERN	121.0	AND 151.0	PLOT	SYMBOL	×
BEAUFIDRT	MO. OF PATA		MEAN	RMS	ST. DE	VIATION
HIMMEH	PHINTS					
1	0					
,	12		426.	476.		211.
	91		454	730.		382.
5	78		1016-	1159.		557.
;	50		1102.	1393.		563.
	59		660,	743.		342.
•	0		1470.			
10	4		1470.	1470.		21.
15	0					
					-	DIAMONO
		131.0		PLOT		
MEAUF IRT NUMBER	NO. UF DATA		MEAN	RH5	ST. DE	VIATION
;	0		424,	525.		43.
	19		480-	505.		159.
;	45		1306.	863.		442.
;	16		A 2 0	1365.		70.
,	50		ASO	1017-		556.
:	12		802.	848.		276.
10	7		1119.	1327.		714.
11	0					
15	•					

IIXXX

IIIXXX

MARTHUM FORMARD HOLL VERTICAL ACCELERATION VS REAUFORT NUMBER

SHEP SPEED HETHEN	1.0 AND 15.0		OCTAG	ONAL	
REAMFORT	POINTS	MFAN		ST.	DEVIATION
Nilaiten	POINTS				
;	ò				
	7	1101.	1123.		219.
	55	1067.	1150.		451. 755.
:	15	1215.	12551		134
,	15	2404.	2876.		614.
	0				
9	0				
10	0				
13	•				
SHIP SPEED RETHEN	15.0 AND 20.0	PLOT SYMBOL	TRIAN	GLF	
REAUFORT	NO. OF DATA	HEAN	PH3	ST.	DEVIATION
Hijuned					
!	^				
,		851.	861,		142.
,	a	989,	1018.		243.
5	•				
• •	0				
7	2	5065.	5100.		590.
	•				
10	4	7191.	7198.		524.
- !!	•				
841P SPFFN 951-564	20.0 ALD 25.0	PLOT SYMBOL	PLUS		
REAMENRY		MFAN	PHS	97.	DEVIATION
NUMBER	POTNER			3	
,	0				
,		1012.	1046.		171.
	40	2309.	2745.		1485.
4	110	1932.	2397.		1418.
,	12		3065		1070.
,	67	2849.	3130.		1304.
	67		1350.		1875.
10	12	6717.	6303.		HA1.
11	0	6/1/.	K/41.		. 507.
12	· ·				
	25.0 AND 30.0	PLOT SYMBOL	¥		
BF 411F 107	40. 05 DATA	MEAN	B = 5		DEVIATION
H-MHF H	POINTS		n-3	3	DEVIATION
1	٨				
*	16	730.	1188.		917.
4	7A 157	203A. 1891.	2405.		1613.
4	160	2001-	2480.		1464.
4	44	1936.	1742.		821.
, ,	71	2288	2541.		1158.
•	51	1994.	5749		2313.
10	50	4145.	4531.		1830.
!!	2				
SHIP SPEED DETWEEN	30.0 AND 35.0	PLAT SYMBOL			
REALIFTOT	NO. OF DATA	HEAN		97.	DEVIATION
,		2031.	2050.		279.
,	22	1150	1535.		721.
,	47	1583.	1816.		
4	100		1950.		1069.
	121	2454.	1015.		1340.
;	121	3215.	3819.		2061.
	15	3215.	4153.		2021.
,					
!1	*				
17	*				

MAYIMUM FOR AND HILL VENTICAL ACCELERATION VA REAUFORT NUMBER

RELATIVE MAVE OTRECTION RETHERN 0:0 AND 31:0 PLOT SYMBOL OCTAGONAL XXXIV MA. OF PATA WFAN MMS BY DEVIATION NUMBER 2031. 1364. 2335. 2125. 2429. 2475. 3414. 2378. 7298. 6201. 2050. 1717. 2555. 2736. 2649. 5106. 3621. 4232. 7337. 6387. 1 2 3 4 5 7 8 9 10 11 12 279. 1044. 1036. 1723. 1489. 1877. 1208. 2188. 756. 1531. RELATIVE MAVE OTHECTION HETHERN 31.0 AND 61:0 PLOT SYMBOL TRIANGLE NO. OF DATA MEAN RMS ST. DEVIATION 165. 1891. 1201. 1812. 1767. 2458. 5501. 6031. 179; 2104; 1641; 2230; 1899; 2903; 5637; 6078; 6997; 71. 925. 1118. 1300. 695. 1545. 1232. 755. 423. RELATIVE MAVE OTOFCTION RETWEEN 61.0 AND 121.0 PLOT SYMBOL PLUS RESURTING NO. OF DATA MESH RMS ST, DEVIATION 100 733. 2638. 2343. 2747. 2545. 1546. 2140. 3713. 2937. A6A. 2123. 1A15. 2375. 2160. 3174. 1933. 3557. 2493. 302. 1565. 1513. 1457. 1583. 1590. 919. 1064. 508. RELATIVE WAVE DISECTION RETHEFN 121.0 AND 151.0 PLOT SYMBOL X 942. 1050. 1430. 2275. 2482. 2850. 1508. 1067; 1244; 1604; 2575; 3116; 3179; 1718; 502. 666. 908. 1205. 1683. 1410. 822. 3507. 3523. 353. BELLTIVE MAVE DIRECTION PETHEEN ISL'S AND 180.0 PLOT SYMBOL DIAMOND PERSONNEL NO. OF DATA MEAN NUMBER POINTS RMS ST. DEVIATION 1117. 1079. 1649. 299A. 96A. 1965. 1874. 2881. 1132. 1153. 1923. 1923. 993. 993. 1926. 1926. 181. 406. 9A8. 9A6. 217. 1314. 615. 10 4 4 7 7 7 7 7 7

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BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE 2. GOVT ACCESSION NO. ECIPLENT'S CATALOG NUMBER SSC-264 TITLE Fand Subtine TYRE OF REPORT & PERTOD COVERED FIRST SEASON RESULTS FROM SHIP RESPONSE INSTRU-MENTATION ABOARD THE SL-7 CLASS CONTAINERSHIP S.S. SEA-LAND McLEAN IN NORTH ATLANTIC SERVICE. Technical Repert, 10/8/72 - 4/5/73 PERFORMING ORG. REPORT NUMBER

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CONTRACT OR GRANT NUMBER (*) AUTHOR(s) R. R. Boentgen, R. A. Fain and J. W. Wheaton N00024-73-C-5059 9. PERFORMING ORGANIZATION NAME AND ADDRESS PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Teledyne Materials Research Inc. Waltham, MA. 02154 SR-211 Naval Ship Engineering Center REPORT DATE September 1976 Department of the Navy Washington, D.C. 20364 182 14. MONITORING AGENCY NAME & ADDRESS(If different from Controlling Office) Ship Research Committee Unclassified National Academy of Sciences Washington, D.C. 20418 DECLASSIFICATION DOWNGRADING 16. DISTRIBUTION STATEMENT (of this Report) This document has been approved for public release and sale; its distribution is unlimited. ntered in Block 20, Il different from Report) 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necess ry and identify by block number) 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report contains data, with appropriate evaluation and discussions, collected during the first season on board the S.S. SEA-LAND McLEAN. collection began with westbound Voyage 1 on October 8, 1972 and terminated with the eastbound passage of Voyage 12 on April 5, 1973. A total of 80 data tapes were recorded containing in excess of 50,000 separate data intervals from more than 100 transducers. Mage

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cont

20. ABSTRACT (Cont'd).

Discussions include a description of the digitized data, comparisons of stresses with sea state, simultaneous response data from all transducers during selected portions of a rough voyage, and a consideration of torsional responses.

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TELEDYNE MATERIALS RESEARCH WALTHAM MASS
FIRST SEASON RESULTS FROM SHIP RESPONSE INSTRUMENTATION ABOARD --ETC(U)
SEP 76 R R BOENTGEN, R A FAIN, J W WHEATON N00024-73-C-5059
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METRIC CONVERSION FACTORS

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	eden Frank	Square inches square yands square mides acces	ences pende son ros	fluid ounces pints quests gallons cubic fest cubic yands	Fahrenheit temperature	00 00 00 00 00 00 00 00 00 00 00 00 00
nsions from Metri Mattight by LENGTH	\$200 5	. 0.14 1.2 0.4 .7 2.5 MASS (weight)	0.036 2.2 1.1 VOLUME	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	TEMPERATURE (exact) 3.5 (these need 32)	02 03 04 04 05 04 05 05 05 05 05 05 05 05 05 05 05 05 05
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